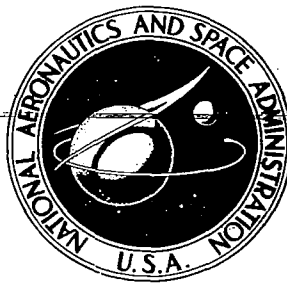


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**DESAP 1 - A STRUCTURAL DESIGN PROGRAM
WITH STRESS AND DISPLACEMENT CONSTRAINTS**

Volume III: Program Listing

J. Kiusalaas and G. B. Reddy

Prepared by

THE PENNSYLVANIA STATE UNIVERSITY

University Park, Pa. 16802

for George C. Marshall Space Flight Center

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16. ABSTRACT <p>DESAP 1 is a finite element program for computer-automated, minimum weight design of elastic structures with constraints on stresses (including local instability criteria) and displacements. Volume 1 of the report contains the theoretical and user's manual of the program. Sample problems and the listing of the program are included in Volumes 2 and 3, respectively.</p> <p>The static analysis portion of DESAP 1 is based on the SOLID SAP finite element program developed at the University of California, Berkeley. In design, the stress ratio method is employed for the stress constraints, whereas the displacement constraints are handled by solving the appropriate optimality criterion.</p> <p>The element subroutines have been organized so as to facilitate additions and changes by the user. As a result, a relatively minor programming effort would be required to make DESAP 1 into a special-purpose program to handle the user's specific design requirements and failure criteria.</p> <p>DESAP 1 is a companion program of DESAP 2, "A Structural Design Program with Stress and Buckling Constraints." With the exception of a few cards, the same data deck can be used for both programs.</p> <p>This is Volume 3 of three volumes.</p>					
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```

C*****CMAIN0000
C*****CMAIN0010
C**                                     **CMAIN0020
C**  DFSAP1---AN AUTOMATED DESIGN PROGRAM WITH STRESS AND          **CMAIN0030
C**  DISPLACEMENT CONSTRAINTS BASED ON SAP2 ANALYSIS PROGRAM      **CMAIN0040
C**                                     **CMAIN0050
C**  BY J.KIUSALAS AND G.A.REDDY   ( MAY , 1976 )                 **CMAIN0060
C**                                     **CMAIN0070
C*****CMAIN0080
C*****CMAIN0090
COMMON /JUNK / HED(20),JUN(280)                                MAIN0100
COMMON /FLPAR/ NPAR(14),NUMNP,MRAND,NELTYP,N1,N2,N3,N4,N5,MTOT,NEOMAIN0110
1,NUMF1,NUMDV,M1,M2,M3,LL,LR,NFOR,NALOCK                          MAIN0120
COMMON/UNITS/ IR,IW,IP,I1,I2,I3,I4,I5,I10,I11,I12                MAIN0130
COMMON/FM/ QQQ(5066)                                             MAIN0140
COMMON/CONTR/ ICYCL,NCYCL,ISCALE,NSCALE,KSCALE,KONVG,IDESN,IWTMIN,MAIN0150
IWTMIN,EPSIL,DELTA1,DELTA2,KPUNCH,KDISP,NMAXD,NDISP,LB1,ALPA,SF,IS,MAIN0160
1,SMAX,DMAX,DMFGA                                               MAIN0170
C*****CMAIN0180
C-----PROGRAM CAPACITY CONTROLLED BY THE FOLLOWING THREE STATEMENTS  MAIN0190
C*****CMAIN0200
DIMENSION A(6000)                                               MAIN0210
REAL*8 AD(3000)                                                 MAIN0220
FOURVALENCE (A(1),AD(1))                                       MAIN0230
MTOT=6000                                                        MAIN0240
C*****CMAIN0250
C-----INPUT-OUTPUT UNIT ASSIGNMENTS                               MAIN0260
C*****CMAIN0270
IR=5                                                             MAIN0280
IW=6                                                             MAIN0290
IP=7                                                             MAIN0300
I1=1                                                             MAIN0310
I2=2                                                             MAIN0320
I3=3                                                             MAIN0330
I4=4                                                             MAIN0340
I5=5                                                             MAIN0350
I10=10                                                            MAIN0360
I11=11                                                            MAIN0370
I12=12                                                            MAIN0380
C*****CMAIN0390
C-----PROGRAM CONTROL DATA                                     MAIN0400
C                                                             MAIN0410
C-----NUMNP = NUMBER OF NODE POINTS                             MAIN0420
C-----NELTYP = NUMBER OF ELEMENT TYPES                           MAIN0430
C-----LL = NUMBER OF LOAD CONDITIONS                             MAIN0440
C-----NUMDV = NUMBER OF INDEPENDENT DESIGN VARIABLES            MAIN0450
C*****CMAIN0460
5 READ(IR,1000)HED,NUMNP,NELTYP,LL,NUMDV                        MAIN0470
IF (NUMNP.EQ.0) STOP                                             MAIN0480
WRITE(IW,2000)HED,NUMNP,NELTYP,LL,NUMDV                         MAIN0490
C*****CMAIN0500
C-----DESIGN CONTROL DATA                                     MAIN0510
C                                                             MAIN0520
C-----KPRINT = PRINT OUT CODE                                    MAIN0530
C          =0 NOODAL DISPLACEMENTS NOT PRINTED                 MAIN0540
C          =1 NOODAL DISPLACEMENTS ARE PRINTED                 MAIN0550
C-----KPUNCH = PUNCH OUT CODE FOR RESTART DECK                 MAIN0560
C          =0 NO RESTART DECK PUNCHED                           MAIN0570
C          =1 PUNCHES RESTART DECK FOR DESIGN VARIABLE DATA   MAIN0580
C-----KDISP = CODE FOR DISPLACEMENT CONSTRAINTS               MAIN0590

```

```

C          =0 NO DISPLACEMENT CONSTRAINTS ARE PRESENT          MAIN0600
C          =1 DISPLACEMENT CONSTRAINTS ARE PRESENT             MAIN0610
C-----NMAXD = NO. OF MAX. DISPLACEMENT CONSTRAINT RATIOS TO BE MAIN0620
C              CONSIDERED IN REDESIGN                            MAIN0630
C-----IDESN = CURRENT DESIGN NO.                               MAIN0640
C-----ICYCL = CURRENT CRITICAL DESIGN NO.                     MAIN0650
C-----NCYCL = MAX. ALLOWABLE NUMBER OF CRITICAL DESIGNS       MAIN0660
C-----KONVG  = DESIGN CONVERGENCE CODE                         MAIN0670
C          =1 DESIGN IS NOT CRITICAL                             MAIN0680
C          =2 DESIGN IS CRITICAL FOR DISPLACEMENT CONSTRAINTS  MAIN0690
C          =3 DESIGN IS CRITICAL FROM STRESS CONSTRAINTS        MAIN0700
C          =4 DESIGN IS ACCEPTABLE                               MAIN0710
C-----DELTA = DEFINES BAND OF CRITICAL DESIGNS               MAIN0720
C-----EPSIL = DEFINES ALLOWABLE WEIGHT INCREASE OVER WTMIN    MAIN0730
C-----WTMIN = MIN WEIGHT CRITICAL DESIGN                      MAIN0740
C-----IWTMIN = DESIGN NUMBER OF MIN. WT. CRITICAL DESIGN      MAIN0750
C-----ISCALF = SCALING OPERATION NUMBER                       MAIN0760
C-----NSCALF = MAX. ALLOWABLE NUMBER OF SUCCESSIVE SCALING OPERATIONS MAIN0770
C-----KSCALF = CODE FOR SCALING OPERATION                     MAIN0780
C          =-1 SCALING SHOULD NOT BE USED                       MAIN0790
C          =0 SCALING IS APPROXIMATE. REANALYSE SCALED STRUCTURE MAIN0800
C          =1 SCALING IS EXACT. STIFFNESS IS PROPORTIONAL TO SIZE MAIN0810
C          =2 SCALING IS EXACT. STIFFNESS IS PROPORTIONAL TO (SIZE)**2 MAIN0820
C          =3 SCALING IS EXACT. STIFFNESS IS PROPORTIONAL TO (SIZE)**3 MAIN0830
C          =4 SCALING IS EXACT. STIFFNESS IS PROPORTIONAL TO (SIZE)**4 MAIN0840
C              AND SO ON                                         MAIN0850
C-----ALPA  = RELAXATION PARAMETER IN DISPLACEMENT REDESIGN MAIN0860
C          =0.05                                                MAIN0870
C-----OMEGA = RATIO OF STRESS AREA RATIO TO DISP. CONSTRAINT RATIO MAIN0880
C              TO BE CONSIDERED IN DETERMINING NO. OF POTENTIALLY ACTIVE MAIN0890
C              DISPLACEMENT CONSTRAINTS                        MAIN0900
C*****MAIN0910
C          IDESN=0          MAIN0920
C          ICYCL=0          MAIN0930
C          ISCALF=0          MAIN0940
C          NMAXD=2          MAIN0950
C          WTMIN=.0F20      MAIN0960
C          IWTMIN=0         MAIN0970
C          READ(IR,100) NCYCL,NSCALF,KSCALF,DELTA,EPSIL,KPUNCH,KPRINT,KDISP,MAIN0980
C          1 OMEGA,ALPA     MAIN0990
C          IF(NSCALF.F0.0) NSCALF=3          MAIN1000
C          IF(DELTA.F0.0.0) DELTA=0.05       MAIN1010
C          IF(EPSIL.F0.0.0) EPSIL=0.1        MAIN1020
C          IF(OMEGA.F0.0.) OMEGA=0.8         MAIN1030
C          DELTA1=1.0-DELTA                  MAIN1040
C          DELTA2=1.0+DELTA                  MAIN1050
C          WRITE(IW,2001) NCYCL,KSCALF,DELTA,EPSIL,KDISP,OMEGA,ALPA MAIN1060
C*****MAIN1070
C-----DESIGN VARIABLE DATA---AOLD ON I1,AMIN ON I11          MAIN1080
C*****MAIN1090
C          M1=1          MAIN1100
C          N1=M1+NIUMDV   MAIN1110
C          N2=N1+NIUMDV   MAIN1120
C          N3=N2+NIUMDV   MAIN1130
C          IF(N3.GT.MTOT) CALL ERROR (N3-MTOT) MAIN1140
C          CALL DEVAR(A(M1),A(N1),A(N2),NIUMDV,I1,I11,IR,IW) MAIN1150
C*****MAIN1160
C-----NODE DATA---IN ARRAY STORED ON IR                      MAIN1170
C*****MAIN1180
C          N2=N1+6*NIUMNP MAIN1190

```

```

      N3=N2+NUMNP                                MAIN1200
      N4=N3+NUMNP                                MAIN1210
      N5=N4+NUMNP                                MAIN1220
      N6=N5+NUMNP                                MAIN1230
      IF(N6.GT.MT01) CALL FRRDR(N6-MT01)         MAIN1240
      CALL INPUTJ(A(N1),A(N2),A(N3),A(N4),A(N5),NUMNP,NEQ,IR,IR,IW) MAIN1250
C*****MAIN1260
C-----ELEMENT DATA --- UNIT STIFFNESS AND LOAD DATA ON I12    MAIN1270
C      UNIT STRESS RECOVERY DATA ON IR                                MAIN1280
C*****MAIN1290
      MRAND=0                                    MAIN1300
      NUMFL=0                                    MAIN1310
      RFWIND I12                                MAIN1320
      NBOUND=0                                    MAIN1330
      DO 900 M=1,NFLTYR                          MAIN1340
      READ(IR,1002) NPAR                          MAIN1350
      WRITE(IR)NPAR                              MAIN1360
      NUMFL=NUMFL+NPAR(2)                        MAIN1370
      MTYPE=NPAR(1)                              MAIN1380
      IF(MTYPE.EQ.7) NBOUND=NPAR(2)              MAIN1390
      900 CALL FLTYPE(A,MT01,MTYPE,IW)           MAIN1400
C*****MAIN1410
C-----WRITE UNIT WEIGHT ARRAY ON IR AND REARRANGE STORAGE OF ID  MAIN1420
C*****MAIN1430
      CALL UNITWT(A(M1),IR,NUMDV)                MAIN1440
      J=6*NUMNP                                  MAIN1450
      DO 121 I=1,J                                MAIN1460
      121 A(I)=A(NUMDV+I)                        MAIN1470
C*****MAIN1480
C-----ELEMENT LOAD MULTIPLIERS---STORED ON UNIT I11             MAIN1490
C*****MAIN1500
      N1=1                                        MAIN1510
      N2=N1+6*NUMNP                              MAIN1520
      CALL FLMULT(A(N2),LL,IR,IW,I11)            MAIN1530
      M=LL                                         MAIN1540
      IF(KDISP.FQ.0) GO TO 110                    MAIN1550
C*****MAIN1560
C-----READ IN DISPLACEMENT CONSTRAINTS AND WRITE ON UNIT I12    MAIN1570
C      CONSTRAINTS SHOULD END WITH ONE BLANK CARD                MAIN1580
C      IF NO DISPLACEMENT CONSTRAINTS,DO NOT LEAVE ANY BLANK CARDS MAIN1590
C*****MAIN1600
      N3=N2+12*LL                                MAIN1610
      MN=MT01-N3                                  MAIN1620
      CALL INPUTD(A(N1),A(N2),A(N3),MN,NUMNP,LL,LD,IR,IW,I12) MAIN1630
C*****MAIN1640
C-----NODAL LOADS AND MASSES -- STORED ON UNIT I11              MAIN1650
C*****MAIN1660
      IF(M.LT.NMAXD) M=NMAXD                     MAIN1670
      110 NFOR=(MT01-4*LL)/((MRAND+M)*4+1)        MAIN1680
      NRIOCK=(NFO-1)/NFOR +1                     MAIN1690
      IF (NFOR.GT.NFO) NFOR=NFO                  MAIN1700
      N3=N2+6*LL                                  MAIN1710
      N03=(N3-1)/2+1                             MAIN1720
      N4=(N03+NFOR*LL*2)*2                       MAIN1730
      IF(N4.GT.MT01) CALL FRRDR(N4-MT01)         MAIN1740
      CALL INL(A(N1),A(N2),AD(N03),              NUMNP,NFOR,LL,IR,IW,I11) MAIN1750
      WRITE (IW,2002)                             MAIN1760
      WRITE (IW,2003)NFO,MRAND,NFOR,NRIOCK        MAIN1770
      WRITE (IW,2002)                             MAIN1780
C*****MAIN1790

```



```

C-----FORM ELEMENT STIFFNESS AND LOAD VECTOR AND WRITE ON UNIT 12      MAIN1800
C*****MAIN1810
  995 N1=1      MAIN1820
    CALL FLSTIF (A(N1),NUMDV,NUMEL,I1,I2,I11,I12)      MAIN1830
C*****MAIN1840
C-----FORM STRUCTURAL STIFFNESS AND LOAD VECTORS AND WRITE ON UNIT 110  MAIN1850
C*****MAIN1860
  NE2R=2*NEOR      MAIN1870
  ND2=N1+NE2R*MBAND      MAIN1880
  ND4=ND2+NE2R *LL      MAIN1890
  N4=(ND4-1)*2+1      MAIN1900
  N5=N4+4*LL      MAIN1910
  IF(N5.GT.MTOT) CALL FRROR(N5-MTOT)      MAIN1920
  CALL ADDSTF(AD(N1),AD(ND2),      A(N4),NUMEL,NBLOCK,NE2R,LL,      MAIN1930
  1 MBAND,I2,I9,I10,I11)      MAIN1940
C*****MAIN1950
C-----SOLVE FOR DISPLACEMENT UNKNOWNNS      MAIN1960
C*****MAIN1970
  NSR=(MBAND+LL )*NEOR      MAIN1980
  N2=N1+NEOR      MAIN1990
  ND2=N2/2+1      MAIN2000
  ND3=ND2+NSR      MAIN2010
  CALL USOL (A(N1),AD(ND2),AD(ND3),NEOR,MBAND,LL,NBLOCK,NSR,I10,I3,MAIN2020
  1 I9,I2,IW)      MAIN2030
  IF(KDISP.EQ.0) GO TO 150      MAIN2040
C*****MAIN2050
C-----FIND OUT FOUR MAXIMUM DISPLACEMENT CONSTRAINT RATIOS      MAIN2060
C*****MAIN2070
  N2=N1+10      MAIN2080
  N3=N2+10*LL*2      MAIN2090
  ND3=N3/2+1      MAIN2100
  MN=(ND3+NEOR*LL-1)*2-MTOT      MAIN2110
  IF(MN.GT.0) CALL FRROR(MN)      MAIN2120
  CALL MAXD(A(N1),A(N2),AD(ND3),NEOR,LL,LD,NBLOCK,I2,I12,IW,NMAXD)      MAIN2130
C*****MAIN2140
C-----PRINT NODAL DISPLACEMENTS      MAIN2150
C*****MAIN2160
  150 N2=N1+NUMNP*6      MAIN2170
  ND2=N2/2+1      MAIN2180
  ND3=ND2+4*LL      MAIN2190
  WRITE(1W,2004)IDFSN      MAIN2200
  CALL PRINTD(A(N1),AD(ND2),AD(ND3),NEOR,NUMNP,LL,NBLOCK,NEQ,I2,18,      MAIN2210
  1 IW,KPRINT)      MAIN2220
C*****MAIN2230
C-----COMPUTE STRESSES AND CARRY OUT FULLY STRESSED DESIGN      MAIN2240
C*****MAIN2250
  M1=1      MAIN2260
  M2=M1+NUMDV      MAIN2270
  M3=M2+NUMDV      MAIN2280
  N1=M3+NUMDV      MAIN2290
  N2=N1+4*LL      MAIN2300
  ND2=N2/2+1      MAIN2310
  N3=(ND2-1+NEOR*LL)*2+1      MAIN2320
  LR=(MTOT-N3)/NEO      MAIN2330
  IF (LR.GE.1) GO TO 31      MAIN2340
  MM=NEO+N3      MAIN2350
  CALL FRROR (MM-MTOT)      MAIN2360
  31 IF(LR.GT.LL)LR=LL      MAIN2370
  CALL STRESS(A(M1),A(M2),A(M3),A(N1),AD(ND2),A(N3),LL,LR,NEO,NUMDV,      MAIN2380
  1 NEOR,A,MTOT,I1,I2,I8,I11,IW)      MAIN2390

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C*****MAIN2400
C-----EVALUATE CURRENT DESIGN AND PERFORM REDESIGN          MAIN2410
C*****MAIN2420
      IF (NCYCL.F0.0) GO TO 996                                MAIN2430
      M4=M3+NUMDV                                              MAIN2440
      CALL DESIGN(A(M1),A(M2),A(M3),A(M4),NUMDV,I1,I2,I11,IW,IP)  MAIN2450
      IDFSM=IDFSM+1                                           MAIN2460
      IF (KONVG.F0.4) GO TO 996                                MAIN2470
      IF (NDISP.F0.0) GO TO 995                                MAIN2480
C*****MAIN2490
C-----CALCULATE DISPLACEMENT DERIVATIVES                    MAIN2500
C*****MAIN2510
      MTOT2= MTOT/2                                           MAIN2520
      CALL DDERV( A,AD,MTOT,MTOT2,NBOUND)                     MAIN2530
C*****MAIN2540
C-----CARRY OUT DISPLACEMENT REDESIGN                        MAIN2550
C*****MAIN2560
      M1=1                                                     MAIN2570
      M2=M1+NUMDV+NDISP                                         MAIN2580
      M3=M2+NUMDV                                              MAIN2590
      M4=M3+NUMDV                                              MAIN2600
      M5=M4+NUMDV                                              MAIN2610
      M6=M5+NUMDV                                              MAIN2620
      M7=M6+NUMDV                                              MAIN2630
      MM=M7+NUMDV-MTOT                                         MAIN2640
      CALL DESIN(A(M1),A(M2),A(M3),A(M4),A(M5),A(M6),A(M7),NUMDV,NDISP,  MAIN2650
      1 I1,I3,I2,IW)                                           MAIN2660
      IF (KONVG.F0.4) GO TO 995                                MAIN2670
996  STOP                                                     MAIN2680
1000 FORMAT(20A4/6I5)                                         MAIN2690
1001 FORMAT(3I5,2F10.0,3I5,2F10.5)                            MAIN2700
1002 FORMAT (14I5)                                             MAIN2710
2000 FORMAT(1H1,20A4//
      . 28H NUMBER OF NODAL POINTS = ,I5/
      . 28H NUMBER OF ELEMENT TYPES = ,I5/
      . 28H NUMBER OF LOAD CASES = ,I5/
      . 28H NUMBER OF DES. VARIABLES = ,I5 )
2001 FORMAT(// 22H DESIGN CONTROL DATA //
      1 9H NCYCL = ,I5/
      2 9H KSCALE = ,I5/
      3 9H DELTA = ,F12.4/
      4 9H EPSIL = ,F12.4/
      5 9H KDISP = ,I5/
      6 9H OMEGA = ,F10.5/
      7 9H ALPA = ,F10.5 )
2002 FORMAT(//
2003 FORMAT(34H TOTAL NUMBER OF EQUATIONS = ,I5,
      1 /34H RANDWIDTH = ,I5,
      2 /34H NUMBER OF EQUATIONS IN A BLOCK = ,I5,
      3 /34H NUMBER OF BLOCKS = ,I5)
2004 FORMAT(31H1*****//
      1 26H ANALYSIS OF DESIGN NUMBER,14 /
      2 31H *****//)
      FND
      MAIN2930

```

```

      SUBROUTINE INPUT, I( ID, X, Y, Z, T, NUMNP, NFO, IAR, IR, IW)
C*****MAIN2950
C-----READ OR GENERATE NODAL POINT DATA
C*****MAIN2960
      DIMENSION X(NUMNP), Y(NUMNP), Z(NUMNP), ID(NUMNP, 6), T(NUMNP)
      READ(1, 1)
      WRITE(IW, 2000)
      WRITE(IW, 2001)
      NFO=0
      10 READ (1, 1000) N, ( ID(N, I), I=1, 6), X(N), Y(N), Z(N), KN, T(N)
      WRITE(IW, 2002) N, ( ID(N, I), I=1, 6), X(N), Y(N), Z(N), KN, T(N)
C*****MAIN3050
C-----CHECK IF GENERATION IS REQUIRED
C*****MAIN3060
      IF(NFO, F0, 0) GO TO 50
      DO 20 I=1, 6
      IF( ID(N, I), F0, 0, AND, ID(NFO, I), LT, 0) ID(N, I)=ID(NFO, I)
      20 CONTINUE
      IF(KN, F0, 0) GO TO 50
      NIUM=(N-NFO)/KN
      NIUM=NIUM-1
      IF(NIUM, LT, 1) GO TO 50
      XNIUM=NIUM
      DX=(X(N)-X(NFO))/XNIUM
      DY=(Y(N)-Y(NFO))/XNIUM
      DZ=(Z(N)-Z(NFO))/XNIUM
      DT=(T(N)-T(NFO))/XNIUM
      K=NFO
      DO 30 I=1, NIUM
      KK=K
      K=K+KN
      X(K)=X(KK)+DX
      Y(K)=Y(KK)+DY
      Z(K)=Z(KK)+DZ
      T(K)=T(KK)+DT
      DO 30 I=1, 6
      ID(K, I)=ID(KK, I)
      IF ( ID(K, I), GT, 1) ID(K, I)=ID(KK, I)+KN
      30 CONTINUE
      50 NFO=N
      IF(N, NF, NUMNP) GO TO 10
C*****MAIN3350
C-----PRINT ALL NODAL POINT DATA
C*****MAIN3360
      WRITE (IW, 2003)
      WRITE (IW, 2001)
      WRITE (IW, 2005) (N, (ID(N, I), I=1, 6), X(N), Y(N), Z(N), T(N), N=1, NUMNP)
C*****MAIN3410
C-----NUMBER UNKNOWN AND SET MASTER NODES NEGATIVE
C*****MAIN3420
      NFO=0
      DO 60 N=1, NUMNP
      DO 60 I=1, 6
      ID(N, I)=1ABS( ID(N, I))
      IF( ID(N, I)-1) 57, 58, 59
      57 NFO=NFO+1
      ID(N, I)=NFO
      GO TO 60
      58 ID(N, I)=0
      GO TO 60
      59

```

```

      MAIN2940
      MAIN2950
      MAIN2960
      MAIN2970
      MAIN2980
      MAIN2990
      MAIN3000
      MAIN3010
      MAIN3020
      MAIN3030
      MAIN3040
      MAIN3050
      MAIN3060
      MAIN3070
      MAIN3080
      MAIN3090
      MAIN3100
      MAIN3110
      MAIN3120
      MAIN3130
      MAIN3140
      MAIN3150
      MAIN3160
      MAIN3170
      MAIN3180
      MAIN3190
      MAIN3200
      MAIN3210
      MAIN3220
      MAIN3230
      MAIN3240
      MAIN3250
      MAIN3260
      MAIN3270
      MAIN3280
      MAIN3290
      MAIN3300
      MAIN3310
      MAIN3320
      MAIN3330
      MAIN3340
      MAIN3350
      MAIN3360
      MAIN3370
      MAIN3380
      MAIN3390
      MAIN3400
      MAIN3410
      MAIN3420
      MAIN3430
      MAIN3440
      MAIN3450
      MAIN3460
      MAIN3470
      MAIN3480
      MAIN3490
      MAIN3500
      MAIN3510
      MAIN3520
      MAIN3530

```

59 ID(N,I)=-ID(N,I)	MAIN3540
60 CONTINUE	MAIN3550
WRITE(IW,2004) (N,(ID(N,I),I=1,6),N=1,NUMNP)	MAIN3560
WRITE(I8) ID	MAIN3570
RETURN	MAIN3580
1000 FORMAT (7I5,3F10.0,15,F10.0)	MAIN3590
2000 FORMAT(// 23H NODAL POINT INPUT DATA)	MAIN3600
2001 FORMAT (5HONNDF,3X,24HBOUNDARY CONDITION CODES,3X,	MAIN3610
139H/-----NODAL POINT COORDINATES-----//,	MAIN3620
27H NUMBER,2X,1HX,4X,1HY,4X,1HZ,3X,2HXX,3X,2HYY,3X,2HZZ,12X,	MAIN3630
31HX,12X,1HY,12X,1HZ,12X,1H1//)	MAIN3640
2002 FORMAT (15,6I5,3F13.3,15,F13.3)	MAIN3650
2003 FORMAT (// 21H GENERATED NODAL DATA)	MAIN3660
2004 FORMAT (// 17H EQUATION NUMBERS//	MAIN3670
1 35H N X Y Z XX YY 27 / (7I5))	MAIN3680
2005 FORMAT (15,6I5,4F13.3)	MAIN3690
END	MAIN3700
SUBROUTINE DEVAR(IJW,ANLD,AMIN,NQVAR,I1,I1),IR,IW)	MAIN3710
C*****	MAIN3720
C-----READ OR GENERATE DESIGN VARIABLE DATA	MAIN3730
C*****	MAIN3740
DIMENSION ANLD(NQVAR),AMIN(NQVAR),IJW(NQVAR)	MAIN3750
REWIND I1	MAIN3760
REWIND I11	MAIN3770
NQLD=0	MAIN3780
WRITE (IW,100)	MAIN3790
9 READ(IR,101)N,ANLD(N),AMIN(N)	MAIN3800
NN=N-1	MAIN3810
IF(NN.EQ.NQLD)GO TO 11	MAIN3820
KK=NQLD+1	MAIN3830
DO 10 I=KK,NN	MAIN3840
ANLD(I)=ANLD(N)	MAIN3850
10 AMIN(I)=AMIN(N)	MAIN3860
11 NQLD=N	MAIN3870
IF(N.LT.NQVAR)GO TO 9	MAIN3880
DO 13 N=1,NQVAR	MAIN3890
IJW(N)=0.	MAIN3900
IF(ANLD(N).LT.AMIN(N))ANLD(N)=AMIN(N)	MAIN3910
13 WRITE(IW,102)N,ANLD(N),AMIN(N)	MAIN3920
WRITE (I1) ANLD	MAIN3930
WRITE(I11) AMIN	MAIN3940
RETURN	MAIN3950
100 FORMAT(// 35H DESIGN VARIABLE INPUT DATA //	MAIN3960
1 33H DESIGN /	MAIN3970
2 35H VARIABLE INITIAL MIN ALLOWABLE/	MAIN3980
3 35H NUMBER VALUE VALUE //	MAIN3990
101 FORMAT(15,2F10.0)	MAIN4000
102 FORMAT(16,2X,2F13.4)	MAIN4010
END	MAIN4020

```

      SUBROUTINE FLTYPE (A,MTOT,MTYPE,IW)
      *****MAIN4030
C-----CALL APPROPRIATE ELEMENT SUBROUTINE TO DEVELOP ELEMENT MATRICES
      *****MAIN4040
      DIMENSION A(MTOT)
      *****MAIN4070
      GO TO (1,2,3,4,5,6,7,8),MTYPE
      *****MAIN4080
C-----THREE DIMENSIONAL TRUSS ELEMENTS
      *****MAIN4100
      1 CALL TRUSS (A,MTOT)
      *****MAIN4120
      GO TO 900
      *****MAIN4130
C-----THREE DIMENSIONAL BEAM ELEMENTS
      *****MAIN4140
      2 CALL BEAM (A,MTOT)
      *****MAIN4160
      GO TO 900
      *****MAIN4180
C-----PLANE STRESS ELEMENTS
      *****MAIN4190
      3 CALL PLANE (A,MTOT)
      *****MAIN4220
      GO TO 900
      *****MAIN4230
C-----SHEAR PANEL ELEMENTS
      *****MAIN4240
      4 CALL SHEAR (A,MTOT)
      *****MAIN4250
      GO TO 900
      *****MAIN4260
C-----PROVISION FOR OTHER TYPES OF ELEMENTS
      *****MAIN4280
      5 CALL NOELEM(MTYPE,0,IW)
      *****MAIN4290
      GO TO 900
      *****MAIN4300
C-----PLATE/SHELL ELEMENTS
      *****MAIN4310
      6 CALL SHELL (A,MTOT)
      *****MAIN4330
      GO TO 900
      *****MAIN4340
C-----BOUNDARY ELEMENTS
      *****MAIN4350
      7 CALL BOUND (A,MTOT)
      *****MAIN4360
      GO TO 900
      *****MAIN4370
C-----PROVISION FOR OTHER TYPES OF ELEMENTS
      *****MAIN4380
      8 CALL NOELEM(MTYPE,0,IW)
      *****MAIN4390
      900 RETURN
      *****MAIN4400
      FND
      *****MAIN4490

      SUBROUTINE NOELEM (MTYPE,KODE,IW)
      *****MAIN4500
C-----PRINT THE MESSAGE THAT REQUIRED ELEMENT SUBROUTINE IS MISSING
      *****MAIN4510
      WRITE (IW,100) MTYPE
      *****MAIN4520
      IF (KODE.NE.0) WRITE (IW,101) KODE
      *****MAIN4530
      STOP
      *****MAIN4540
      100 FORMAT (//46H THE FOLLOWING ELEMENT HAS NOT BEEN PROGRAMED:
      *****MAIN4550
      1 14H ELEMENT TYPE=,I2)
      *****MAIN4560
      101 FORMAT( 14H CONSTR CODE=,I2)
      *****MAIN4570
      FND
      *****MAIN4580

```

```

      SUBROUTINE UNITWT(UWT,IR,NUMDV)
      C*****
      C-----WRITE UNIT WEIGHT ON TAPE IR
      C*****
      DIMENSION UWT(NUMDV)
      WRITE(IR)UWT
      RETURN
      END
      MAIN4610
      MAIN4620
      MAIN4630
      MAIN4640
      MAIN4650
      MAIN4660
      MAIN4670
      MAIN4680

```

```

      SUBROUTINE ELMULT(STR,LL,IR,IW,I11)
      C*****
      C-----READ IN STRUCTURE LOAD MULTIPLIERS
      C*****
      DIMENSION STR(4,LL)
      WRITE(IW,2000)
      DO 50 L=1,LL
      READ(IR,1002) (STR(I,L),I=1,4)
      50 WRITE(IW,2002) L,(STR(I,L),I=1,4)
      WRITE(I11) STR
      RETURN
      1002 FORMAT (4F10.0)
      2000 FORMAT(/10H STRUCTURE,12X,26HSTRUCTURE LOAD MULTIPLIERS/
      . 10H LOAD CASE,9X,1HA,9X,1HB,9X,1HC,9X,1HD/)
      2002 FORMAT (16,7X,4F10.3)
      END
      MAIN4690
      MAIN4700
      MAIN4710
      MAIN4720
      MAIN4730
      MAIN4740
      MAIN4750
      MAIN4760
      MAIN4770
      MAIN4780
      MAIN4790
      MAIN4800
      MAIN4810
      MAIN4820
      MAIN4830
      MAIN4840

```

```

      SUBROUTINE INTERP(F,FF,NUMTC,NUMMAT,NUM1,NUM2,NT,MAT,TFMP)
      C*****
      C-----INTERPOLATES MATERIAL PROPERTIES FOR AVERAGE ELEMENT TEMPERATURE
      C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*4 F
      DIMENSION F(NUMTC,NUM1,NUMMAT),FF(NUM2)
      IF(NT.NF.1) GO TO 220
      DO 210 KK=1,NUM2
      FF(KK)=F(1,KK+1,MAT)
      GO TO 260
      220 DO 230 I=2,NT
      II=I
      T1=F(I-1,1,MAT)
      T2=F(I,1,MAT)
      IF(T2.GF.TFMP) GO TO 240
      230 CONTINUE
      RI=(T2-TFMP)/(T2-T1)
      RJ=(TFMP-T1)/(T2-T1)
      DO 250 KK=1,NUM2
      FF(KK)=F(II-1,KK+1,MAT)*RI+F(II,KK+1,MAT)*RJ
      260 RETURN
      END
      MAIN4850
      MAIN4860
      MAIN4870
      MAIN4880
      MAIN4890
      MAIN4900
      MAIN4910
      MAIN4920
      MAIN4930
      MAIN4940
      MAIN4950
      MAIN4960
      MAIN4970
      MAIN4980
      MAIN4990
      MAIN5000
      MAIN5010
      MAIN5020
      MAIN5030
      MAIN5040
      MAIN5050
      MAIN5060
      MAIN5070

```

```

      SUBROUTINE CALBAN(NDIF,LM,S,P,ST,TT,NIJ,NV,NS,ND,NW,IDVAR,IFX,FRC) MAIN5080
C*****MAIN5090
C-----CALCULATE BANDWIDTH OF STRUCTURE STIFFNESS MATRIX MAIN5100
C-----WRITE UNIT STRESS RECOVERY MATRICES AND STRESS-CORRECTION MATRICES MAIN5110
C      ON TAPE 18 MAIN5120
C-----WRITE UNIT STIFFNESS AND LOAD VECTOR ON TAPE 12 MAIN5130
C*****MAIN5140
      IMPLCIT REAL*8 (A-H,O-Z) MAIN5150
      REAL*4 FRC MAIN5160
      DIMENSION LM(MD),S(MD,ND,NIJ),P(MD,4,NV),ST(NS,ND,NIJ),TT(NS,4,NW) MAIN5170
      I,IS(6) MAIN5180
      COMMON/ELPAR/NPAR(14),NUMNP,MRAND,IFLP(17) MAIN5190
      COMMON/INITTS/IR,IW,IP,I1,I2,I3,I8,I9,I10,I11,I12 MAIN5200
      MTN=100000 MAIN5210
      MAY=0 MAIN5220
      DO 800 I=1,MD MAIN5230
        IF (LM(I).EQ.0) GO TO 800 MAIN5240
        IF (LM(I).GT.MAX) MAX=LM(I) MAIN5250
        IF (LM(I).LT.MTN) MTN=LM(I) MAIN5260
      800 CONTINUE MAIN5270
      NDIF=MAX-MIN+1 MAIN5280
      IF (NDIF.GT.MRAND) MRAND=NDIF MAIN5290
      IIR=6+ND*(1+NIJ*NIJ)+NV*4 MAIN5300
      IS(1)=NIJ MAIN5310
      IS(2)=NW MAIN5320
      IS(3)=NS MAIN5330
      IS(4)=ND MAIN5340
      IS(5)=IDVAR MAIN5350
      IS(6)=IFX MAIN5360
      WRITE(JR) IS,FRC,LM,S,TT MAIN5370
      IS(1)=IIR MAIN5380
      IS(2)=NIJ MAIN5390
      IS(3)=NV MAIN5400
      IS(4)=ND MAIN5410
      WRITE(I12) IS,FRC,LM,S,P MAIN5420
      RETURN MAIN5430
      END MAIN5440

```

```

      SUBROUTINE REARRAN(S,SS,NM1,NM2,NM3,N1,N2,N3,NN) MAIN5450
C*****MAIN5460
C-----REARRANGE MATRIX S MAIN5470
C*****MAIN5480
      IMPLCIT REAL*8 (A-H,O-Z) MAIN5490
      DIMENSION S(NM1,NM2,NM3),SS(NN) MAIN5500
      IT=0 MAIN5510
      DO 10 K=1,N3 MAIN5520
        DO 10 J=1,N2 MAIN5530
          DO 11 I=1,N1 MAIN5540
            11 SS(I+I)=S(I,J,K) MAIN5550
          10 JJ=JJ+1 MAIN5560
        10 RETURN MAIN5570
      END MAIN5580

```

```

SUBROUTINE VECTOR(V,XI,YI,ZI,XJ,YJ,ZJ)
C*****
C-----CALCULATE COMPONENTS OF A VECTOR
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION V(4)
      X=XI-XJ
      Y=YI-YJ
      Z=ZJ-ZI
      V(4)=DSORT(X*X+Y*Y+Z*Z)
      V(3)=Z/V(4)
      V(2)=Y/V(4)
      V(1)=X/V(4)
      RETURN
      END

```

```

MAIN5590
MAIN5600
MAIN5610
MAIN5620
MAIN5630
MAIN5640
MAIN5650
MAIN5660
MAIN5670
MAIN5680
MAIN5690
MAIN5700
MAIN5710
MAIN5720
MAIN5730

```

```

SUBROUTINE CROSS(A,R,C)
C*****
C-----CROSS PRODUCT OF TWO VECTORS
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION A(4),R(4),C(4)
      X=A(2)*R(3)-A(3)*R(2)
      Y=A(3)*R(1)-A(1)*R(3)
      Z=A(1)*R(2)-A(2)*R(1)
      C(4)=DSORT(X*X+Y*Y+Z*Z)
      C(3)=Z/C(4)
      C(2)=Y/C(4)
      C(1)=X/C(4)
      RETURN
      END

```

```

MAIN5740
MAIN5750
MAIN5760
MAIN5770
MAIN5780
MAIN5790
MAIN5800
MAIN5810
MAIN5820
MAIN5830
MAIN5840
MAIN5850
MAIN5860
MAIN5870
MAIN5880

```

```

REAL FUNCTION DOT*8 (A,R)
C*****
C-----DOT PRODUCT OF TWO VECTORS
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION A(4),R(4)
      DOT=A(1)*R(1)+A(2)*R(2)+A(3)*R(3)
      RETURN
      END

```

```

MAIN5890
MAIN5900
MAIN5910
MAIN5920
MAIN5930
MAIN5940
MAIN5950
MAIN5960
MAIN5970

```

```

SUBROUTINE ERROR(N)
C*****
C-----PRINT STORAGE EXCEEDED MESSAGE
C*****
      COMMON/UNITS/ IR,IW,IP,II,I2,I3,IR,I9,I10,I11,I12
      WRITE (IW,2000) N
2000 FORMAT (// 'STORAGE EXCEEDED BY ',I6)
      STOP
      END

```

```

MAIN5980
MAIN5990
MAIN6000
MAIN6010
MAIN6020
MAIN6030
MAIN6040
MAIN6050
MAIN6060

```



```

      SUBROUTINE INPUTD ( ID, TR, DCNN,M,NUMNP,LL,LD,IR,IW,I12)          MAIN6070
C*****MAIN6080
C-----READ DISPLACEMENT CONSTRAINTS AND SET UP DISP. CONSTS. TABLE  MAIN6090
C*****MAIN6100
      DIMENSION ID(NUMNP,6),TR(LL,12),DCNN(M)          MAIN6110
      COMMON/JUNK/ R(12),JUNK1(288)          MAIN6120
      COMMON/FM/ I0D(5066)          MAIN6130
      WRITE(IW,3001)          MAIN6140
      LD=0          MAIN6150
      NC=0          MAIN6160
      LRD=0          MAIN6170
      DO 851 I=1,LL          MAIN6180
      DO 851 J=1,12          MAIN6190
851  TR(I,J)=0.0          MAIN6200
      DO 900 NN=1,NUMNP          MAIN6210
      IF(NN.EQ.1)GO TO 300          MAIN6220
150  IF(N.NF.NN) GO TO 400          MAIN6230
      DO 200 I=1,6          MAIN6240
      TR(I,I)= ABS(R(I))          MAIN6250
200  TR(I,I+6)=-ABS(R(I+6))          MAIN6260
      NC=1          MAIN6270
300  READ(IR,1001)N,L,R          MAIN6280
      GO TO 150          MAIN6290
400  IF(NC.EQ.0) GO TO 900          MAIN6300
      NC=0          MAIN6310
      DO 800 J=1,6          MAIN6320
      DO 70 I=1,LL          MAIN6330
      IF(TR(I,J).NF.0..OR.TR(I,J+6).NF.0) GO TO 80          MAIN6340
70  CONTINUE          MAIN6350
      GO TO 810          MAIN6360
80  II=I0(NN,I)          MAIN6370
      IF(II) 810,810,830          MAIN6380
830  LD=LD+1          MAIN6390
      I0D(LD)=II          MAIN6400
      DO 30 J=1,LL          MAIN6410
      DCNN(LRD+LL+I)=TR(I,J+6)          MAIN6420
30  DCNN(LRD+I)=TR(I,J)          MAIN6430
      LRD=LRD+2*LL          MAIN6440
      GO TO 800          MAIN6450
810  DO 815 I=1,LL          MAIN6460
      TR(I,J)=0.          MAIN6470
815  TR(I,J+6)=0.          MAIN6480
800  CONTINUE          MAIN6490
      WRITE(IW,2001) (NN,I,(TR(I,J),J=1,12),I=1,LL)          MAIN6500
      DO 850 I=1,LL          MAIN6510
      DO 850 J=1,12          MAIN6520
850  TR(I,J)=0.0          MAIN6530
900  CONTINUE          MAIN6540
      M1=LD*2*I1-M          MAIN6550
      IF(MT.GT.0) CALL FRROR(MT)          MAIN6560
      WRITE(I12) (I0D(I),I=1,LD), (DCNN(I),I=1,LRD)          MAIN6570
      RETURN          MAIN6580
1001  FORMAT(2I4,12F6.5)          MAIN6590
2001  FORMAT(1X,2I5,12F10.5)          MAIN6600
3001  FORMAT(/41H NODAL DISPLACEMENT/ROTATION CONSTRAINTS//          MAIN6610
112H NODL LOAD ,119H/-----MAX,ALL          MAIN6620
20WABLE DISPLACEMENTS AND ROTATIONS-----          MAIN6630
3-----//,13H NO. CASE ,4X,2HDX,4X,2HDX,          MAIN6640
4RX,2HDX,4X,2HDX,4X,2HDX,4X,2HDX,4X,2HDX,4X,2HDX,4X,2HDX,4X,2HDX,          MAIN6650
53H-RX,7X,3H-RY,7X,3H-RZ)          MAIN6660

```

FMD

MAIN6670

```

SUBROUTINE INL (ID,TR,R,NIUMNP,NFOR,LL,IR,IW,I11)
C*****
C-----INPUT NODAL LOADS
C*****
      REAL*8 R(NFOR,LL)
      DIMENSION ID(NIUMNP,6),TR(6,LL)
      COMMON/JUNK/R(6),JUN(294)
      KSHF=0
      WRITE (IW,2002)
      DO 750 I=1,NFOR
      DO 750 K=1,LL
750  R(I,K)=0.0
      DO 900 NN=1,NIUMNP
      DO 100 I=1,6
      DO 100 J=1,LL
100  TR(I,J)=0.0
      IF(NN.FO.1) GO TO 300
150  IF(N.NE.NN) GO TO 400
      DO 200 I=1,6
200  TR(I,I)=R(I)
300  READ (IR,1001) N,L,R
      IF (N.FO.0) GO TO 150
      WRITE(IW,2001) N,L,R
      GO TO 150
400  DO 800 J=1,6
      II=ID(NN,J)-KSHF
      IF (II) 800,800,500
500  DO 600 K=1,LL
600  R(II,K)=TR(J,K)
610  IF(II.NF.NFOR) GO TO 800
      WRITE(I11) R
      KSHF=KSHF+NFOR
      DO 700 I=1,NFOR
      DO 700 K=1,LL
700  R(I,K)=0.0
800  CONTINUE
900  CONTINUE
      WRITE(I11) R
      RETURN
1001 FORMAT (2I5,7F10.4)
2001 FORMAT (2I5,6F13.3)
2002 FORMAT(/18H NODAL POINT LOADS // 10H NODE LOAD,23X
. 14HAPPLIED LOADS / 10H NO. CASE ,9X, 2HRX, 11X,
. 2HRX,11X,2HRZ,11X,2HMX,11X,2HMY,11X,2HMZ 1
      FMD

```

```

MAIN6680
MAIN6690
MAIN6700
MAIN6710
MAIN6720
MAIN6730
MAIN6740
MAIN6750
MAIN6760
MAIN6770
MAIN6780
MAIN6790
MAIN6800
MAIN6810
MAIN6820
MAIN6830
MAIN6840
MAIN6850
MAIN6860
MAIN6870
MAIN6880
MAIN6890
MAIN6900
MAIN6910
MAIN6920
MAIN6930
MAIN6940
MAIN6950
MAIN6960
MAIN6970
MAIN6980
MAIN6990
MAIN7000
MAIN7010
MAIN7020
MAIN7030
MAIN7040
MAIN7050
MAIN7060
MAIN7070
MAIN7080
MAIN7090
MAIN7100
MAIN7110
MAIN7120

```

```

      SUBROUTINE FLSTIF (AOLD,NUMDV,NUMEL,I1,I2,I11,I12)          MAIN7130
C*****MAIN7140
C-----FORM ELEMENT STIFFNESS FROM UNIT STIFFNESS MATRICES    MAIN7150
C*****MAIN7160
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*4 AOLD,FRC
      DIMENSION AOLD (NUMDV),S1(24,24),S2(24,24),P1(24,4),P2(24,4)
      COMMON/EM/LM(24),S(24,24,2),P(24,4,2),EM1(1177)
      EQUIVALENCE (S1,S),(S2,S(577)),(P1,P),(P2,P(97))
      RFWIND I1
      RFWIND I2
      RFWIND I11
      RFWIND I12
      READ(I1) AOLD
      DO 100 N=1,NUMEL
      READ(I12) LRD,NU,NV,ND,INVAR,IFX,FRC,(LM(I),I=1,ND),((S(I,J,K),
1 I=1,ND),J=1,ND),K=1,NU),((P(I,J,K),I=1,ND),J=1,4),K=1,NV)
      IF(INVAR.FO.O) GO TO 106
      AREA=AOLD(INVAR)*FRC
      XINERT=AREA**IFX
      DO 101 I=1,ND
      DO 102 J=1,4
102 P1(I,J)=P1(I,J)*AREA
      DO 101 J=1,ND
101 S1(I,J)=S1(I,J)*AREA
      IF(NU.FO.1) GO TO 105
      DO 104 I=1,ND
      DO 104 J=1,ND
104 S1(I,J)=S1(I,J)+S2(I,J)*XINERT
105 IF(NV.FO.1) GO TO 106
      DO 107 I=1,ND
      DO 107 J=1,4
107 P1(I,J)=P1(I,J)+P2(I,J)
106 LRD=ND*(ND+4)
      NN=ND*ND
      CALL REARAN(S1,S1,24,24,1,ND,ND,],NN)
      NN=ND*4
      CALL REARAN(P1,P1,24,4,1,ND,4,1,NN)
      CALL FLSTFW(LRD,ND,LM,S1,P1,I2)
100 CONTINUE
C*****MAIN7530
C-----READ AMIN TO ADVANCE UNIT I1 TO NEXT RECORD : STR    MAIN7540
C*****MAIN7550
      READ (I11) AOLD
      RETURN
      END
      MAIN7560
      MAIN7570
      MAIN7580

```

```

      SUBROUTINE FLSTFW(LRD,ND,LM,S1,P1,I2)          MAIN7590
C*****MAIN7600
C-----WRITE ELEMENT STIFFNESSES ON TAPE I2          MAIN7610
C*****MAIN7620
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION LM(ND),S1(ND,ND),P1(ND,4)
      WRITE(I2) LRD,ND,LM,S1,P1
      RETURN
      END
      MAIN7630
      MAIN7640
      MAIN7650
      MAIN7660
      MAIN7670

```

```

      SUBROUTINE ADDSTF(A,R,STR,NUMFL,NBLOCK,NF2R,LL,MRAND,I2,I9,I10,      MAIN7680
      I I11)                                                                MAIN7690
C-----FORMS GLOBAL EQUILIBRIUM FORMATIONS IN BLOCKS                      MAIN7710
C-----FORM EQUATIONS IN BLOCKS { TWO BLOCKS AT A TIME }                 MAIN7910
C-----DETERMINE IF STIFFNESS IS TO BE PLACED ON UNIT I9                MAIN8270

      REAL*8 A(NF2R,MRAND),R(NF2R,LL),SS
      DIMENSION STR(4,LL)
      COMMON /FM/ LRD,ND,LM(24),SS(672),FM1(3696)
      NFOR=NF2R/2
      K=NFOR+1
      X=NBLOCK
      MR=SORT(X)
      MR=MR/2+1
      NFRR=MR*NF2R
      MM=1
      NUMQ=0
      NSHIFT=0
      RFWIND I10
C-----READ STRUCTURE LOAD MULTIPLIERS                                  MAIN7870
C-----READ (I11) STR                                                    MAIN7890
C-----FORM EQUATIONS IN BLOCKS { TWO BLOCKS AT A TIME }                 MAIN7910
C-----DETERMINE IF STIFFNESS IS TO BE PLACED ON UNIT I9                MAIN8270

      DO 1000 M=1,NBLOCK,2
      DO 100 I=1,NF2R
      DO 100 J=1,MRAND
      100 A(I,J)=0.
      READ(I11)((R(I,L),I=1,NFOR),L=1,LL)
      IF (M.FO.NBLOCK) GO TO 200
      READ(I11)((R(I,L),I=K,NF2R),L=1,LL)
      200 CONTINUE
      RFWIND I9
      RFWIND I2
      MA=I9
      NUMF=NUMQ
      IF (MM,NF,1) GO TO 75
      MA=I2
      NUMF=NUMFL
      NUMQ=0
      75 DO 700 N=1,NUMF
      READ(MA) LRD,ND,(LM(I),I=1,ND),(SS(I),I=1,LRD)
      DO 600 I=1,ND
      LMM=1-LM(I)
      II=LM(I)-NSHIFT
      IF (II,LF,0,OR,II.GT,NF2R) GO TO 600
      DO 300 L=1,LL
      DO 300 J=1,4
      KK=ND*(ND+J-1)
      300 R(I,L)=R(I,L)+SS(I+KK)*STR(J,L)
      DO 500 J=1,ND
      JJ=LM(J)+LMM
      IF(J,J) 500,500,390
      390 KK=ND*(J-ND)
      400 A(I,J,J)=A(I,J,J)+SS(I+KK)
      500 CONTINUE
      600 CONTINUE
C-----DETERMINE IF STIFFNESS IS TO BE PLACED ON UNIT I9

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C*****MAINR280
      IF (MM.GT.1) GO TO 700                                MAINR290
      DO 650 I=1,ND                                          MAINR300
      II=LM(I) -NSHIFT                                       MAINR310
      IF (II.GT.NF2B.AND.II.LE.NERR) GO TO 660             MAINR320
650 CONTINUE                                                MAINR330
      GO TO 700                                              MAINR340
660 WRITE(19) LRD,ND,(LM(I),I=1,ND),(SS(I),I=1,LRD)      MAINR350
      NIM9=NIM9+1                                           MAINR360
700 CONTINUE                                                MAINR370
      WRITE (110) ((A(I,J),I=1,NFOR),J=1,MRAND),((B(I,L),I=1,NFOR),L=1,MAINR380
      LL)                                                    MAINR390
      IF(M.FO.NRLNCK) GO TO 1000                            MAINR400
      WRITE(110) ((A(I,J),I=K,NF2B),J=1,MRAND),((B(I,L),I=K,NE2B),L=1,LL,MAINR410
1)                                                         MAINR420
      IF (MM.FO.MR) MM=0                                     MAINR430
      MM=MM+1                                                MAINR440
1000 NSHIFT=NSHIFT+NF2B                                     MAINR450
      RETURN                                                MAINR460
      END                                                    MAINR470

      SUBROUTINE USOL (MAXR,A,R,NFOR,MR,LL,NRLNCK,NSR,NORG,NRKS,NT1,    MAINR480
1 NT2,IW)                                                  MAINR490
C*****MAINR500
C-----THIS SUBPROGRAM SOLVES SIMULTANEOUS EQUATIONS FOR DISPLACEMENTS MAINR510
C-----TAPES USED ARE AS FOLLOW                               MAINR520
C-----A AND R (TWO BLOCKS OF STRUCTURAL STIFFNESS AND LOAD VECTORS) ARE MAINR530
C      STORED ON TAPE NORG                                  MAINR540
C-----SCRATCH ON NRKS , NT1 , NT2                         MAINR550
C-----RESULTS ON TAPE NT2                                 MAINR560
C*****MAINR570
      DIMENS(ON MAXR(NFOR)                                  MAINR580
      REAL*8 A(NSR),R(NSR)                                  MAINR590
      NC=MR+LL                                               MAINR600
      NRR=(MR-1)/NFOR+1                                     MAINR610
      JNC=NFOR-1                                           MAINR620
      NMR=NFOR*MR                                           MAINR630
      NT=NT2                                                MAINR640
      NJ=NT1                                                MAINR650
      REWIND NORG                                           MAINR660
      REWIND NRKS                                           MAINR670
C*****MAINR680
C-----REDUCE EQUATIONS BLOCK-BY-BLOCK                     MAINR690
C*****MAINR700
      DO 900 N=1,NRLNCK                                     MAINR710
      IF (N.GT.1.AND.NRR.FO.1) GO TO 110                   MAINR720
      IF (NRR.FO.1) GO TO 105                               MAINR730
      REWIND N1                                              MAINR740
      REWIND N2                                              MAINR750
105 N1=N1                                                    MAINR760
      IF(M.FO.1) N1=NORG                                     MAINR770
      READ (N1) A                                           MAINR780
110 DO 300 I=1,NFOR                                         MAINR790
      D=A(I)                                                 MAINR800
      IF(D) 115,300,120                                     MAINR810
115 M=NFOR*(N-1)+1                                         MAINR820
      WRITE (116) M,D                                       MAINR830
120 II=I                                                    MAINR840

```

```

      DO 125 J=2,NC
      II=II+NFOR
125  A(II)=A(II)/D
      DO 130 J=1,NMR,NFOR
      IF (A(J),NF,0.) MAXR(J)=J
130  CONTINUE
      JL=J+1
      IF (JL.GT,NFOR) GO TO 300
      II=J
      DO 200 J=JL,NFOR
      II=II+NFOR
      IF (II.GT,NMR) GO TO 200
      C=A(II)
      IF (C.EQ,0.0) GO TO 200
      C=C*A(J)
      KK=J-II
      MAX=MAXR(J)
      DO 150 JI=II,MAX,NFOR
150  A(JI+KK)=A(JI+KK)-C*A(JI)
      KK=J+NMR
      JI=J+NMR
      DO 175 L=1,LL
      A(KK)=A(KK)-C*A(JI)
      KK=KK+NFOR
175  JI=JI+NFOR
200  CONTINUE
300  CONTINUE
      WRITE (NRKS) A,MAXR
C*****
C-----SUBSTITUTE INTO REMAINING EQUATIONS
C*****
      DO 800 NN=1,NRR
      IF (N+NN.GT,NR1,OCK) GO TO 800
      NI=NI
      IF (N.FO,1) NI=NDRG
      IF (NN.FO,NRR) NI=NDRG
      RFAD (NI) R
      IL=1+NN*NFOR*NFOR
      DO 700 I=1,NFOR
      II=IL
      DO 690 K=1,NFOR
      IF (II.GT,NMR) GO TO 690
      C=A(II)
      IF (C.FO,0.0) GO TO 690
      C=C*A(K)
      MAX=MAXR(K)
      KK=I-II
      DO 640 JI=II,MAX,NFOR
640  R(JI+KK)=R(JI+KK)-C*A(JI)
      KK=I+NMR
      JI=K+NMR
      DO 650 L=1,LL
      R(KK)=R(KK)-C*A(JI)
      KK=KK+NFOR
650  JI=JI+NFOR
690  II=II-INC
700  IL=IL+NFOR
      IF (NRR.NF,.) GO TO 750
      DO 740 I=1,NMR
740  A(I)=R(I)

```

```

MAJNR850
MAJNR860
MAJNR870
MAJNR880
MAJNR890
MAJNR900
MAJNR910
MAJNR920
MAJNR930
MAJNR940
MAJNR950
MAJNR960
MAJNR970
MAJNR980
MAJNR990
MAJN9000
MAJN9010
MAJN9020
MAJN9030
MAJN9040
MAJN9050
MAJN9060
MAJN9070
MAJN9080
MAJN9090
MAJN9100
MAJN9110
MAJN9120
MAJN9130
MAJN9140
MAJN9150
MAJN9160
MAJN9170
MAJN9180
MAJN9190
MAJN9200
MAJN9210
MAJN9220
MAJN9230
MAJN9240
MAJN9250
MAJN9260
MAJN9270
MAJN9280
MAJN9290
MAJN9300
MAJN9310
MAJN9320
MAJN9330
MAJN9340
MAJN9350
MAJN9360
MAJN9370
MAJN9380
MAJN9390
MAJN9400
MAJN9410
MAJN9420
MAJN9430
MAJN9440

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```

      GO TO 800
750  WRITE (N2) R
800  CONTINUE
      M=N1
      N1=N2
      900  N2=M
C*****
C-----BACKSUBSTITUTION - RESULTS ON TAPE N1?
C*****
      LS=LL*NFOR
      NFB=NFOR*(NBR+1)
      NIIM=NBR*NFOR
      MAX=NFB*LL
      DO 905 I=1,MAX
905  R(I)=0.
      REWIND N1?
      DO 1000 M=1,NBLOCK
      BACKSPACE NRKS
      READ (NRKS) A,MAXR
      BACKSPACE NRKS
      DO 910 I=1,LL
      K=I*NFB
      DO 910 J=1,NIIM
      I=K-NFOR
      R(K)=R(I)
910  K=K-1
      J=NMR
      DO 920 I=1,LL
      K=(I-1)*NFB
      DO 920 J=1,NFOR
      I=J+1
      K=K+1
920  R(K)=A(I)
      DO 955 I=1,NFOR
      J=NFOR+1-I
      MAX=MAX*(J)
      IF (A(J, 0,0.) GO TO 955
      DO 950 I=1,LL
      KK=J+(I-1)*NFB
      JJ=KK+1
      II=J+NFOR
      C=R(KK)
      DO 940 II=II,MAX,NFOR
      C=C-A(II)*R(JJ)
940  JJ=JJ+1
950  R(KK)=C
955  CONTINUE
      I=0
      DO 960 I=1,LL
      K=(I-1)*NFB
      DO 960 J=1,NFOR
      K=K+1
      I=I+1
960  A(I)=R(K)
      WRITE(N12) (A(I),I=1,LS)
1000 CONTINUE
      RETURN
116  FORMAT ('33HOSEI OF EQUATIONS MAY BE SINGULAR /
      . 26H DIAGONAL TERM OF EQUATION .18, RH EQUALS .1PF12.4)
      ENDD

```

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MAIN9450
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MAIN0000
MAIN0010
MAIN0020
MAIN0030
MAIN0040

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      SUBROUTINE MAXDISP(DCON,R,NFOR,LL,I,D,NRLNCK,I2,I12,IW,NMAXD)      MAI N0050
C*****MAIN0060
C-----CALCULATE MAXIMUM DISPLACEMENT CONSTRAINT RATIOS      MAIN0070
C*****MAIN0080
      DIMENSION IDO(LD),DCON(LL,2,LD)      MAIN0090
      REAL*8 R(NFOR,LL)      MAIN0100
      COMMON/JUNK/M1(4),MF(4),RM(4),DC(4) ,JUN(284)      MAIN0110
      DO 1 I=1,NMAXD      MAIN0120
1    RM(I)=0.0      MAIN0130
      READ(I2) IDO,DCON      MAIN0140
      REWIND I2      MAIN0150
      NN=NFOR*NRLNCK      MAIN0160
      LD1=LD      MAIN0170
      DO 500 KK=1,NRLNCK      MAIN0180
        READ(I2)R      MAIN0190
        NN=NN-NFOR      MAIN0200
1      LT=IDO(LD1)      MAIN0210
        IF(LT,LF,NN) GO TO 500      MAIN0220
        LTN=LT-NN      MAIN0230
C*****MAIN0240
C-----CALCULATE ACTUAL DISPLACEMENT TO CONSTRAINED DISPLACEMENT RATIO      MAIN0250
C      FOR ALL LOAD CONDITIONS      MAIN0260
C*****MAIN0270
      DO 10 J=1,LL      MAIN0280
        RATIO=0.0      MAIN0290
        RB=R(LTN,J)      MAIN0300
        IF(RB) 20,10,30      MAIN0310
30    DD=DCON(J,1,LD1)      MAIN0320
        IF(DD,FO,0) GO TO 10      MAIN0330
        GO TO 50      MAIN0340
20    DD=-DCON(J,2,LD1)      MAIN0350
        IF(DD,FO,0) GO TO 10      MAIN0360
50    RATIO=RB/DD      MAIN0370
        ARATIO=ABS(RATIO)      MAIN0380
C*****MAIN0390
C-----FIND THE MIN. RATIO OF FOUR MAX. DISP. RATIOS FOUND SO FAR      MAIN0400
C*****MAIN0410
      R=1.0E20      MAIN0420
      J1=0      MAIN0430
      DO 70 JJ=1,NMAXD      MAIN0440
        R1=ABS(RM1(J,J))      MAIN0450
        IF(R1,GF,R) GO TO 70      MAIN0460
        R=R1      MAIN0470
        J1=JJ      MAIN0480
70    CONTINUE      MAIN0490
C*****MAIN0500
C-----REPLACE THIS MIN.RATIO WITH NEW RATIO IF IT IS GREATER      MAIN0510
C*****MAIN0520
      IF(ARATIO,LF,R) GO TO 10      MAIN0530
      RM1(J1)=RATIO      MAIN0540
      MF(J1)=LT      MAIN0550
      M1(J1)=J      MAIN0560
      DC(J1)=DD      MAIN0570
10    CONTINUE      MAIN0580
      LD1=LD1-1      MAIN0590
      IF(LD1,FO,0) GO TO 100      MAIN0600
      GO TO 1      MAIN0610
500    CONTINUE      MAIN0620
100    RETURN      MAIN0630
      END      MAIN0640

```



```

      SUBROUTINE PRINTN (ID,N,R,NFOR,NUMNP,LL,NRLOCK,NFO,I2,I8,IW,KP)      MAIN0650
C*****
C-----PRINT NODAL DISPLACEMENTS                                     MAIN0660
C*****
      DIMENSION ID(NUMNP,6),D(6,LL)                                     MAIN0670
      REAL*8 R(NFOR,LL)                                               MAIN0680
      REWIND IR                                                         MAIN0690
      READ (IR) ID                                                     MAIN0700
      IF(KP.FO.O) RETURN                                              MAIN0710
      REWIND I2                                                         MAIN0720
      M=NFO                                                            MAIN0730
      NN=NFOR*NRLNCK                                                  MAIN0740
      N=NUMNP                                                         MAIN0750
      WRITE(IW,2003)                                                  MAIN0760
      DO 500 KK=1,NUMNP                                              MAIN0770
      I=6                                                              MAIN0780
      DO 250 I=1,6                                                    MAIN0790
      DO 100 L=1,LL                                                    MAIN0800
100  D(I,L)=0.                                                         MAIN0810
      IF(M.GT.NN) GO TO 150                                           MAIN0820
      IF (M.FO.O) GO TO 150                                           MAIN0830
      READ(I2) R                                                       MAIN0840
      NN=NN-NFOR                                                       MAIN0850
150  IF (ID(N,I),I,I,1) GO TO 250                                     MAIN0860
      K=M-NN                                                           MAIN0870
      M=M-1                                                            MAIN0880
      DO 200 L=1,LL                                                    MAIN0890
200  D(I,L)=R(K,L)                                                    MAIN0900
250  I=I-1                                                            MAIN0910
      WRITE(IW,2004) N,(I,(D(I,L),I=1,6),L=1,LL)                   MAIN0920
500  N=N-1                                                            MAIN0930
      RETURN                                                           MAIN0940
2003 FORMAT (34H NODAL DISPLACEMENTS AND ROTATIONS//
. 5H NODF,5H LOAD,11X,1HX,11X,1HY,11X,1HZ,10X,2HXX,
. 10X,2HYY,10X,2HZZ/)
2004 FORMAT (1H,14,15,1P3F12,3,3F12.4/(10,3E12.3,3E12.4))
      FMD

```

```

      SUBROUTINE DPRINT (A,NV,IW)                                     MAIN1020
C*****
C-----PRINT DESIGN VARIABLE ARRAY                                     MAIN1030
C*****
      DIMENSION A(NV)                                                 MAIN1040
      WRITE(IW,1006)                                                  MAIN1050
      NROW=(NV-1)/10+1                                               MAIN1060
      DO 220 N=1,NROW                                                 MAIN1070
      M=(N-1)*10                                                      MAIN1080
      ISTART=M+1                                                       MAIN1090
      ISTOP=M+10                                                       MAIN1100
      IF (ISTOP.GT.NV) ISTOP=NV                                       MAIN1110
220  WRITE(IW,1007) M,(A(I),I=ISTART,ISTOP)                         MAIN1120
      RETURN                                                           MAIN1130
1006 FORMAT(//28H VALUES OF DESIGN VARIABLES //
1125H      1      2      3      4      5
2      6      7      8      9      10 /)
1007 FORMAT(1H,15,10F12.4)
      FMD

```

```

      SUBROUTINE STRESS(ADLD,ASTR,LOAD,STR,R,D,LL,LR,NFO,NUMDV,NFQB MAIN1210
      1 ,A,MTOT,I1,I2,I3,I11,IW) MAIN1220
C***** MAIN1230
C-----CALCULATE STRESSES MAIN1240
C***** MAIN1250
      DIMENSION STR(4,LL),D(NFO,LR),LOAD(NUMDV),ADLD(NUMDV),ASTR(NUMDV) MAIN1260
      1 ,A(MTOT) MAIN1270
      REAL*8 R(NFOR,LL) MAIN1280
      COMMON /ELPAR/ NPAR(14),NUMNP,MRAND,NELTYP,N1,N2,N3,N4,N5,MTIT, MAIN1290
      1 ELP(9),NRLDCK MAIN1300
      COMMON/JUNK/JUN(16),LT,LH ,JUN1(2R2) MAIN1310
      RFWIND I1 MAIN1320
      RFWIND I11 MAIN1330
      READ (I1) ADLD MAIN1340
      READ(I11) ASTR MAIN1350
C***** MAIN1360
C-----PRINT DESIGN VARIABLE ARRAY FOR CURRENT DESIGN MAIN1370
C***** MAIN1380
      CALL DPRINT (ADLD,NUMDV,IW) MAIN1390
      DO 111 I=1,NUMDV MAIN1400
      111 LOAD(I)=0 MAIN1410
      READ (I11) STR MAIN1420
      NT=(LL-1)/LR +1 MAIN1430
      LH=0 MAIN1440
      DO 1000 II=1,NT MAIN1450
C***** MAIN1460
C-----MOVE DISPLACEMENTS INTO CORE FOR LR LOAD CONDITIONS MAIN1470
C***** MAIN1480
      CALL MOVFDIR,R,D,NFOR,NRLDCK,NFO,LL,LR,LH,LT,I2) MAIN1490
C***** MAIN1500
C-----CALCULATE ELEMENT STRESSES AND PERFORM FULLY STRESSED DESIGN MAIN1510
      FOR LR LOAD CONDITIONS MAIN1520
C***** MAIN1530
      DO 1000 M=1,NELTYP MAIN1540
      READ (J8) NPAR MAIN1550
      MTYPF=NPAR(1) MAIN1560
      NPAR(1)=0 MAIN1570
      CALL FLTYPF (A,MTOT,MTYPF,IW) MAIN1580
      1000 CONTINUE MAIN1590
      RETURN MAIN1600
      END MAIN1610

      SUBROUTINE MOVFD(R,D,NFOR,NRLDCK,NFO,LL,LR,LH,LT,I2) MAIN1620
C***** MAIN1630
C-----MOVE DISPLACEMENTS INTO CORE FOR LR LOAD CONDITIONS FROM TAPE NT MAIN1640
C***** MAIN1650
      DIMENSION D(NFO,LR) MAIN1660
      REAL*8 R(NFOR,LL) MAIN1670
      RFWIND I2 MAIN1680
      LT=LH+1 MAIN1690
      I1T=1-LT MAIN1700
      LH=LT+LR-1 MAIN1710
      IF(LH.GT.LL ) LH=LL MAIN1720
      ND=NFOR*NRLDCK MAIN1730
      DO 200 NN=1,NRLDCK MAIN1740
      READ( I2) R MAIN1750

```

```

N=NFQR
IF (NN.EQ.1) N=NFQ-ND+NFQR
NQ=NQ-NFQR
DO 200 J=1,N
I=NQ+J
DO 200 L=L+1,LH
K=I+L+1
200 D(I,K)=R(J,L)
RETURN
END

```

```

MAIN1760
MAIN1770
MAIN1780
MAIN1790
MAIN1800
MAIN1810
MAIN1820
MAIN1830
MAIN1840
MAIN1850

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```

SUBROUTINE STRSC (AOLD,STR,D,NFQ,NUMDV,LL,LR,IR,NTAG)
C*****
C-----SET UP STRESS MATRIX AND CALCULATE STRESSES
C*****
REAL*8 P1,P2,ST1,ST2,ST,P
DIMENSION STR(4,LL),D(NEQ,LR),AOLD(NUMDV),P1(15,4),P2(15,4),
1 ST1(15,24),ST2(15,24)
COMMON/UNK/UN(16),LT,LH,L,SG(27),IDVAR,IFX,FRC,AREA,XINFR1,
1 DFSINF(249)
COMMON/EM/NU,NW,NS,ND,LM(24),ST(15,24,2),P(15,4,2),EM1(3358)
EQUIVALENCE (P1,P),(P2,P(61)),(ST,ST1),(ST(361),ST2)
IF (NTAG.EQ.0) GO TO 800
NL=L-LT+1
DO 300 I=1,NS
SG(I)=0.0
DO 300 J=1,4
300 SG(I)=SG(I)+P1(I,J)*STR(J,L)
DO 500 J=1,ND
JJ=LM(J)
IF (JJ.EQ.0) GO TO 500
DO 400 I=1,NS
400 SG(I)=SG(I)+ST1(I,J)*D(JJ,NL)
500 CONTINUE
GO TO 110
800 READ(18) NU,NW,NS,ND,IDVAR,IFX,FRC,(LM(I),I=1,ND),((ST(I,J,K),
1 J=1,NS),J=1,ND),K=1,NU),((P(I,J,K),I=1,NS),J=1,4),K=1,NW)
IF (IDVAR.EQ.0) GO TO 110
AREA= AOLD(IDVAR)*FRC
XINFR1=AREA**IFX
DO 100 I=1,NS
DO 101 J=1,4
101 P1(I,J)=P1(I,J)*AREA
DO 100 J=1,ND
100 ST1(I,J)=ST1(I,J)*AREA
READ(18) NI,(DFSINF(I),I=1,NI)
IF (NI.EQ.1) GO TO 900
DO 104 I=1,NS
DO 104 J=1,ND
104 ST1(I,J)=ST1(I,J)+ST2(I,J)*XINFR1
900 IF (NW.EQ.1) GO TO 110
DO 105 I=1,NS
DO 105 J=1,4
105 P1(I,J)=P1(I,J)+P2(I,J)
110 RETURN
END

```

```

MAIN1860
MAIN1870
MAIN1880
MAIN1890
MAIN1900
MAIN1910
MAIN1920
MAIN1930
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MAIN1950
MAIN1960
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MAIN1980
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MAIN2010
MAIN2020
MAIN2030
MAIN2040
MAIN2050
MAIN2060
MAIN2070
MAIN2080
MAIN2090
MAIN2100
MAIN2110
MAIN2120
MAIN2130
MAIN2140
MAIN2150
MAIN2160
MAIN2170
MAIN2180
MAIN2190
MAIN2200
MAIN2210
MAIN2220
MAIN2230
MAIN2240
MAIN2250
MAIN2260
MAIN2270
MAIN2280
MAIN2290
MAIN2300

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      SUBROUTINE DESIGN(ADLD,ASTP,LOAD,IWGT,NUMDV,I,IR,I11,IW,IP)      MAIN2310
C*****MAIN2320
C-----EVALUATE THE CURRENT DESIGN AND PERFORM REDESIGN OPERATION      MAIN2330
C*****MAIN2340
      DIMENSJON ADLD(NUMDV),ASTR(NUMDV),LOAD(NUMDV),IWGT(NUMDV)      MAIN2350
      COMMON/CONTR/ICYCL,NCYCL,ISCALE,NSCALE,KSCALE,KONVG,IDESN,IWTMIN,      MAIN2360
      IWTMIN,FPSIL,DELTA1,DELTA2,KPUNCH,KDISP,NMAXI,NDISP,LB1,ALPA,SF,IS,      MAIN2370
      I,SMAX,DMAX,CONST      MAIN2380
      COMMON/JUNK/ML1(4),MF1(4),DRAT(4),DCON(4),JUN(284)      MAIN2390
      READ(18) IWGT      MAIN2400
      KONVG=1      MAIN2410
      SMAX=0.      MAIN2420
      SMIN=1.0F20      MAIN2430
      DMAX=0.      MAIN2440
      NDISP=0      MAIN2450
      IS=0      MAIN2460
      WT=0.      MAIN2470
      RCONST=2.0      MAIN2480
      DO 221 I=1,NUMDV      MAIN2490
221 WT=WT+ADLD(I)*IWGT(I)      MAIN2500
C*****MAIN2510
C-----COMPUTE MAX. AND MIN. STRESS RATIOS AND PRINT THEM      MAIN2520
C*****MAIN2530
      DO 68 I=1,NUMDV      MAIN2540
      R=ASTR(I)/ADLD(I)      MAIN2550
      IF(R.LF.SMAX) GO TO 69      MAIN2560
      SMAX=R      MAIN2570
      IMAX=I      MAIN2580
      LMAX=LOAD(I)      MAIN2590
69 IF(R.GF.SMIN) GO TO 68      MAIN2600
      SMIN=R      MAIN2610
      IMIN=I      MAIN2620
      LMIN=LOAD(I)      MAIN2630
68 CONTINUE      MAIN2640
      WRITE(IW,1000) IDESN,SMAX,LMAX,IMAX,SMIN,LMIN,IMIN      MAIN2650
      IF(KDISP.FO.0) GO TO 80      MAIN2660
C*****MAIN2670
C-----PRINT DISPLACEMENT CONSTRAINT RATIOS      MAIN2680
C*****MAIN2690
      WRITE(IW,2002)      MAIN2700
      DO 79 J=1,NMAXD      MAIN2710
      IF(DRAT(J).NE.0) WRITE(IW,2001) DRAT(J),ML1(J),MF1(J)      MAIN2720
79 CONTINUE      MAIN2730
C*****MAIN2740
C-----CALCULATE NO. OF POSSIBLE ACTIVE DISPLACEMENT CONSTRAINTS      MAIN2750
C-----ZERO OUT DISPLACEMENT RATIOS WHICH ARE NOT LIKELY TO BE ACTIVE      MAIN2760
C-----FIND MAX. DISPLACEMENT RATIO      MAIN2770
C*****MAIN2780
      DO 70 J=1,NMAXD      MAIN2790
      ARD=ABS(DRAT(J))      MAIN2800
      IF(KSCALE.GT.0) ARD=(ARD)**(1.0/KSCALE)      MAIN2810
      R=ARD/SMAX      MAIN2820
      IF(R.LT.CONST) GO TO 71      MAIN2830
      NDISP=NDISP+1      MAIN2840
      IF(ARD.GT.DMAX) DMAX=ARD      MAIN2850
      GO TO 70      MAIN2860
71 DRAT(J)=0.      MAIN2870
70 CONTINUE      MAIN2880
80 SF=SMAX      MAIN2890
      IF(SF.LT.DMAX) SF=DMAX      MAIN2900

```

IF(SF.LT.DELTA1.OR.SF.GT.DELTA2) GO TO 305	MAIN2910
IF(SMIN.LT.DELTA1.OR.SMIN.GT.DELTA2) GO TO 83	MAIN2920
WRITE(IW,1004)	MAIN2930
KONVVG=4	MAIN2940
WRITE(IW,1008) WT	MAIN2950
GO TO 85	MAIN2960
83 WRITE(IW,1003)	MAIN2970
WRITE(IW,1008) WT	MAIN2980
84 WRITE(IW,2005)	MAIN2990
KONVVG=3	MAIN3000
IF(DMAX.GT.SMAX) KONVVG=2	MAIN3010
ISCALF=0	MAIN3020
ICYCL=ICYCL+1	MAIN3030
IF(ICYCL.LE.NCYCL) GO TO 85	MAIN3040
KONVVG=4	MAIN3050
WRITE(IW,1005) NCYCL	MAIN3060
GO TO 85	MAIN3070
305 IF(KSCALF.GE.0 .AND. SF.LT.RCONST) GO TO 101	MAIN3080
WRITE(IW,1002)	MAIN3090
GO TO 84	MAIN3100
101 IS=1	MAIN3110
IF(KSCALF.LE.0) SF=SMAX	MAIN3120
DO 103 I=1,NIMDV	MAIN3130
103 ADLN(I)=ADLN(I)*SF	MAIN3140
IF(KSCALF.LE.0) GO TO 803	MAIN3150
WRITE(IW,2004)	MAIN3160
CALL MSG(SMAX,DMAX,SF,IW)	MAIN3170
WRITE(IW,2006)	MAIN3180
CALL DPRINT (ADLN,NIMDV,IW)	MAIN3190
WT=WT*SF	MAIN3200
WRITE(IW,1008) WT	MAIN3210
GO TO 84	MAIN3220
802 WRITE(IW,1002)	MAIN3230
WRITE(IW,2004)	MAIN3240
ISCALF=ISCALF+1	MAIN3250
IF(ISCALF.EQ.NSCALF) GO TO 203	MAIN3260
IF(NDISP.NE.0) RETURN	MAIN3270
REWIND 11	MAIN3280
WRITE(J1) ADLN	MAIN3290
CALL MSG(SMAX,SMAX,SMAX,IW)	MAIN3300
RETURN	MAIN3310
203 KONVVG=4	MAIN3320
WRITE(IW,1001) NSCALF	MAIN3330
85 IF(KONVVG.EQ.4) GO TO 501	MAIN3340
IF(KSCALF.LT.0 .OR.SF.GE.2.0) GO TO 503	MAIN3350
IF(WT.LT.WTMIN) GO TO 502	MAIN3360
R=(WT-WTMIN)/WTMIN	MAIN3370
IF(R.LT.FPS1L) GO TO 503	MAIN3380
KONVVG=4	MAIN3390
WRITE(IW,1009) WTMIN	MAIN3400
GO TO 501	MAIN3410
502 WTMIN=WT	MAIN3420
WTMIN=JNFSN	MAIN3430
503 IF(NDISP.EQ.0) REWIND 11	MAIN3440
WRITE(J1) ASTR	MAIN3450
RETURN	MAIN3460
501 IF(KPUNCH.NE.1) RETURN	MAIN3470
REWIND 11	MAIN3480
READ(I1) ASTR	MAIN3490
DO 250 I=1,NIMDV	MAIN3500

```

250 WRITE(IP,1010) I,APLD(I),ASTR(I)
RETURN
1000 FORMAT (// 32H *****/
1      28H EVALUATION OF DESIGN NUMBER,I4 /
2      32H *****///
350H      STRESS RATIO LOAD COND DES VARIABLE/.
4 4H MAX,F18.4,I10,I13, /
5 4H MIN,F18.4,I10,I13 / )
1001 FORMAT(49H TERMINAL DESIGN---NUMBER OF SCALING OPERATIONS= ,I4//)
1002 FORMAT(//23H DESIGN IS NOT CRITICAL//)
1003 FORMAT(//23H DESIGN IS CRITICAL //)
1004 FORMAT(//23H DESIGN IS ACCEPTABLE //)
1005 FORMAT(//48H TERMINAL DESIGN---NUMBER OF CRITICAL DESIGNS =,I5//)
1008 FORMAT(//19H STRUCTURAL WEIGHT=F11.4)
1009 FORMAT(60H TERMINAL DESIGN---LIGHTEST CRITICAL DESIGN IS DESIGN
NUMBER,I4//)
1010 FORMAT(I5,2F10.5)
2001 FORMAT(7X,F13.4,2I10)
2002 FORMAT(48H MAX DISP RATIOS LOAD COND FOR NUMBER/ )
2004 FORMAT(//1X,33HUNIFORM SCALING OPERATION FOLLOWS)
2005 FORMAT(//1X,26HREDDESIGN OPERATION FOLLOWS)
2006 FORMAT(//1X,48HDESIGN VARIABLES OF SCALED (CRITICAL) DESIGN ARE)
END

```

```

MAIN3510
MAIN3520
MAIN3530
MAIN3540
MAIN3550
MAIN3560
MAIN3570
MAIN3580
MAIN3590
MAIN3600
MAIN3610
MAIN3620
MAIN3630
MAIN3640
MAIN3650
MAIN3660
MAIN3670
MAIN3680
MAIN3690
MAIN3700
MAIN3710
MAIN3720
MAIN3730

```

```

SURROUNDING MSG(SF,DF,SFF,IW)
C*****
C-----PRINT SCALE FACTOR FOR DESIGN SCALING
C*****
IF(SF,GF,DF) GO TO 550
WRITE(IW,1003) SFF
WRITE(IW,1004)
GO TO 551
550 WRITE(IW,1003) SF
WRITE(IW,1005)
551 RETURN
1003 FORMAT(//1X,15HSCALE FACTOR IS,F7.3,17HAND DETERMINED BY)
1004 FORMAT(1H+,40X,24HDISPLACEMENT CONSTRAINTS)
1005 FORMAT(1H+,40X,18HSTRESS CONSTRAINTS)
END

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```

MAIN3740
MAIN3750
MAIN3760
MAIN3770
MAIN3780
MAIN3790
MAIN3800
MAIN3810
MAIN3820
MAIN3830
MAIN3840
MAIN3850
MAIN3860
MAIN3870
MAIN3880

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      SUBROUTINE DDFRV (A,AD,MTOT,MTOT2,NR(NIND))          MA1N3890
C*****
C-----CALCULATE DISPLACEMENT DERIVATIVES              MA1N3900
C*****
      COMMON/ELPAR/NPAR(14),NUMNP,MRAND,NFLYP,N1,N2,N3,N4,N5,MTT,NEQ  MA1N3910
      I,NUMFL,NUMDV,M1,M2,M3,LL,LR,NFOR,NRLOCK              MA1N3920
      COMMON/JUNK/JUNK1(16),JUNK2(16),JUNK3(268)            MA1N3930
      COMMON/JNITS/IR,IW,IP,I1,I2,I3,IA,I9,I10,I11,I12       MA1N3940
      COMMON/CONTR/ICYCL,NCYCL,ISCALF,NSCALF,KSCALF,KONVG,IDESN,IWTMIN,MA1N3950
      IWTMIN,FPSIL,DFLTA1,DFLTA2,KPUNCH,KDISP,NMAXD,NDISP,LB1,ALPA,SF,IS,MA1N3960
      I,SMAX,NMAX,OMEGA                                         MA1N3970
      DIMENSION A(MTOT)                                         MA1N3980
      REAL*8 AD(MTOT2)                                          MA1N3990
      DO 10 J=1,16                                              MA1N4000
      10 JUNK2(I)=0                                              MA1N4010
C*****
C-----REARRANGE ACTUAL DISPLACEMENTS AND DISP. CONSTRAINT RATIOS MA1N4020
C-----A(I), I=1..NUMDV IS AOLD CARRIED FROM STRESS AND DESIGN SUBROUTINE MA1N4030
C*****
      IRI=(MTOT-NFOR*(I*2-NUMDV))/NFO                          MA1N4040
      IF(LR1,GT,LL)LR1=IL                                       MA1N4050
      M1=1                                                       MA1N4060
      N2=N1+NUMDV                                                MA1N4070
      N3=N2+NFO*LR1                                              MA1N4080
      ND3=N3/2+1                                                 MA1N4090
      CALL ARRAN(A(N2),AD(ND3),LR1,LL,NFOR,NRLOCK,NFO,NMAXD,I2,I3) MA1N4100
C*****
C-----CALCULATE THE PRODHCT OF ACTUAL TRANSPOSE* STIFFNESS MATRIX DFR. MA1N4110
C*****
      IRI=(MTOT-NFOR*NDISP*2)/(NUMDV+NFO)                     MA1N4120
      IF(LR1,GE,1) GO TO 25                                     MA1N4130
      MM=NFOR*NDISP*2+NFO+NUMDV-MTOT                           MA1N4140
      CALL FRROR(MM)                                             MA1N4150
      25 IF(LR1,GT,NDISP)LR1=NDISP                              MA1N4160
      CALL FORCES(A(N1),A(N2),LR1,NFO,NDISP,NUMFL,NUMDV,I1,I3,I12) MA1N4170
C*****
C-----INPUT DIMMY LOADS                                  MA1N4180
C*****
      ND2=N1+NFOR*MRAND                                          MA1N4190
      CALL DIMMAN(AD(N1),AD(ND2),AD(ND2),NFOR,MBAND,NRLOCK,LL,NDISP,I2, MA1N4200
      I110)                                                      MA1N4210
C*****
C-----CALCULATE DIMMY DISPLACEMENTS                     MA1N4220
C*****
      NSR=(MBAND+NDISP)*NFOR                                     MA1N4230
      N2=N1+NFOR                                                 MA1N4240
      ND2=N2/2+1                                                 MA1N4250
      ND3=ND2+NSR                                                MA1N4260
      CALL HSNL(A(N1),AD(ND2),AD(ND3),NFOR,MRAND,NDISP,NRLOCK,NSR MA1N4270
      ,I2,I3,I9,I10,IW)                                         MA1N4280
C*****
C-----CALCULATE DERIVATIVES                              MA1N4290
C*****
      N2=N1+NUMDV*LR1                                           MA1N4300
      N3=N2+NFO*LR1                                              MA1N4310
      ND3=N3/2+1                                                 MA1N4320
C*****
C-----READ AOLD AND/OR ASIR TO ADVANCE FILE 1          MA1N4330
C*****
      PFWJND 11                                                 MA1N4340

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```

      READ(I1) (A(I),I=1,NUMDV)
      IF(KONVG,NF,I) READ(I1) (A(I),I=1,NUMDV)
      NUMF=NUMFL-NRROUND
      CALL DFRV(AIN1),A(N2),AD(N23),NDISP,I,RI,NUMDV,NEQ,NEQB,NBLOCK,
1 NUMF ,I1,I3,I10,I11)
      RETURN
      END

```

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      MAJN4490
      MAJN4500
      MAJN4510
      MAJN4520
      MAJN4530
      MAJN4540
      MAJN4550

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      SUBROUTINE ARRAN(D,R,LR1,LL,NFOR,NBLOCK,NFO,NMAXD,I2,I3)
C*****
C-----REARRANGE ACTUAL DISPLACEMENTS WHICH ARE ON TAPE I2
C*****
      DIMENSION D(NFO,LR1)
      REAL*8 R(NFOR,LL)
      COMMON/JUNK/ML(4),MF(4),RM(4),DC(4),MLC(4),MEO(4),DRAT(4),DCON(4)
      I=JUNK(268)
      NT=(LL-1)/LR1+1
      IH=0
      IL=0
      REWINO I3
      DO 10 I=1,NT
      CALL MOVEO(R,D,NFOR,NBLOCK,NFO,LL,LR1,IH,LI,I2)
C*****
C-----WRITE THE DISPLACEMENTS FOR MAX. RATIOS ON TAPE I3
C-----REARRANGE MAX. DISPLACEMENT RATIOS IN INCREASING ORDER OF LOAD
C      CONDITION NUMBERS
C*****
      DO 10 J=1,I,LI
      DO 10 K=1,NMAXD
      IF(RM(K),FO,O) GO TO 10
      KK=ML(K)
      IF(KK,NF,J) GO TO 10
      WRITE(I3) (D(M,KK),M=1,NFO)
      L=L+1
      MLC(L)=ML(K)
      MEO(L)=MF(K)
      DRAT(L)=RM(K)
      DCON(L)=DC(K)
10 CONTINUE
      RETURN
      END

```

```

      MAJN4560
      MAJN4570
      MAJN4580
      MAJN4590
      MAJN4600
      MAJN4610
      MAJN4620
      MAJN4630
      MAJN4640
      MAJN4650
      MAJN4660
      MAJN4670
      MAJN4680
      MAJN4690
      MAJN4700
      MAJN4710
      MAJN4720
      MAJN4730
      MAJN4740
      MAJN4750
      MAJN4760
      MAJN4770
      MAJN4780
      MAJN4790
      MAJN4800
      MAJN4810
      MAJN4820
      MAJN4830
      MAJN4840
      MAJN4850
      MAJN4860
      MAJN4870
      MAJN4880

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      SUBROUTINE FORCES(ADLD,D,LR1,NFO,NDISP,MUMFL,MUMDV,I1,I3,I12)      MAIN4890
C*****MAIN4900
C-----CALCULATE THE INTERMEDIATE PRODUCT U(I) TRANSPOSE*      MAIN4910
C      (STIFFNESS MATRIX DERIVATIVE) IN CALCULATING DEFLECTION CONSTRAINT      MAIN4920
C      DERIVATIVES      MAIN4930
C*****MAIN4940
      REAL*P S,P,S1,S2
      DIMENSION ADLD(NUMDV),D(NFO,LR1),S1(24,24),S2(24,24)      MAIN4950
      COMMON/FM/LM(24),S(24,24,2),P(24,4,2),FM(2354)      MAIN4960
      COMMON/JUNK/JUN(32),C(4,24),JUN1(172)      MAIN4970
      EQUIVALENCE (S1,S),(S2,S(577))      MAIN4980
      REWIND 13      MAIN4990
      LI=LR1      MAIN5000
      NT=(NDISP-1)/LR1+1      MAIN5010
      DO 100 I=1,NT      MAIN5020
C*****MAIN5030
C-----READ ACTUAL DISPLACEMENT FOR LR LOAD CONDITIONS      MAIN5040
C*****MAIN5050
      LT=I*LR1      MAIN5060
      IF(LT,GT,NDISP)LT=NDISP-LT+LR1      MAIN5070
      DO 200 L=1,LI      MAIN5080
      200 READ(13) (D(I,L),I=1,NFO)      MAIN5090
      REWIND 12      MAIN5100
      DO 100 NN=1,MUMFL      MAIN5110
C*****MAIN5120
C-----READ ELEMENT INFORMATION      MAIN5130
C*****MAIN5140
      READ(12) LRD,MU,NV,ND,IDVAR,IFX,FRC,(LM(I),I=1,ND),((S(I,J,K),      MAIN5150
      I=1,ND),J=1,ND),K=1,MU),((P(I,J,K),I=1,ND),J=1,4),K=1,NV)      MAIN5160
      IF(IDVAR,LE,0) GO TO 100      MAIN5170
C*****MAIN5180
C-----CALCULATE STIFFNESS MATRIX DERIVATIVE      MAIN5190
C*****MAIN5200
      IF(MU,FO,1) GO TO 501      MAIN5210
      FR=IFX*(FRC*ADLD(IDVAR))**(IFX-1)      MAIN5220
      DO 502 I=1,ND      MAIN5230
      DO 502 J=1,ND      MAIN5240
      502 S1(I,J)=S1(I,J)+S2(I,J)*FR      MAIN5250
      501 DO 300 I=1,ND      MAIN5260
      DO 300 J=1,ND      MAIN5270
      300 S1(I,J)=S1(I,J)*FRC      MAIN5280
C*****MAIN5290
C-----CALCULATE THE PRODUCT U(I) TRANSPOSE *STIFFNESS MATRIX DERIVATIVE      MAIN5300
C*****MAIN5310
      DO 950 I=1,LI      MAIN5320
      DO 950 J=1,ND      MAIN5330
      950 C(I,J)=0.0      MAIN5340
      DO 610 K=1,ND      MAIN5350
      MM=LM(K)      MAIN5360
      IF(MM,LE,0) GO TO 610      MAIN5370
      DO 600 I=1,LI      MAIN5380
      DO 600 J=1,ND      MAIN5390
      600 C(I,J)=C(I,J)+D(MM,I)*S1(K,J)      MAIN5400
      610 CONTINUE      MAIN5410
      WRITE(11) ND,IDVAR , ((C(I,J),J=1,ND),I=1,LI), (LM(I),I=1,ND)      MAIN5420
      100 CONTINUE      MAIN5430
      RETURN      MAIN5440
      END      MAIN5450
      FMD      MAIN5460

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      SUBROUTINE DIHMAN(A,R,C,NFOR,MRAND,NBLOCK,LL,NDISP,I2,I10)      MAIN5470
C*****MAIN5480
C-----PUT IN DIMMY LOADS FOR CALCULATION OF DISPLACEMENT DERIVATIVES      MAIN5490
      REAL*8 A(NFOR,MRAND),R(NFOR,LL),C(NFOR,NDISP)      MAIN5510
      COMMON/JUNK/JUN(16),MLC(4),MFO(4),DRAT(4),DCON(4),JUN1(268)      MAIN5520
      RFWIND I2      MAIN5530
      RFWIND I10      MAIN5540
      DO 10 I=1,NBLOCK      MAIN5550
      READ(I10) A,R      MAIN5560
      DO 20 I=1,NFOR      MAIN5570
      DO 20 J=1,NDISP      MAIN5580
20 C(I,J)=0.0      MAIN5590
      NT=(I-1)*NFOR      MAIN5600
      NF=NT+NFOR      MAIN5610
      DO 50 J=1,NDISP      MAIN5620
      J=MFO(I)      MAIN5630
      IF(J,LF,MJ) GO TO 50      MAIN5640
      IF(J,GT,NF) GO TO 50      MAIN5650
      C(I-MJ,J)=1.      MAIN5660
      IF(DRAT(I),LT,0) C(J-MJ,I)=-1.0      MAIN5670
50 CONTINUE      MAIN5680
10 WRITE(I2)A,C      MAIN5690
      RETURN      MAIN5700
      END      MAIN5710

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      SUBROUTINE DERVFOR I,D,R,NDISP,LR1,NUMDV,NFO,NFOR,NBLOCK,NUMFL,I1,      MAIN5720
      I13,I10,I11)      MAIN5730
C*****MAIN5740
C-----CALCULATE DISPLACEMENT DERIVATIVES      MAIN5750
C*****MAIN5760
      DIMENS ION DR1(NUMDV,LR1),D(NFO,LR1)      MAIN5770
      REAL*8 R(NFOR,NDISP)      MAIN5780
      COMMON/JUNK/JUN(32),ND,INVAR,I1,C(4,24),LM(24),JUN1(145)      MAIN5790
      NT=(NDISP-1)/LR1+1      MAIN5800
      LH=0      MAIN5810
      RFWIND I3      MAIN5820
      DO 200 I=1,NT      MAIN5830
C*****MAIN5840
C-----MOVE DISPLACEMENTS INTO CORE FOR LR LOAD CONDITIONS.      MAIN5850
C*****MAIN5860
      CALL MOVFOR(R,D,NFOR,NBLOCK,NFO,NDISP,LR1,LH,LT,I10)      MAIN5870
      LI=LH-LT+1      MAIN5880
      DO 50 I=1,NUMDV      MAIN5890
      DO 50 J=1,LI      MAIN5900
50 DR1(I,J)=0.0      MAIN5910
      DO 100 M=1,NUMFL      MAIN5920
C*****MAIN5930
C-----READ THE PRODUCT U(ACTUAL) TRANSPOSE* STIFFNESS MATR. DERIVATIVE      MAIN5940
C*****MAIN5950
      READ(I1) ND,INVAR, (C(I,J),J=1,ND),I=1,LI),(LM(I),I=1,ND)      MAIN5960
C*****MAIN5970
C-----CALCULATE DERIVATIVES      MAIN5980
C*****MAIN5990
      DO 100 I=1,ND      MAIN6000
      MM=LM(I)      MAIN6010
      IF(MM,LF,0) GO TO 100      MAIN6020
      DO 510 K=1,LI      MAIN6030

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```

510 ORT((IDVAR,K)=ORT((IDVAR,K )-C(K,I)*D(MM,K)          MAIN6040
100 CONTINUE          MAIN6050
C*****          MAIN6060
C-----WRITE DISPLACEMENT DERIVATIVES ON TAPE          MAIN6070
C*****          MAIN6080
      DO 300 J=1,L1
      300 WRITE(J3) (ORT((K,J),K=J),NUMDV)          MAIN6090
      200 CONTINUE          MAIN6100
      RETURN          MAIN6110
      END          MAIN6120
          MAIN6130

      SUBROUTINE DISP(R,D,AMDA,NDISP,ICCN)          MAIN6140
C*****          MAIN6150
C-----FIND OUT ACTIVE LAMBDAS(IF +VE DISP. CONSTRAINTS)          MAIN6160
C*****          MAIN6170
      DIMENSION R(4),D(4,4),AMDA(4)
      ICEN=NDISP          MAIN6180
      IF(MDISP.GT.1) GO TO 900          MAIN6190
      AMDA(1)=R(1)/D(1,1)          MAIN6200
      IF(AMDA(1).GT.0.) RETURN          MAIN6210
      AMDA(1)=0.          MAIN6220
      ICEN=0          MAIN6230
      RETURN          MAIN6240
900  IF(D(2,2).NE.0.) GO TO 10          MAIN6250
      IF(D(1,1).NE.0.) GO TO 11          MAIN6260
      AMDA(1)=0.          MAIN6270
      AMDA(2)=0.          MAIN6280
      ICEN=0          MAIN6290
      RETURN          MAIN6300
11   AMDA(1)=R(1)/D(1,1)          MAIN6310
      AMDA(2)=0.          MAIN6320
      ICEN=1          MAIN6330
      IF(AMDA(1).GT.0.) RETURN          MAIN6340
      AMDA(1)=0.          MAIN6350
      ICEN=0          MAIN6360
      RETURN          MAIN6370
10   IF(D(1,1).NE.0.) GO TO 20          MAIN6380
      AMDA(1)=0.          MAIN6390
      AMDA(2)=R(2)/D(2,2)          MAIN6400
      ICEN=1          MAIN6410
      IF(AMDA(2).GT.0.) RETURN          MAIN6420
      AMDA(2)=0.          MAIN6430
      ICEN=0          MAIN6440
      RETURN          MAIN6450
20   DFI=D(1,1)*D(2,2)-D(1,2)*D(1,2)          MAIN6460
      C1=D(1,1)*D(2,2)*1.0E-06          MAIN6470
      IF(ABS(DFI).GT.C1) GO TO 30          MAIN6480
      A1=R(1)/D(1,1)          MAIN6490
      A2=R(2)/D(2,2)          MAIN6500
      IF(A1.LE.0..AND.A2.LE.0.) GO TO 40          MAIN6510
      IF(A2.GT.A1) GO TO 50          MAIN6520
      AMDA(1)=A1          MAIN6530
      AMDA(2)=0.          MAIN6540
      ICEN=1          MAIN6550
      RETURN          MAIN6560
50   AMDA(1)=0.          MAIN6570

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```

      AMDA(2)=A2
      ICON=1
      RETURN
40  AMDA(1)=0.
      AMDA(2)=0.
      ICON=0
      RETURN
30  AMDA(1)=(D(2,2)*R(1)-D(1,2)*R(2))/DFL
      AMDA(2)=(-D(2,1)*R(1)+D(1,1)*R(2))/DFL
      IF(AMDA(1).GT.0..AND. AMDA(2).GT.0.) RETURN
      IF(AMDA(1).GT. AMDA(2)) GO TO 60
      AMDA(1)=0.
      AMDA(2)=R(2)/D(2,2)
      ICON=1
      IF(AMDA(2).GT.0.) RETURN
      AMDA(2)=0.
      ICON=0
      RETURN
60  AMDA(1)=R(1)/D(1,1)
      AMDA(2)=0.
      ICON=1
      IF(AMDA(1).GT.0.) RETURN
      AMDA(1)=0.
      ICON=0
      RETURN
      END

```

```

MAIN6590
MAIN6600
MAIN6610
MAIN6620
MAIN6630
MAIN6640
MAIN6650
MAIN6660
MAIN6670
MAIN6680
MAIN6690
MAIN6700
MAIN6710
MAIN6720
MAIN6730
MAIN6740
MAIN6750
MAIN6760
MAIN6770
MAIN6780
MAIN6790
MAIN6800-
MAIN6810
MAIN6820
MAIN6830
MAIN6840

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      SUBROUTINE DDESIGN(ORI, ID1, ADL0, ASTR, ADIS, UWT, OPTIND, NUMDV, NDISP, MAIN6850
      1 IL, IR, IR, TW) MAIN6860
C***** MAIN6870
C-----CARRY OUT DISPLACEMENT REDESIGN OR SCALING MAIN6880
C***** MAIN6890
      DIMENS(ND1(NUMDV), ADL0(NUMDV), ASTR(NUMDV), ADIS(NUMDV), MAIN6900
      JORI(NUMDV, NDISP), UWT(NUMDV), OPTIND(NUMDV) MAIN6910
      COMMON/CONST/ ICYCL, NCYCL, ISCALE, NSCALE, KCONVG, IDFSN, IWTMIN, MAIN6920
      IWTMIN, FPSTL, DELTA1, DELTA2, KPUNCH, KDISP, NMAXD, NDISS, LH1, ALPA, SF, IS, MAIN6930
      1 SMAX, DMAX, DMFGA MAIN6940
      COMMON/JUNK/JUN(16), ML(4), ME(4), DRAT(4), PCPN(4), D(4,4), R(4), AMDA(4) MAIN6950
      1, S(4), JUN1(240) MAIN6960
      DATA TAG1, TAG2/3HACT, 4HPASS/ MAIN6970
      DEL5=5.0*(1.0-DELTA1) MAIN6980
      DELT11=1.0-DEL5 MAIN6990
      DELT22=1.0+DEL5 MAIN7000
      BACKSPACE IR MAIN7010
      READ( IR ) UWT MAIN7020
      REWIND IR MAIN7030
      READ( IR ) ADL0 MAIN7040
      REWIND IR MAIN7050
      DO 61 J=1, NDISP MAIN7060
      61 READ( IR ) (ORI(J, I), J=1, NUMDV) MAIN7070
      60 IF (KCONVG, EQ, 1) GO TO 501 MAIN7080
C***** MAIN7090
C-----DISPLACEMENT CONSTRAINT REDESIGN MAIN7100
C***** MAIN7110
      READ( IR ) ASTR MAIN7120
      REWIND IR MAIN7130
      IF (IS, NE, 1) GO TO 101 MAIN7140
C***** MAIN7150
C-----CONVERT DISPLACEMENT RATIOS AND DERIVATIVES TO THE SCALED DESIGN MAIN7160
C***** MAIN7170
      DO 99 I=1, NUMDV MAIN7180
      99 ADL0(I)=ADL0(I)*SF MAIN7190
      SFF=SF*KSCALE MAIN7200
      SFFF=SFF*SF MAIN7210
      DO 102 I=1, NDISP MAIN7220
      DRAT(I)=DRAT(I)/SFF MAIN7230
      DO 102 J=1, NUMDV MAIN7240
      102 ORI(J, I)=ORI(J, I)/SFFF MAIN7250
C***** MAIN7260
C-----CLASSIFY DESIGN VARIABLES EITHER AS ACTIVE OR PASSIVE MAIN7270
C-----DESIGN VARIABLES WITH THEIR DERIVATIVES FOR ALL POTENTIALLY MAIN7280
C-----ACTIVE DISPLACEMENT CONSTRAINTS AS POSITIVE ARE PASSIVE VARIABLES MAIN7290
C***** MAIN7300
      DO 50 J=1, NUMDV MAIN7310
      DO 51 J=1, NDISP MAIN7320
      IF (ORI(J, J), LT, 0.) GO TO 49 MAIN7330
      51 CONTINUE MAIN7340
      ID1(I)=0 MAIN7350
      GO TO 50 MAIN7360
      49 ID1(I)=1 MAIN7370
      50 CONTINUE MAIN7380
C***** MAIN7390
C-----ITERATION TO FIND OUT ACTIVE/PASSIVE CLASSIFICATION OF DESIGN MAIN7400
C-----VARIABLES MAIN7410
C***** MAIN7420
      700 MAC=1 MAIN7430
C***** MAIN7440

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C-----CHECK IF ALL DESIGN VARIABLES ARE PASSIVE                                MAIN7450
C*****MAIN7460
      DO 52 I=1,NIMDV                                MAIN7470
      IF (D1(I),F0,1) GO TO 599                        MAIN7480
      52 CONTINUE                                       MAIN7490
C*****MAIN7500
C-----ALL DESIGN VARIABLES ARE PASSIVE. TAKE STRESS DESIGN AND GO FOR          MAIN7510
C      NEXT DESIGN CYCLE                                MAIN7520
C*****MAIN7530
      ICNN=0                                            MAIN7540
      GO TO 602                                         MAIN7550
C*****MAIN7560
C-----CALCULATE RIGHT HAND SIDES OF SIMULTANEOUS EQUATIONS FOR LAMBDA'S        MAIN7570
C*****MAIN7580
      599 DO 80 I=1,4                                  MAIN7590
      R(I)=0.                                           MAIN7600
      AMDA(I)=0.                                         MAIN7610
      DO 80 J=1,4                                       MAIN7620
      DO 100 I=1,NDISP                                  MAIN7630
      NP=0.0                                             MAIN7640
      NA=0.0                                             MAIN7650
      DO 110 J=1,NIMDV                                  MAIN7660
      IF (D1(J),F0,1) GO TO 120                         MAIN7670
      NP=NP+DR1(J,I)*(ASTR(I)-AOLD(I))                 MAIN7680
      GO TO 110                                          MAIN7690
      120 NA=NA+DR1(J,I)*AOLD(I)                        MAIN7700
      110 CONTINUE                                       MAIN7710
      100 R(I)=(I-ALPA)*NA+(1-BHS(DRAT(I))) * DCNN(I) -NP MAIN7720
C*****MAIN7730
C-----DEVELOP COEFFICIENT MATRIX FOR LAMBDA'S                                MAIN7740
C*****MAIN7750
      DO 250 I=1,NDISP                                  MAIN7760
      DO 250 J=1,NDISP                                  MAIN7770
      D(I,J)=0.                                         MAIN7780
      DO 260 K=1,NIMDV                                  MAIN7790
      IF (D1(K),F0,1) D(I,J)=D(I,J)+DR1(K,I)*DR1(K,J)*AOLD(K)/UW1(K) MAIN7800
      260 CONTINUE                                       MAIN7810
      D(I,J)=-D(I,J)*(1.-ALPA)                         MAIN7820
      250 D(I,J)=D(I,J)                                MAIN7830
C*****MAIN7840
C-----ITERATION TO FIND ACTIVE DISPLACEMENT CONSTRAINTS (IF +VE LAMBDA'S)      MAIN7850
C*****MAIN7860
      CALL DISP(R,D,AMDA,NDISP,ICNN)                   MAIN7870
      IF (ICNN,NF,0) GO TO 601                           MAIN7880
      602 WRITE(10,1006) ICNN                            MAIN7890
      WRITE(11) ASTR                                     MAIN7900
      GO TO 971                                          MAIN7910
C*****MAIN7920
C-----CALCULATE REDESIGN FROM DISPLACEMENT CONSTRAINTS                      MAIN7930
C*****MAIN7940
      601 DO 500 I=1,NIMDV                                MAIN7950
      C=0.                                               MAIN7960
      DO 510 J=1,NDISP                                  MAIN7970
      510 C=C+AMDA(J)*DR1(I,J)                          MAIN7980
      DR1ND(I)=C/UW1(I)                                MAIN7990
      C=(ALPA-(1.-ALPA)*DR1ND(I))*AOLD(I)              MAIN8000
      IF (C,GF,ASTR(I)) GO TO 520                      MAIN8010
      IF (D1(I),F0,1) MAC=C                             MAIN8020
      D1(I)=0                                           MAIN8030
      MAIN8040

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      ADIS(I)=ASTP(I)                                MAINR050
      GO TO 500                                        MAINR060
520  ADIS(I)=C                                         MAINR070
      IF (ID1(I).EQ.0) MAC=0                          MAINR080
      ID1(I)=1                                         MAINR090
      500 CONTINUE                                     MAINR100
C*****MAINR110
C-----CHECK FOR ANY CHANGE IN ACTIVE/PASSIVE CLASSIFICATION OF DESIGN  MAINR120
C      VARIABLES                                     MAINR130
C*****MAINR140
      IF (MAC.EQ.0) GO TO 700                          MAINR150
C*****MAINR160
C-----PRINT OPTIMALITY INDEX                        MAINR170
C*****MAINR180
      WRITE(IW,2002)                                    MAINR190
      DO 750 I=1,NUMDV                                MAINR200
      TAG=TAG1                                          MAINR210
      IF (ID1(I).EQ.0) TAG=TAG2                        MAINR220
750  WRITE(IW,2003) I,TAG,OPTIND(I)                  MAINR230
      WRITE(IW,1006) ICN                                MAINR240
      IF (SF.GT.DELTA2.OR.SF.LT.DELTA1) GO TO 701     MAINR250
      IF (DMAX.GT.DELTA2.OR.DMAX.LT.DELTA1) GO TO 701 MAINR260
C*****MAINR270
C-----CHECK FOR DISPLACEMENT DESIGN CONVERGENCE.  MAINR280
C*****MAINR290
      DO 702 I=1,NUMDV                                MAINR300
      IF (ID1(I).EQ.0) GO TO 702                      MAINR310
      C=-OPTIND(I)                                     MAINR320
      IF (C.GT.DELT22.OR.C.LT.DELT11) GO TO 701     MAINR330
702  CONTINUE                                     MAINR340
      KCONVC=4                                         MAINR350
      WRITE(IW,2001)                                    MAINR360
      RETURN                                           MAINR370
C*****MAINR380
C-----CALCULATE SCALE FACTOR FOR UNIFORM SCALING FROM DISPLACEMENT  MAINR390
C      CONSTRAINTS                                  MAINR400
C*****MAINR410
501  DO 503 J=1,NDISP                                MAINR420
      S(J)=0                                           MAINR430
      DO 502 I=1,NUMDV                                MAINR440
502  S(I)=S(I)+OR(I(I,J)*ADID(I))                   MAINR450
503  S(J)=DCON(J)*(1.0-ABS(DRAT(J)))/S(J)+1.         MAINR460
      DF=0.                                            MAINR470
      DO 504 I=1,NDISP                                MAINR480
      IF (S(I).GT.DF) DF=S(I)                         MAINR490
504  CONTINUE                                     MAINR500
      CALL MFSG(SF,DF,DF,IW)                         MAINR510
      IF (DF.GT.SF) SF=DF                             MAINR520
      DO 505 I=1,NUMDV                                MAINR530
505  ADIS(I)=ADID(I)*SF                             MAINR540
      REWIND I1                                       MAINR550
701  WRITE(11) ADIS                                  MAINR560
971  RETURN                                           MAINR570
1006 FORMAT(//1X,42HNO. OF ACTIVE DISPLACEMENT CONSTRAINTS ARE ,I5)  MAINR580
2001 FORMAT(43H DISPLACEMENT-CRITICAL DESIGN HAS CONVERGED //)      MAINR590
2002 FORMAT(//62H OPTIMALITY INDEX OF DESIGN VARIABLES FOR DISPT.  CONMA1NR600
      15TPAINTS //5X,5HNO. NO,1X,7HACT/PAS,4X,5HINDEX //)
2003 FORMAT(5X,I5,A10,F15.5)                                MAINR610
      FND                                           MAINR620
      FND                                           MAINR630

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SUBROUTINE TRISS (A,MTOT)
C*****
C-----THREE DIMENSIONAL BAR ELEMENTS
C*****
      DIMENSION A(MTOT)
      COMMON /FLPAR/ NPAR(14),NIUMNP,MRAND,NELTYP,N1,N2,N3,N4,N5,MTIT,NFO
      1,NIUMFL,NIUMDV,M1,M2,M3,LL,LR,NFOR,NBLNCK
      COMMON/JUNK/JUNK(16),LT,LLH,L,SIG(27),IDVAR,IFX,FRC,AREA,JUN1(250)
      COMMON/INIT/IR,IW,IP,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10,I11,I12
      NIUMF=NPAP(2)
      KODF=NPAP(5)
      IF(NPAR(1),EO,0)GO TO 500
      GO TO (1,1,2),KODF
C*****
C-----KODF =1 INERTIA IS PROPORTIONAL TO AREA FOR LOCAL BUCKLING
C
      2 INERTIA IS PROPORTIONAL TO AREA**2 FOR LOCAL BUCKLING
C*****
      1 NIUMAT=NPAP(3)
      NIUMGF=NPAP(4)
      NIUMTC=NPAP(6)
      NA=N5+NIUMNP
      N7=N6+NIUMAT
      NR=N7+NIUMAT
      N9=NR+NIUMAT*NIUMTC*5
      MM=N9+NIUMGF*2-MTOT
      IF(MM,GT,0)CALL ERROR(MM)
      CALL TRISS (A(M1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),
      1A(N8),A(N9),NIUMDV,NIUMNP,NIUMAT,NIUMTC,NIUMGF,KODF,NIUMF)
      RETURN
C*****
C-----PROVISION FOR SPECIAL TRISS ELEMENT
C*****
      2 CALL NOFLM (NPAR(1),NPAR(5),IW)
      RETURN
500 WRITE (IW,2002) KODF
      DO 800 MM=1,NIUMF
      CALL STPSC(A(M1),A(N1),A(N3),MFO,NIUMDV,LL,LR,IR,0)
      WRITE (IW,2005) MM,AREA
      DO 800 L=LT,LR
      IF(L,GT,LT) WRITE(IW,2004)
      CALL STPSC(A(M1),A(N1),A(N3),MFO,NIUMDV,LL,LR,IR,1)
      WRITE(IW,2003) L,SIG(1)
      GO TO (3,3,4),KODF
C*****
C-----DESIGN OF BAR ELEMENTS FOR STRESS AND LOCAL BUCKLING
C*****
      2 CALL DTRISS (A(M1),A(M2),A(M3),NIUMDV)
      GO TO 800
C*****
C-----PROVISION FOR DESIGN OF SPECIAL TRISS ELEMENT
C*****
      4 CONTINUE
      800 CONTINUE
      RETURN
2002 FORMAT(//42H ANALYSIS OF TRISS ELEMENTS, CUMSTRN CODE=,I2 //
      1 4TH ELEMENT X-SECT AREA LOAD COND AXIAL FORCE /)
2003 FORMAT(1H+,24X,15,4X,F12.4)
2004 FORMAT(/)
2005 FORMAT(17,2X,F12.4)
      END

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TRIS0000
TRIS0010
TRIS0020
TRIS0030
TRIS0040
TRIS0050
TRIS0060
TRIS0070
TRIS0080
TRIS0090
TRIS0100
TRIS0110
TRIS0120
TRIS0130
TRIS0140
TRIS0150
TRIS0160
TRIS0170
TRIS0180
TRIS0190
TRIS0200
TRIS0210
TRIS0220
TRIS0230
TRIS0240
TRIS0250
TRIS0260
TRIS0270
TRIS0280
TRIS0290
TRIS0300
TRIS0310
TRIS0320
TRIS0330
TRIS0340
TRIS0350
TRIS0360
TRIS0370
TRIS0380
TRIS0390
TRIS0400
TRIS0410
TRIS0420
TRIS0430
TRIS0440
TRIS0450
TRIS0460
TRIS0470
TRIS0480
TRIS0490
TRIS0500
TRIS0510
TRIS0520
TRIS0530
TRIS0540
TRIS0550
TRIS0560
TRIS0570
TRIS0580
TRIS0590

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SUBROUTINE RUSS (IWT, ID, X, Y, Z, I, NTC, WT, PMAT, PGFN, NUMDV, NUMNP,      TRUS0600
1 NUMMAT, NUMTC, NUMGEO, KODF, NUIMF)      TRUS0610
C*****      TRUS0620
C-----INIFORM CROSS SECTION BAR ELEMENTS      TRUS0630
C*****      TRUS0640
IMPLICIT REAL*8 (A-H, O-Z)      TRUS0650
REAL*4 X, Y, Z, I, WT, PMAT, PGFN, IWT, FPC, RUCKYY, RUCKZZ, EE3, EF4      TRUS0660
DIMENSION ID (NUMNP, 6), X (NUMNP), Y (NUMNP), Z (NUMNP), T (NUMNP),      TRUS0670
1 NTC (NUMMAT), WT (NUMMAT), PMAT (NUMTC, 5, NUMMAT), PGFN (NUMGEO, 2),      TRUS0680
2 IWT (NUMDV)      TRUS0690
COMMON/EM/LM(6), S(6, 6), P(6, 4), ST(6), IT(4), XM(6), EM1(2454)      TRUS0700
COMMON/JUNK/FMUL(4, 4), FE(4), RHO, TEMP, XX(2), YY(2), ZZ(2), V(4),      TRUS0710
1 JUNK(236)      TRUS0720
COMMON/UNITS/IR, IW, IP, I1, I2, I3, I8, I9, I10, I11, I12      TRUS0730
C*****      TRUS0740
C-----CONTROL INFORMATION      TRUS0750
C*****      TRUS0760
MI=1      TRUS0770
NV=1      TRUS0780
MW=1      TRUS0790
ND=6      TRUS0800
NS=1      TRUS0810
NJ=4      TRUS0820
IFX=KODF      TRUS0830
WRITE(IW, 2000) NUIMF, KODF, NUMMAT, NUMTC, NUMGEO      TRUS0840
C*****      TRUS0850
C-----MATERIAL PROPERTY CARDS      TRUS0860
C*****      TRUS0870
WRITE(IW, 2001)      TRUS0880
DO 10 I=1, NUMMAT      TRUS0890
READ (IR, 1001) N, NTC(N), WT(N)      TRUS0900
IF (NTC(N), EQ, 0) NTC(N)=1      TRUS0910
WRITE(IW, 2002) N, NTC(N), WT(N)      TRUS0920
C*****      TRUS0930
C-----TEMPERATURE DEPENDENT MATERIAL PROPERTIES      TRUS0940
C*****      TRUS0950
NI=NTC(N)      TRUS0960
DO 10 J=1, NI      TRUS0970
READ (IR, 2008) (PMAT(J, K, N), K=1, 5)      TRUS0980
IF (PMAT(J, 5, N), LE, 0) PMAT(J, 5, N)=PMAT(J, 4, N)      TRUS0990
IF (J, NE, 1) WRITE(IW, 2009)      TRUS1000
10 WRITE (IW, 2010) (PMAT(J, K, N), K=1, 5)      TRUS1010
C*****      TRUS1020
C-----GEOMETRIC PROPERTY CARDS      TRUS1030
C*****      TRUS1040
WRITE(IW, 2004)      TRUS1050
DO 51 I=1, NUMGEO      TRUS1060
READ (IR, 1006) N, ARFA, (PGFN(N, J), J=1, 2)      TRUS1070
IF (ARFA, LE, 0) ARFA=1.0      TRUS1080
DO 80 J=1, 2      TRUS1090
80 IF (PGFN(N, J), LE, 0) PGFN(N, J)=1000000.      TRUS1100
WRITE(IW, 2007) N, ARFA, (PGFN(N, J), J=1, 2)      TRUS1110
AA=ARFA**IFX      TRUS1120
DO 51 J=1, 2      TRUS1130
51 PGFN(N, J)=0.8696*PGFN(N, J)/AA      TRUS1140
C*****      TRUS1150
C-----ELEMENT LOAD INITIALIERS      TRUS1160
C*****      TRUS1170
READ (IR, 1003) FMUL      TRUS1180
WRITE(IW, 2003) FMUL      TRUS1190

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C*****TRUS1200
C-----ELEMENT CARDS                                     TRUS1210
C*****TRUS1220
      WRITE(IW,2005)                                     TRUS1230
      N=1                                                 TRUS1240
      100 READ(IR,1004) IF1,II,IJ,IMAT,IGEN,INDV ,FRC,RFFT,ELPHY,FLPZZ,INC TRUS1250
      IF(IF1.LT.N) GO TO 700                             TRUS1260
      IF(FRC.LE.0.0) FRC=1.0                             TRUS1270
      IF(INC.F0.0) INC=1                                  TRUS1280
      IF(ELPHY.I.F.0.0) ELPYY=1.0                       TRUS1290
      IF(FLPZZ.LF.0.0) FLPZZ=1.0                       TRUS1300
      KK=INC*(IF1-N)                                     TRUS1310
      I=I-KK                                             TRUS1320
      J=J-KK                                             TRUS1330
      DO 500 NFI=N,IF1                                  TRUS1340
      XX(1)=X(I)                                         TRUS1350
      XX(2)=X(J)                                         TRUS1360
      YY(1)=Y(I)                                         TRUS1370
      YY(2)=Y(J)                                         TRUS1380
      ZZ(1)=Z(I)                                         TRUS1390
      ZZ(2)=Z(J)                                         TRUS1400
C*****TRUS1410
C-----INTERPOLATE MATERIAL PROPERTIES FOR AVERAGE ELEMENT TEMPERATURE TRUS1420
C*****TRUS1430
      TEMP=0.5*(T(I)+T(J))                               TRUS1440
      CALL INTERP(PMAT,FF,NUM1C,NUMMAT,5,4,NTC(IMAT),IMAT,TEMP) TRUS1450
C*****TRUS1460
C-----FORM ELEMENT UNIT MATRICES AND LOAD VECTORS      TRUS1470
C*****TRUS1480
      RHO=WT(IMAT)                                       TRUS1490
      TEMP=TEMP-RFFT                                     TRUS1500
      CALL FTRUSS                                         TRUS1510
      HH=FF(I)/(V(4)*V(4))                               TRUS1520
      BUCKYY=PGEN(IGEN,1)*HH*ELPHY                      TRUS1530
      BUCKZZ=PGEN(IGEN,2)*HH*ELPZZ                      TRUS1540
      FF3=FF(3)                                           TRUS1550
      FF4=FF(4)                                           TRUS1560
      IWT(INDV)=IWT(INDV)+RHO*V(4)*FRC                 TRUS1570
C*****TRUS1580
C-----FORM LOCATION MATRIX AND COMPUTE BAND WIDTH      TRUS1590
C*****TRUS1600
      DO 400 L=1,3                                       TRUS1610
      LM(L)=ID(I,L)                                     TRUS1620
      400 LM(L+3)=ID(J,L)                                TRUS1630
      CALL CALBAN(NDIF,LM,S,P,ST,T),NU,NV,NS,ND,NW,(INDV,IFX,FRC) TRUS1640
      WRITE(IR) NI,BUCKYY,BUCKZZ,FF3,FF4               TRUS1650
      WRITE(IW,2004) NFI,I,J,IMAT,IGEN,INDV,FRC,RFFT,ELPHY,FLPZZ,NDIF TRUS1660
C*****TRUS1670
C-----CHECK FOR MORE ELEMENTS                          TRUS1680
C*****TRUS1690
      I=I+INC                                             TRUS1700
      J=J+INC                                             TRUS1710
      500 CONTINUE                                       TRUS1720
      N=IF1+1                                             TRUS1730
      IF(N.LE.NUMF) GO TO 100                             TRUS1740
      RETURN                                             TRUS1750
      700 WRITE(IW,2011)                                  TRUS1760
      STOP                                              TRUS1770
      1001 FORMAT(2I5,F10.0)                             TRUS1780
      1003 FORMAT(4F10.0)                                TRUS1790

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1004 FORMAT(16,5,4F10.0,15)
1006 FORMAT(15,5X,3F10.0)
2000 FORMAT(44H)NUMBER OF TRUSS ELEMENTS =,15/
1 44H CONSTRUCTION CODE =,15/
2 44H NUMBER OF MATERIALS =,15/
3 44H NUMBER OF TEMPS FOR WHICH MAIL PROPS GIVEN=,15/
4 44H NUMBER OF DIFFERENT GEOMETRIES PROPS GIVEN=,15/
2001 FORMAT(/ 25H MATERIAL PROPERTY CARDS //
191H MATERIAL NUMBER SPECIFIC YOUNGS COEFFT
2 OF /--ALLOWABLE STRESSES--/ /
391H NUMBER OF TEMPS WEIGHT IFMP MODULUS THERM E
4XPAN TENSION COMPRESSION /)
2002 FORMAT(16,5X,15,F12.4)
2003 FORMAT(/ 25H ELEMENT LOAD MULTIPLIERS / 20X,1HA,14X,1HB,14X,1HC,
1 14X,1HD,16H X-DIR,4F15.6/ 6H Y-DIR,4F15.6/ 6H Z-DIR,4F15.6/
2 6H IFMP,4F15.6)
2004 FORMAT(17,1X,5I7,4F13.4,17)
2005 FORMAT(/ 23H PROCESSED ELEMENT DATA//
1116H ELEMENT /-NODE NOS-/ /--ELEMENT ID NOS-/ DESIGN VAR REF
2RENCE END FIXITY COEFFICIENTS BAND /
3116H NUMBER I J MATL GEOMY D VAR FRACTION
4FMP YY ZZ WIDTH /)
2006 FORMAT(/ 25H GEOMETRIC PROPERTY CARDS//
146H GEOMETRY X-SFCT /--MOMENTS OF INERTIA--/ /
245H NUMBER AREA YY ZZ /)
2007 FORMAT(16,2X,3F12.4)
2008 FORMAT(5F10.0)
2009 FORMAT(/)
2010 FORMAT(1H,30X,5F12.4)
2011, FORMAT(28H TRUSS ELEMENT CARD IN ERROR )
END

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TRUS1800
 TRUS1810
 TRUS1820
 TRUS1830
 TRUS1840
 TRUS1850
 TRUS1860
 TRUS1870
 TRUS1880
 TRUS1890
 TRUS1900
 TRUS1910
 TRUS1920
 TRUS1930
 TRUS1940
 TRUS1950
 TRUS1960
 TRUS1970
 TRUS1980
 TRUS1990
 TRUS2000
 TRUS2010
 TRUS2020
 TRUS2030
 TRUS2040
 TRUS2050
 TRUS2060
 TRUS2070
 TRUS2080
 TRUS2090
 TRUS2100

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SHARDLINE TRUSS
C*****
C-----FORM TRUSS ELEMENT MATRICES
C*****
IMPLICIT REAL*8 (A-H,O-7)
COMMON/FM/LM(6),S(6,6),P(6,4),ST(6),TT(4),XM(6),EM(12454)
COMMON/JUNK/FMU(4,4),F(4),RHO,IFMP,X(2),Y(2),Z(2),V(4),JUN(236)
DIMENSION FMM(76)
EQUIVALENCE (S,FMM)
DO 5 I=1,76
5 FMM(I)=0.
C*****
C-----COMPUTE UNIT STIFFNESS AND LOAD MATRICES
C*****
CALL VECTDR (V,X(1),Y(1),Z(1),X(2),Y(2),Z(2))
DO 10 I=1,3
ST(I)=-V(I)/V(4)
10 ST(I+3)=-ST(I)
DO 200 L=1,6
YY=ST(L)*F(1)*V(4)
DO 250 K=L,6
S(K,L)=ST(K)*YY
250 S(L,K)=S(K,L)
300 ST(L)=F(1)*ST(L)

```

TRUS2110
 TRUS2120
 TRUS2130
 TRUS2140
 TRUS2150
 TRUS2160
 TRUS2170
 TRUS2180
 TRUS2190
 TRUS2200
 TRUS2210
 TRUS2220
 TRUS2230
 TRUS2240
 TRUS2250
 TRUS2260
 TRUS2270
 TRUS2280
 TRUS2290
 TRUS2300
 TRUS2310
 TRUS2320
 TRUS2330
 TRUS2340

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C*****TRUS2350
C-----GRAVITY AND THERMAL LOADS      TRUS2360
C*****TRUS2370
      FT=-TFMP*F(1))*F(2)      TRUS2380
      F=0.5*RH0*V(4)      TRUS2390
      DO 350 I=1,4      TRUS2400
      HH=FMUL(I,4)*F1      TRUS2410
      TT(I)=HH      TRUS2420
      DO 350 M=1,3      TRUS2430
      P(M,I)=FMUL(I,M)*F+HH*V(M)      TRUS2440
350 P(M+3,I)=FMUL(I,M)*F-HH*V(M)      TRUS2450
      RETURN      TRUS2460
      END      TRUS2470

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SUBROUTINE DTRUSS( APLD, ANEW, L0AD, NUMDV) TRUS2480
C***** TRUS2490
C-----FULLY STRESSSED DESIGN FOR TRUSS ELEMENTS TRUS2500
C***** TRUS2510
DIMS ION APLD( NUMDV), ANEW( NUMDV), L0AD( NUMDV) TRUS2520
COMMON/ JUNK / JIN( 16), L, T, L, L, SG( 27), IDVAR, IFX, FRC, ARFA, XINFR1, RYY, TRUS2530
1 R7Z, TENS, COP1, JIN1( 245) TRUS2540
P=SG( 1) TRUS2550
IF( P.GT.0.0) GO TO 100 TRUS2560
P1=COP1*ARFA TRUS2570
P2=0.5*P1 TRUS2580
P=-P TRUS2590
PFY=XINFR1*RYY TRUS2600
XLY=P/PFY TRUS2610
RMAX=SORT( XLY) TRUS2620
CALL JONNS ( IFX, P, P1, P2, PFY, P) TRUS2630
IF ( R.GT.RMAX) RMAX=R TRUS2640
PF7=XINFR1*R7Z TRUS2650
XL7=P/PF7 TRUS2660
R=SORT( XL7) TRUS2670
IF ( R.GT.RMAX) RMAX=R TRUS2680
CALL JONNS ( IFX, P, P1, P2, PF7, R) TRUS2690
IF ( R.GT.RMAX) RMAX=R TRUS2700
GO TO 118 TRUS2710
100 P1=TENS*ARFA TRUS2720
RMAX=P/P1 TRUS2730
118 AA=RMAX*APLD( IDVAR) TRUS2740
IF( AA.L.T.ANEW( IDVAR)) GO TO 60 TRUS2750
ANEW( IDVAR)=AA TRUS2760
L0AD( IDVAR)=L TRUS2770
60 CONTINUE TRUS2780
RETURN TRUS2790
END TRUS2800

```

```

SUBROUTINE JONNS ( I, A, B, C, D, AA) TRUS2810
C***** TRUS2820
C-----JONNSON'S PARABOLA USED FOR REDESIGN UNDER COMPRESSIVE FORCE TRUS2830
C***** TRUS2840
GO TO ( 1, 2, 3), I TRUS2850
1 AA=B-( B-C)*C/D TRUS2860
IF ( AA.L.T.0.00001) GO TO 50 TRUS2870
AA=A/AA TRUS2880
RETURN TRUS2890
50 AA=0.0 TRUS2900
RETURN TRUS2910
2 AA=( A+ ( B-C)*C/D) /B TRUS2920
RETURN TRUS2930
3 AA=SORT( A**2+ ( 4*B*C*( B-C)/D)) TRUS2940
AA=( AA+A) /2/B TRUS2950
RETURN TRUS2960
END TRUS2970

```

```

SURROUNDING BEAM(A,MTOT)
C*****
C-----THREE DIMENSIONAL BEAM ELEMENTS
C*****
      DIMENSION A(MTOT)
      COMMON /FLPAR/ NPAR(14),NUMNP,MBAND,NFL1YP,N1,N2,N3,N4,N5,MITT,NFOR,MBLOCK
      1,NIMF1,NIMDV,M1,M2,M3,LL,LR,NFOR,NBLOCK
      COMMON/JUNK/JUN1(16),LT,LH,L,SIG(27),IDVAR,IFX,FRC,ARFA,JUN1(250)
      COMMON/UNIT/IR,IW,IP,IJ,I2,I3,IR,I9,I10,I11,I12
      NIME=NPAR(2)
      KODE=NPAR(5)
      IF(NPAR(1),FO,0) GO TO 500
      GO TO (1,1,2),KODE
C*****
C-----BEAM ELEMENTS WITH INSTABILITY CONSTRAINTS
C-----KODE =1 INERTIAS AND MODULI ARE PROPORTIONAL TO ARFA
C          2 INERTIAS AND MODULI ARE PROPORTIONAL TO ARFA**2 AND
C          ARFA**1.5 RESPECTIVELY
C*****
      1 NIMMAT=NPAR(3)
      NIMGFD=NPAR(4)
      NIMFIX=NPAR(6)
      IF (NIMFIX,FO,0) NIMFIX=1
      N6=N5+NUMNP
      N7=N6+NIMGFD
      NR=N7+NIMGFD*9
      NO=NR+NIMMAT
      N10=NR+NIMMAT*5
      MM=N10+NIMFIX*12-MTOT
      IF(MM,GT,0)CALL ERRPR(MM)
      CALL TFAM (A(M1),A(N1),A(N2),A(N3),A(N4),A(N6),A(N7),A(NR),A(N9),
      1A(N10),NUMDV,NIMNP,NIMGFD,NIMMAT,NIMFIX,KODE,NIME,NPAR(16))
      RETURN
C*****
C-----PROVISION FOR SPECIAL BEAM ELEMENTS
C*****
      2 CALL NDFLEMINPAR(1),KODE,IW)
      RETURN
      500 WRITE (IW,2008) KODE
      DO 800 MM=1,NIME
      CALL STRSC(A(M1),A(N1),A(N3),NFO,NIMDV,LL,LR,IR,0)
      WRITE (IW,2005) MM,ARFA
      DO 800 L=LT,LH
      CALL STRSC(A(M1),A(N1),A(N3),NFO,NIMDV,LL,LR,IR,1)
      IF(L,GT,1) WRITE(IW,2006)
      WRITE(6,2007) L,(SIG(I),I=1,12)
      GO TO (3,3,4),KODE
C*****
C-----DESIGN OF BEAM ELEMENTS FOR STRESS AND LOCAL BUCKLING CONSTRAINTS
C*****
      3 CALL DBEAM(A(M1),A(M2),A(M3),NUMDV)
      GO TO 800
C*****
C-----PROVISION FOR REDSIGN OF SPECIAL BEAM ELEMENTS
C*****
      4 CONTINUE
      800 CONTINUE
      RETURN
      2005 FORMAT(17,F13.4)
      2006 FORMAT(1)

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BFAM0000
BFAM0010
BFAM0020
BFAM0030
BFAM0040
BFAM0050
BFAM0060
BFAM0070
BFAM0080
BFAM0090
BFAM0100
BFAM0110
BFAM0120
BFAM0130
BFAM0140
BFAM0150
BFAM0160
BFAM0170
BFAM0180
BFAM0190
BFAM0200
BFAM0210
BFAM0220
BFAM0230
BFAM0240
BFAM0250
BFAM0260
BFAM0270
BFAM0280
BFAM0290
BFAM0300
BFAM0310
BFAM0320
BFAM0330
BFAM0340
BFAM0350
BFAM0360
BFAM0370
BFAM0380
BFAM0390
BFAM0400
BFAM0410
BFAM0420
BFAM0430
BFAM0440
BFAM0450
BFAM0460
BFAM0470
BFAM0480
BFAM0490
BFAM0500
BFAM0510
BFAM0520
BFAM0530
BFAM0540
BFAM0550
BFAM0560
BFAM0570
BFAM0580
BFAM0590

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2007 FORMAT(1H+,20X,15.6X,6F12.4/32X,6F12.4)          RFAM0600
2008 FORMAT(/41H ANALYSIS OF BEAM ELEMENTS, CONSTN CODE= ,12// RFAM0610
      1104H ELEMENT X-SECT AREA LOAD COND AXIAL RX SHFAR RY SHFRFAM0620
      2AR RZ TORQUE MX MOMENT MY MOMENT MZ /)          RFAM0630
      FND                                              RFAM0640

      SUBROUTINE TEAM(IWT,ID,X,Y,Z,KSEC,PGFN,WT,PMAT,SFT,NUMDV,NUMNP, RFAM0650
      )NUMGFN,NUMMAT,NUMFX,KODE,NUMF,NUMFX)          RFAM0660
C*****RFAM0670
C-----INFORM CROSS-SECTION BEAM ELEMENTS          RFAM0680
C*****RFAM0690
      IMPLICIT REAL*8 (A-H,O-Z)          RFAM0700
      REAL*8 IWT,X,Y,Z, PGFN, PMAT,SFT,FRC          RFAM0710
      DIMENSION IWT(NUMDV),ID(NUMNP),X(NUMNP),Y(NUMNP),Z(NUMNP), RFAM0720
      1 KSEC(NUMGFN), PGFN (NUMGFN,9),PMAT(NUMMAT,6),SFT(NUMFX,12) RFAM0730
      2 ,WT(NUMMAT)          RFAM0740
      COMMON/FM/LM(24),S(24,24,2),P(24,4,2),ST(12,24,2),TT(12,4,2), RFAM0750
      1 XM(24),FM(481)          RFAM0760
      COMMON/JUNK/FMUL(3,4),T(3,3),LC(4),JC(12),XX(3),YY(3),ZZ(3),IE(3), RFAM0770
      1 IX(3),II(3),OIL,JUN(210)          RFAM0780
      COMMON/JNITS/IR,IW,IP,IL,I2,I3,I8,I9,I10,I11,I12          RFAM0790
C*****RFAM0800
C-----CONTROL INFORMATION          RFAM0810
C*****RFAM0820
      NI=2          RFAM0830
      NV=2          RFAM0840
      NS=12          RFAM0850
      NW=2          RFAM0860
      IFX=KODE          RFAM0870
      NI=10          RFAM0880
      WRITE(IW,2005) NUMF,KODE,NUMMAT,NUMGFN,NUMFX          RFAM0890
C*****RFAM0900
C-----MATERIAL PROPERTY CARDS          RFAM0910
C*****RFAM0920
      WRITE(IW,2001)          RFAM0930
      DO 30 J=1,NUMMAT          RFAM0940
      READ(IR,1001) N,WT(N),(PMAT(N,J),J=1,5)          RFAM0950
      IF(PMAT(N,4).LE.0.) PMAT(N,4)=PMAT(N,3)          RFAM0960
      IF(PMAT(N,5).LE.0.) PMAT(N,5)=0.577*PMAT(N,3)          RFAM0970
      WRITE(IW,2002) N,WT(N),(PMAT(N,J),J=1,5)          RFAM0980
      10 PMAT(N,2)=0.5*PMAT(N,1)/(1.0+PMAT(N,2))          RFAM0990
C*****RFAM1000
C-----GEOMETRIC PROPERTY CARDS          RFAM1010
C*****RFAM1020
      WRITE(IW,2003)          RFAM1030
      DO 30 J=1,NUMGFN          RFAM1040
      READ(IR,1002) N,KSEC(N),AREA,( PGFN (N,I),I=1,9)          RFAM1050
      IF(AREA.LE.0.) AREA=1.0          RFAM1060
      IF(KSEC(N).EQ.0.) KSEC(N)=1          RFAM1070
      IF(KSEC(N).NE.3) GO TO 15          RFAM1080
      PGFN(N,3)=PGFN(N,2)          RFAM1090
      PGFN(N,6)=0.          RFAM1100
      PGFN(N,7)=0.          RFAM1110
      PGFN(N,8)=0.          RFAM1120
      PGFN(N,9)=0.          RFAM1130
      15 WRITE(IW,2004) N,KSEC(N),AREA,( PGFN (N,I),I=1,9)          RFAM1140
      AA=AREA**IFX          RFAM1150
      AAA=0.5*AA**AA          RFAM1160
      DO 11 I=1,3          RFAM1170

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11 PGFN(N,I)=PGFN(N,I)/AA RFAM1180
   DO 12 J=4,9 RFAM1190
12 PGFN(N,I)=PGFN(N,I)/AAA RFAM1200
30 CONTINUE RFAM1210
C***** RFAM1220
C-----ELEMENT LOAD MULTIPLIERS RFAM1230
C***** RFAM1240
      READ (IR,1006) (FMIL(I,J),J=1,4),I=1,3) RFAM1250
      WRITE(IW,2006) (FMIL(I,J),J=1,4),I=1,3) RFAM1260
C***** RFAM1270
C-----FIXED-END FORCES RFAM1280
C***** RFAM1290
      IF(NUMEX.FO.O) GO TO 56 RFAM1300
      WRITE(IW,2010) RFAM1310
      DO 55 J=1,NUMEX RFAM1320
      READ (IR,1005) N,(SFT(N,J),J=1,12) RFAM1330
      55 WRITE(IW,2011) N,(SFT(N,J),J=1,12) RFAM1340
C***** RFAM1350
C-----ELEMENT CARDS RFAM1360
C***** RFAM1370
      56 WRITE(IW,4000) RFAM1380
      N=1 RFAM1390
100 READ(IR,3000) IFL,IF,IMAT,IGFO,IOV ,FRC,I.C.,IC,INC RFAM1400
      IF(FRC.LF.O.) FRC=1. RFAM1410
      IF(INC.FO.O) INC=1 RFAM1420
      KK=INC*(IFL-N) RFAM1430
      IX(1)=IF(1)-KK RFAM1440
      IX(2)=IF(2)-KK RFAM1450
      IX(3)=IF(3) RFAM1460
      DO 500 NFL=N,IFL RFAM1470
      DO 120 I=1,3 RFAM1480
      II=IX(1) RFAM1490
      XX(I)=X(II) RFAM1500
      YY(I)=Y(II) RFAM1510
      120 Z(I)=Z(II) RFAM1520
C***** RFAM1530
C-----COMPUTE ELEMENT MATRICES RFAM1540
C***** RFAM1550
      RHO=WT(IMAT) RFAM1560
      F =PMAT(IMAT,1) RFAM1570
      G =PMAT(IMAT,2) RFAM1580
      AAX=PGFN(IGFO,1) RFAM1590
      AAY=PGFN(IGFO,2) RFAM1600
      AA7=PGFN(IGFO,3) RFAM1610
      CALL NEWRM(F,G,RHO,AAX,AAY,AA7,SFT,NUMEX,NFL,IW) RFAM1620
      IWT(IOV)=IWT(IOV)+N1*RHO*FRC RFAM1630
C***** RFAM1640
C-----FORM ELEMENT LOCATION MATRIX RFAM1650
C***** RFAM1660
      I=IX(1) RFAM1670
      J=IX(2) RFAM1680
      DO 170 M=1,6 RFAM1690
      LM(M)=ID(I,M) RFAM1700
      LM(M+12)=0 RFAM1710
      LM(M+18)=0 RFAM1720
      170 LM(M+6)=ID(J,M) RFAM1730
C***** RFAM1740
C-----TRANSFORM TO MASTER DEGREES OF FREEDOM AND REARRANGE MATRICES RFAM1750
C***** RFAM1760
      ND=12 RFAM1770

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CALL SLAVE (X,Y,Z,TD,NUMNP,IX(1),IX(2),ND,NS)          RFAM1780
NN=ND*ND*NNI          RFAM1790
CALL RFARAN( S, S,24,24,2,ND,ND,NN,NN)          RFAM1800
NN=NS*ND*NNI          RFAM1810
CALL RFARAN(ST,ST,12,24,2,NS,ND,NN,NN)          RFAM1820
NN=ND*4*NV          RFAM1830
CALL RFARAN( P, P,24, 4,2,ND, 4,NV,NN)          RFAM1840
C*****RFAM1850
C-----PLACE ELEMENT INFORMATION ON TAPES          RFAM1860
C*****RFAM1870
CALL CALBAN(NDIF,IM,S,P,ST,TT,NN,NV,NS,ND,NW,INDV,TEX,FRC)          RFAM1880
WRITE(18) NI,(PGFN(IGFN,I),I=4,9),(PMAT(IMAT,I),I=3,5),KSEC(IGEN)          RFAM1890
WRITE (18,4001) NFL,IX,IMAT,IGFN,INDV ,FRC,LC,JC,NDIF          RFAM1900
C*****RFAM1910
C-----CHECK FOR LAST ELEMENT          RFAM1920
C*****RFAM1930
IX(1)=IX(1)+INC          RFAM1940
IX(2)=IX(2)+INC          RFAM1950
500 CONTINUE          RFAM1960
N=IFL+1          RFAM1970
IF(N,LF,NUMP) GO TO 100          RFAM1980
RETURN          RFAM1990
1001 FORMAT(15,5X,6F10.0)          RFAM2000
1002 FORMAT(215,4F10.0/6F10.0)          RFAM2010
1005 FORMAT(15,6F10.0/5F10.0)          RFAM2020
1006 FORMAT(4F10.0)          RFAM2030
2001 FORMAT(// 25H MATERIAL PROPERTY CARDS //          RFAM2040
183H MATERIAL SPECIFIC YOUNGS POISSONS /-----ALLOWAB          RFAM2050
2LF STRESSES-----/ /          RFAM2060
383H NUMBER WEIGHT MODULUS RATIO TENSION COM          RFAM2070
4PRESSION SHEAR //          RFAM2080
2002 FORMAT(16,4X,6F12.4)          RFAM2090
2003 FORMAT(// 25H GEOMETRIC PROPERTY CARDS//          RFAM2100
166H PROPERTY X-SECT X-SECT /-----PROPERTIES OF X-SECTION----          RFAM2110
2-/ /          RFAM2120
366H NUMBER KMOD AREA X-AXIS Y-AXIS Z-AXIS          RFAM2130
4 /)          RFAM2140
2004 FORMAT(16,4X,15,4F12.4,22H MOMENTS OF INERTIA /          RFAM2150
1 27X,3F12.4,24H SECT MODULI FOR POINT A/          RFAM2160
2 27X,3F12.4,24H SECT MODULI FOR POINT B)          RFAM2170
2005 FORMAT(32H)THREE DIMENSIONAL BEAM ELEMENTS//          RFAM2180
1 32H NUMBER OF BEAM ELEMENTS =,15/          RFAM2190
2 32H CONSTRUCTION CODE =,15/          RFAM2200
3 32H NUMBER OF MATERIALS =,15/          RFAM2210
4 32H NUMBER OF GEOMETRIC PROPERTIES=,15/          RFAM2220
5 32H NUMBER OF FIXED-END FORCE SETS=,15)          RFAM2230
2006 FORMAT(// 25H ELEMENT LOAD MULTIPLIERS / 20X,1HA,14X,1HR,14X,1HC,          RFAM2240
1 14X,1HD,/6H X-DIR,4F15.6/ 6H Y-DIR,4F15.6/ 6H Z-DIR,4F15.6/ )          RFAM2250
2010 FORMAT(11H)40H FIXED END FORCES IN LOCAL COORDINATES          RFAM2260
1//50H TYPE MODF FORCE X FORCE Y FORCE Z          RFAM2270
2 35H MOMENT X MOMENT Y MOMENT Z          RFAM2280
2011 FORMAT(1H ,13,6X,1H1,3X,6F12.3/1H ,9X,1H1,3X,6F12.3/)          RFAM2290
3000 FORMAT(715,F10.0,415,1211,13)          RFAM2300
4000 FORMAT(// 23H PROCESSED ELEMENT DATA//          RFAM2310
1 106H ELEMENT /---NODE NOS---/ /---ELEMENT ID NOS-/ DESIGN VAR          RFAM2320
2 FIXED END-FORCE IN END RELEASE CODES RAND /          RFAM2330
3 107H NUMBER J J K MATL GFORMY D VAR FRACTION          RFAM2340
4 A B C D I J WIDTH /)          RFAM2350
4001 FORMAT(17,2X,315,317,F12.4,2X,415,5X,611,5X,611,1A)          RFAM2360
END          RFAM2370

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      SUBROUTINE NEWRM (F,G,W1,AAZ,AAZ,SFT,NUMFIX,NFL,IW)      BFAM2380
C*****BFAM2390
C-----CALCULATE ELEMENT MATRICES      BFAM2400
C*****BFAM2410
      IMPLICIT REAL*8 (A-H,O-Z)      BFAM2420
      REAL*4 SFT      BFAM2430
      COMMON/EM/LM(24),S1(24,24),S2(24,24),P1(24,4),P2(24,4),ST1(12,24),BFAM2440
1 ST2(12,24),T1(12,4),TT2(12,4),XM(24),S(12,12),FM1(337)      BFAM2450
      COMMON/JUNK/FMUL(3,4),T(3,3),LC(4),JC(12),XX(3),YY(3),ZZ(3),IE(3),BFAM2460
1 JX(3),U(4),V(4),W(4),R(12),JUN(170)      BFAM2470
      DIMENSION SFT(NUMFIX,12),FMM(12184)      BFAM2480
      EQUIVALENCE (S),FMM)      BFAM2490
      DO 5 I=1,2184      BFAM2500
5 FMM(I)=0.      BFAM2510
C*****BFAM2520
C-----FORM GLOBAL TO LOCAL COORDINATE TRANSFORMATION.      BFAM2530
C*****BFAM2540
      CALL VECTOR(U,XX(1),YY(1),ZZ(1),XX(2),YY(2),ZZ(2))      BFAM2550
      CALL VECTOR(V,XX(1),YY(1),ZZ(1),XX(3),YY(3),ZZ(3))      BFAM2560
      HH=DOT(U,V)      BFAM2570
      IF(DABS(HH)-1.0).LT.0.01) GO TO 40      BFAM2580
      CALL CROSS(U,V,W)      BFAM2590
      CALL CROSS(W,U,V)      BFAM2600
      DO 30 I=1,3      BFAM2610
      T(1,I)=U(I)      BFAM2620
      T(2,I)=V(I)      BFAM2630
30 T(3,I)=W(I)      BFAM2640
C*****BFAM2650
C-----FIXED END FORCES IN LOCAL COORDINATES      BFAM2660
C*****BFAM2670
      DO 73 N=1,4      BFAM2680
      M=LC(N)      BFAM2690
      IF(M.LE.0) GO TO 73      BFAM2700
      DO 72 I=1,12      BFAM2710
72 TT2(I,M)=SFT(M,I)      BFAM2720
73 CONTINUE      BFAM2730
C*****BFAM2740
C-----ELEMENT UNIT STIFFNESS MATRIX IN LOCAL COORDINATES S(I,J)      BFAM2750
C*****BFAM2760
      DL=U(4)      BFAM2770
      ZY=F/(DL*DL)      BFAM2780
      COMMON ZY*AAZ      BFAM2790
      COMMON ZY*AAZ      BFAM2800
      S(1,1)=F/DL      BFAM2810
      S(2,2)= COMMON ZY*12./DL      BFAM2820
      S(3,3)= COMMON ZY*12./DL      BFAM2830
      S(4,4)=G*AAZ/DL      BFAM2840
      S(5,5)= COMMON ZY* 4.*DL      BFAM2850
      S(6,6)= COMMON ZY* 4.*DL      BFAM2860
      S(2,6)= COMMON ZY* 6.      BFAM2870
      S(3,6)= -COMMON ZY* 6.      BFAM2880
      DO 102 I=1,6      BFAM2890
      J=I+6      BFAM2900
102 S(J,I)=S(I,J)      BFAM2910
      DO 104 I=1,4      BFAM2920
      J=I+6      BFAM2930
104 S(I,J)=-S(J,I)      BFAM2940
      S(5,11)= S(5,5)*0.5      BFAM2950
      S(6,12)= S(6,6)*0.5      BFAM2960
      S(2,12)= S(2,6)      BFAM2970

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      S(6, 8)=-S(2,6)
      S(8,12)=-S(2,6)
      S(3,11)= S(3,5)
      S(5, 9)=-S(3,5)
      S(9,11)=-S(3,5)
      DO 106 I=2,12
      K=I-1
      DO 106 J=1,K
      106 S(I,J)=S(J,I)
C*****
C-----MODIFY S AND T2 FOR ZERO END-FORCES
C*****
      DO 140 I=1,12
      SI=S(I,I)
      IF(I.C(1),L.F.O.O.R.SI.F.O.O.) GO TO 140
      DO 125 N=1,12
      125 R(N)=S(I,N)
      DO 126 N=1,4
      126 W(N)=T2(I,N)
      DO 135 M=1,12
      CM=S(M,I)/SI
      DO 130 N=1,12
      130 S(M,N)=S(M,N)-CM*R(N)
      DO 135 N=1,4
      135 T2(M,N)=T2(M,N)-CM*W(N)
      140 CONTINUE
C*****
C-----UNIT STIFFNESS AND FORCE RECOVERY MATRICES DUE TO STRETCHING
C*****
      DO 200 I=1,3
      DO 201 J=1,3
      X=T(1,1)*T(1,J)
      S1(I ,J )=X*S(1,1)
      S1(I ,J+6)=X*S(1,7)
      S1(I+6,J )=X*S(7,1)
      201 S1(I+6,J+6)=X*S(7,7)
      S11(I ,I )=T(1,1)*S(1,1)
      X=T(1,1)*S(1,7)
      S11(I ,I+6)=X
      S11(7 ,I )=X
      200 S11(7 ,I+6)=T(1,1)*S(7,7)
      DO 202 I=1,7,6
      DO 202 J=1,7,6
      202 S(I,J)=0.
C*****
C-----UNIT FORCE RECOVERY MATRIX DUE TO BENDING AND TWISTING
C*****
      DO 150 LA=1,10,3
      LB=LA+2
      DO 150 MA=1,10,3
      MB=MA-1
      DO 150 I=LA,LB
      DO 150 JM=1,3
      J=IM+MB
      X=0.
      DO 151 K=1,3
      151 X=X+S(I,K+MB)*T(K,JM)
      150 S72(I,J)=X
C*****
C-----COORDINATE TRANSFORMATION OF UNIT BENDING AND TWISTING STIFFNESS

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RFAM2980
RFAM2990
RFAM3000
RFAM3010
RFAM3020
RFAM3030
RFAM3040
RFAM3050
RFAM3060
RFAM3070
RFAM3080
RFAM3090
RFAM3100
RFAM3110
RFAM3120
RFAM3130
RFAM3140
RFAM3150
RFAM3160
RFAM3170
RFAM3180
RFAM3190
RFAM3200
RFAM3210
RFAM3220
RFAM3230
RFAM3240
RFAM3250
RFAM3260
RFAM3270
RFAM3280
RFAM3290
RFAM3300
RFAM3310
RFAM3320
RFAM3330
RFAM3340
RFAM3350
RFAM3360
RFAM3370
RFAM3380
RFAM3390
RFAM3400
RFAM3410
RFAM3420
RFAM3430
RFAM3440
RFAM3450
RFAM3460
RFAM3470
RFAM3480
RFAM3490
RFAM3500
RFAM3510
RFAM3520
RFAM3530
RFAM3540
RFAM3550
RFAM3560
RFAM3570

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C*****RFAM3580
  DO 160 LA=1,10,3                                RFAM3590
    LR=LA-1                                          RFAM3600
    DO 160 MA=1,10,3                                RFAM3610
    MR=MA+2                                          RFAM3620
    DO 160 IL=1,3                                    RFAM3630
    J=IL+LR                                          RFAM3640
    DO 160 J=MA,MR                                    RFAM3650
    X=0.                                             RFAM3660
    DO 161 K=1,3                                      RFAM3670
    161 X=X+T(K,IL)*ST2(K+LR,J)                    RFAM3680
    160 S2(I,J)=X                                    RFAM3690
C*****RFAM3700
C-----TRANSFORMATION OF ELEMENT LOAD VECTOR DUE TO FIXED END FORCES RFAM3710
C    TO GLOBAL COORDINATES                          RFAM3720
C*****RFAM3730
  DO 165 LA=1,10,3                                RFAM3740
    LR=LA-1                                          RFAM3750
    DO 165 IL=1,3                                    RFAM3760
    I=IL+LR                                          RFAM3770
    DO 165 N=1,4                                      RFAM3780
    X=0.                                             RFAM3790
    DO 167 K=1,3                                      RFAM3800
    167 X=X-T(K,IL)*TT2(K+LR,N)                    RFAM3810
    165 P2(I,N)=X                                    RFAM3820
C*****RFAM3830
C-----ELEMENT MASS MATRIX                          RFAM3840
C*****RFAM3850
  X =WT*DN/2.                                       RFAM3860
  DO 180 M=1,3                                       RFAM3870
  XM(M)=X                                            RFAM3880
  XM(M+3)=0.                                         RFAM3890
  XM(M+9)=0.                                         RFAM3900
  180 XM(M+6)=X                                       RFAM3910
C*****RFAM3920
C-----COMPUTE GRAVITY LOADING ( POINT LOADS ONLY ) RFAM3930
C*****RFAM3940
  DO 190 I=1,3                                       RFAM3950
  DO 190 J=1,4                                       RFAM3960
  P1(I,J)=P1(I,J)+FMUL(I,J)*XM(I)                 RFAM3970
  190 P1(I+6,J)=P1(I+6,J)+FMUL(I,J)*XM(I+6)       RFAM3980
  RETURN                                             RFAM3990
40 WRITE(1W,4002) NFI.                             RFAM4000
  STOP                                              RFAM4010
4002 FORMAT ('HOREAM NO ,15, 26H      K NODE ON BEAM X-AXIS RFAM4020
. 26H.....EXECUTION TERMINATED )                RFAM4030
  END                                              RFAM4040

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      SURROUINIF SLAVE (X,Y,7,IN,NUMNP,NI,NJ,ND,NS)
      C*****
C-----PERFORMS SLAVE ...MASTER DISPLACEMENT TRANSFORMATION
      C ( FOR NODES CONNECTED TO RFAM ELEMENTS ONLY)
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      RFAL*4 X,Y,7
      COMMON/FM/LM(24),S(24,24,2),P(192),SI(12,24,2),TI(96),XM(24),
      1 FM(481)
      DIMENSION X(NUMNP),Y(NUMNP),Z(NUMNP),IN(NUMNP,6)
      C*****
C-----DETERMINE REQUIRED TRANSLATION DEGREES OF FREEDOM
      C*****
      DO 54 NF=1,12,6
      NDD=N1
      IF (NF,FO,7) NDD=NJ
      DO 30 K=1,3
      I=K+NF-1
      IF (LM(I),GF,0) GO TO 30
      M=-LM(I)
      LM(I)=ID(M,K)
      N1=NDD+1
      N2=NDD+2
      IF(K-2) 35,45,55
      35 D1=-(Y(NDD)-Y(M))
      D2= 7(NDD)-7(M)
      LM(N1)=ID(M,6)
      LM(N2)=ID(M,5)
      GO TO 50
      45 D1=-(7(NDD)-7(M))
      D2= X(NDD)-X(M)
      LM(N1)=ID(M,4)
      LM(N2)=ID(M,6)
      GO TO 50
      55 D1=-(X(NDD)-X(M))
      D2= Y(NDD)-Y(M)
      LM(N1)=ID(M,5)
      LM(N2)=ID(M,4)
      50 CONTINUE
      C*****
C-----TRANSFORMATION...ARRAYS INCREASE IN SIZE
      C*****
      DO 80 IJ=1,2
      DO 60 II=1,NDD
      S(N1,II,IJ)=S(I,II,IJ)*D1
      S(N2,II,IJ)=S(I,II,IJ)*D2
      S(TI,N1,IJ)=S(N1,II,IJ)
      60 S(TI,N2,IJ)=S(N2,II,IJ)
      S(N1,N1,II)=S(I,I,II)*D1*D1
      S(N1,N2,II)=S(I,I,II)*D1*D2
      S(N2,N1,II)=S(N1,N2,II)
      S(N2,N2,II)=S(I,I,II)*D2*D2
      DO 70 IF=1,NS
      SI(TI,N1,IF)=SI(TI,II,IJ)*D1
      70 SI(TI,N2,IF)=SI(TI,II,IJ)*D2
      80 CONTINUE
      XM(N1)=XM(I)*D1*D1
      XM(N2)=XM(I)*D2*D2
      NDD=NDD+2
      30 CONTINUE

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      RFAM4050
      RFAM4060
      RFAM4070
      RFAM4080
      RFAM4090
      RFAM4100
      RFAM4110
      RFAM4120
      RFAM4130
      RFAM4140
      RFAM4150
      RFAM4160
      RFAM4170
      RFAM4180
      RFAM4190
      RFAM4200
      RFAM4210
      RFAM4220
      RFAM4230
      RFAM4240
      RFAM4250
      RFAM4260
      RFAM4270
      RFAM4280
      RFAM4290
      RFAM4300
      RFAM4310
      RFAM4320
      RFAM4330
      RFAM4340
      RFAM4350
      RFAM4360
      RFAM4370
      RFAM4380
      RFAM4390
      RFAM4400
      RFAM4410
      RFAM4420
      RFAM4430
      RFAM4440
      RFAM4450
      RFAM4460
      RFAM4470
      RFAM4480
      RFAM4490
      RFAM4500
      RFAM4510
      RFAM4520
      RFAM4530
      RFAM4540
      RFAM4550
      RFAM4560
      RFAM4570
      RFAM4580
      RFAM4590
      RFAM4600
      RFAM4610
      RFAM4620
      RFAM4630
      RFAM4640

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C*****HEAM4650
C-----SFT ROTATIONS                                RFAM4660
C*****RFAM4670
      DO 54 ,I=1,3
      K=NF+I+2
      IF(LM(K),GF,0) GO TO 54
      M=-LM(K)
      LM(K)=JN(M,I+3)
54 CONTINUE
      RETURN
      END
      RFAM4680
      RFAM4690
      RFAM4700
      RFAM4710
      RFAM4720
      RFAM4730
      RFAM4740
      RFAM4750

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      SHRNUTIME CRR1 (A0,A1,A2,A3,7)                                RFAM4760
C*****RFAM4770
C-----COMPILES THE LARGEST REAL ROOT 7 OF
C      A0+A1*Z+A2*Z**2+A3*Z**3=0                                RFAM4780
C*****RFAM4790
      A0=A0/A3
      A1=A1/A3
      A2=A2/A3
      C=A1/3,0-A2**2/9,0
      R=(A1*A2-3,0*A0)/6,0-A2**3/27,0
      P=Q**3+R**2
      IF (P,LT,0,0) GO TO 200
      P=SQRT (P)
      RP=R+P
      IF(RP,LT,0,0) GO TO 50
      S1=RP**0.3333333
      GO TO 60
50 S1=(-RP)**0.3333333
60 RP=R-P
      IF(RP,LT,0,0) GO TO 70
      S2=RP**0.3333333
      GO TO 80
70 S2=(-RP)**0.3333333
80 Z=S1+S2-A2/3,0
      RETURN
200 P=-P
      P=SQRT(P)
      SRAR=SQRT(R**2+P**2)
      COS3=R/SRAR
      SIN3=P/SRAR
      W=ATAN(SIN3/COS3)
      W=W/3,0
      C=COS(W)
      S=SIN(W)
      IF (S,LT,0,0) S=-S
      SRAR=SRAR**0.3333333
      Z=2,0*SRAR*C-A2/3,0
      R=-SRAR*C-A2/3,0+1.732051*SRAR*S
      IF (R,GT,7) Z=R
      RETURN
      END
      RFAM4810
      RFAM4820
      RFAM4830
      RFAM4840
      RFAM4850
      RFAM4860
      RFAM4870
      RFAM4880
      RFAM4890
      RFAM4900
      RFAM4910
      RFAM4920
      RFAM4930
      RFAM4940
      RFAM4950
      RFAM4960
      RFAM4970
      RFAM4980
      RFAM4990
      RFAM5000
      RFAM5010
      RFAM5020
      RFAM5030
      RFAM5040
      RFAM5050
      RFAM5060
      RFAM5070
      RFAM5080
      RFAM5090
      RFAM5100
      RFAM5110
      RFAM5120
      RFAM5130
      RFAM5140
      RFAM5150
      RFAM5160

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SUBROUTINE DBEAM ( AOLD,ANEW,LOAD,NUMDV)
C*****RFAM5170
C-----DESIGN OF BEAM ELEMENTS
C*****RFAM5180
COMMON/JUNK/JUN(16),LT,LH,L,SIG(27),INVAR,IFX,FRC,AREA,XINERT,
1 ZFF(6),TFNS,COMP,SHFAR,KSEC,SFCMOD(12),JUN(127)
DIMENSION AOLD(NUMDV),ANEW(NUMDV),LOAD(NUMDV)
DEF,TA=0.,DD1
KMAX=6
RMAX=0.
AA=ARFA
IF(IFX.F0.2) AA=SQRT(AA**3)
IF(KSEC.GT.1) GO TO 20
C*****RFAM5190
C-----SET UP SECTION MODULUS ARRAY SFCMOD(I) FOR ALL
C*****RFAM5200
C FOUR STRESS POINTS OF X-SECTION AT NODE I
C*****RFAM5210
DO 10 I=1,3
SFCMOD(I)=ZFF(I)*AA
SFCMOD(I+3)=SFCMOD(I)
SFCMOD(I+6)=-ZFF(I+3)*AA
10 SFCMOD(I+9)=SFCMOD(I+6)
SFCMOD(2)=-SFCMOD(2)
SFCMOD(11)=-SFCMOD(11)
GO TO 25
C*****RFAM5220
C-----SET UP SFCMOD(I) FOR Z-SECTION OR TURE
C*****RFAM5230
DO 15 I=1,3
SFCMOD(I)=ZFF(I)*AA
SFCMOD(I+3)=-SFCMOD(I)
SFCMOD(I+6)=ZFF(I+3)*AA
15 SFCMOD(I+9)=-SFCMOD(I+6)
SFCMOD(2)=-SFCMOD(2)
SFCMOD(5)=-SFCMOD(5)
IF (KSEC.NF.3) GO TO 25
SFCMOD(8)=0.
SFCMOD(11)=0.
C*****RFAM5240
C-----OBTAIN AXIAL FORCE X AND MOMENTS XX,YY,ZZ.
C*****RFAM5250
C FIRST FOR NODE I, THEN FOR NODE J
C*****RFAM5260
25 X=SIG(7)
DO 30 N=1,7,6
IF (N.E0.1) GO TO 26
DO 27 I=1,12
27 SFCMOD(I)=-SFCMOD(I)
26 XX=SIG(N+3)
YY=SIG(N+4)
ZZ=SIG(N+5)
C*****RFAM5270
C-----MODIFY MOMENTS FOR TURE
C*****RFAM5280
IF (KSEC.NF.3) GO TO 40
YY=SQRT(YY*YY+ZZ*ZZ)
ZZ=0.
40 SAXIAL=Y/ARFA
C*****RFAM5290
C-----COMPUTE STRESSES AT FOUR STRESS POINTS ON X-SECTION
C*****RFAM5300

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      DD 35 I=1,10,3                                RFAM5770
      SSHFAR=0.                                        RFAM5780
      IF (SFCMOD(I),NF,0.) SSHFAR=XX/SFCMOD(I)        RFAM5790
      SRFND=0.                                         RFAM5800
      IF (SFCMOD(I+1),NF,0.) SRFND=YY/SFCMOD(I+1)     RFAM5810
      IF (SFCMOD(I+2),NF,0.) SRFND=SRFND+77/SFCMOD(I+2) RFAM5820
      STDT=SAXIAL+SRFND                                RFAM5830
      SSTAR=TFNS                                       RFAM5840
      IF (STDT,LT,0.) SSTAR=-COMP                     RFAM5850
C*****RFAM5860
C-----APPLY REDESIGN FORMATIONS                     RFAM5870
C*****RFAM5880
      IF (FX,FO,2) GO TO R1                            RFAM5890
      R=SQRT((STDT/SSTAR)**2+(SSHFAR/SHEAR)**2)        RFAM5900
      GO TO R2                                          RFAM5910
      R1 ITEST=1                                       RFAM5920
      TEST=(SSHFAR/SHEAR)**2-2.0*ABS(SAXIAL*SRFND)/SSTAR**2 RFAM5930
C*****RFAM5940
C-----CHECK IF SHEAR STRESS DOMINATES              RFAM5950
C*****RFAM5960
      IF (TEST,GT,0.) ITEST=2                          RFAM5970
      KOUNT=0                                           RFAM5980
      RR=1.                                              RFAM5990
      R=0.                                              RFAM6000
      C=-SAXIAL/SSTAR                                  RFAM6010
      R5 GO TO (1,2),ITEST                             RFAM6020
      1 AA=(SSHFAR/SHEAR/RR**3)**2                    RFAM6030
      IF (AA,GT,1.) AA=0.                               RFAM6040
      A=SQRT(1.0-AA)                                   RFAM6050
      D=-SRFND/SSTAR                                   RFAM6060
      GO TO 70                                          RFAM6070
      2 A=1.                                             RFAM6080
      D=-1*(SRFND/SSTAR)**2+(SSHFAR/SHEAR)**2+2.0*SAXIAL*SRFND/(SSTAR**2*RFAM6090
      SQRT(RR)))                                       RFAM6100
      70 CALL CART(D,C,R,A,R)                          RFAM6110
C*****RFAM6120
C-----CHECK FOR CONVERGENCE                         RFAM6130
C*****RFAM6140
      IF (R,LT,0.000001) GO TO R0                     RFAM6150
      DR=ABS((R-RR)/R)                                 RFAM6160
      IF (DR,LT,DFLTA,DR,KOUNT,FO,KMAX) GO TO R0      RFAM6170
      KOUNT=KOUNT+1                                    RFAM6180
      RR=R                                              RFAM6190
      GO TO R5                                          RFAM6200
      R0 IF (ITEST,FO,1) R=R*R                         RFAM6210
      R2 IF (R,GT,RMAX) RMAX=R                       RFAM6220
      35 CONTINUE                                       RFAM6230
      20 CONTINUE                                       RFAM6240
C*****RFAM6250
C-----RECORD NEW DESIGN VARIABLE AND CORRESPONDING LOAD CONDITION RFAM6260
C*****RFAM6270
      AA=RMAX*ADP(D,INVAR)                             RFAM6280
      IF (AA,LT,ANFW(INVAR)) GO TO 60                 RFAM6290
      ANFW(INVAR)=AA                                    RFAM6300
      LONN(INVAR)=L                                     RFAM6310
      60 CONTINUE                                       RFAM6320
      RETURN                                           RFAM6330
      END                                              RFAM6340

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      SHROUTH TIME PLANE(A,MTOT)
C*****PI AN0000
C-----PIANE STRESS ELEMENTSPI AN0010
C*****PI AN0020
      DIMENS(DIM A(MTOT),STRLAB(5)PI AN0030
      COMMON /F1,PAR/ NPAR(14),NIMNP,MBAND,NF1,TYP,N1,N2,N3,N4,N5,M117,NEQPI AN0040
      1,NIMFL,NIMDV,M1,M2,M3,LL,LB,NFOP,NBLNCKPI AN0050
      COMMON/FM/NU,NW,NS,ND ,FM1(5062)PI AN0060
      COMMON/JHINK/JHIN(16),LT,LH,L,SG(20),SIG(7),IDV,IEF,FRC,ARFA,XINERT,PI AN0070
      1 DEFINE(60),JHIN(189)PI AN0080
      COMMON/UNIT/IR,IW,TP,11,12,13,18,19,110,111,112PI AN0090
      DATA STRLAB/3HCFN,3HI-1,3HI-K,3HI-L,3HK-L/PI AN0100
      NIMF=NPAR(2)PI AN0110
      KODF=NPAR(5)PI AN0120
      IF(NPAR(1),FO,0)GO TO 500PI AN0130
      NA=N5+NIMNPPI AN0140
      NIMMAT=NPAR(3)PI AN0150
      NIMTC=NPAR(4)PI AN0160
      GO TO (1,2,3),KODFPI AN0170
C*****PI AN0180
C-----IMIDIRECTIONALLY STIFFENED PANELPI AN0190
C*****PI AN0200
      1 NIMGFN=NPAR(7)PI AN0210
      N7=N6+NIMMATPI AN0220
      NR=N7+NIMMATPI AN0230
      N9=NR+NIMGFN*5PI AN0240
      N10=N9+NIMMAT*NIMTC*8PI AN0250
      MM=N10-MTOTPI AN0260
      IF(MM.GT.0) CALL FRRDR(MM)PI AN0270
      CALL PLMAX1(A(M1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),A(N8),PI AN0280
      1A(N9),NIMDV,NIMNP,NIMMAT,NIMTC,KODF,NIMF,NIMGFN)PI AN0290
      RETURNPI AN0300
C*****PI AN0310
C-----ISOTROPIC PLANE MEMBRANEPI AN0320
C*****PI AN0330
      2 N7=N6+NIMMATPI AN0340
      NR=N7+NIMMATPI AN0350
      N9=NR+NIMMAT*NIMTC*7PI AN0360
      MM=N9-MTOTPI AN0370
      IF(MM.GT.0) CALL FRRDR(MM)PI AN0380
      CALL PLMAX2(A(M1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),A(N8),PI AN0390
      1NIMDV,NIMNP,NIMMAT,NIMTC,KODF,NIMF)PI AN0400
      RETURNPI AN0410
C*****PI AN0420
C-----PROVISION FOR SPECIAL MEMBRANE ELEMENTPI AN0430
C*****PI AN0440
      3 CALL NDEFEM (NPAR(1),KODF,IW)PI AN0450
      RETURNPI AN0460
      500 WRITE (IW,2008) KODFPI AN0470
      DO 800 MM=1,NIMFPI AN0480
      CALL STRSC(A(M1),A(N1),A(N3),NF0,NIMDV,LL,LB,IR,0)PI AN0490
      WRITE (IW,2005) MM,ARFAPI AN0500
      IF(NS.FO,1) GO TO 800PI AN0510
      DO 700 I=LT,LHPI AN0520
      CALL STRSC(A(M1),A(N1),A(N3),NF0,NIMDV,LL,LB,IR,1)PI AN0530
      IF(L.GT.1) WRITE(IW,2007)PI AN0540
      IT=0PI AN0550
      DO 600 KK=1,NS,3PI AN0560
      IF(KK.GT.1) WRITE(IW,2007)PI AN0570
      DO 500 I=1,3PI AN0580

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520 SIG(I)=SG(KK-1+I)
      IT=IT+1
      NP=3
      IF(IT.GT.1) GO TO 530
      NP=6
      ANG=DESI*MF(1)
      IF(ANG.NF.0.) GO TO 540
      DO 550 J=1,3
550  SIG(I+3)=SIG(I)
      GO TO 530
540  ANG=ANG/57.2957795
      SI=SIN(ANG)
      CO=COS(ANG)
      SC=SI*CO
      SI=SI*SI
      CO=CO*CO
      X1=SIG(1)*CO+SIG(2)*SI
      X2=2.0*SIG(3)*SC
      SIG(4)=X1+X2
      SIG(5)=X1-X2
      SIG(6)=(SIG(2)-SIG(1))*SC+SIG(3)*(CO-SI)
530  GO TO (4,5,6),KPOF
C*****PL AN0600
C-----DESIGN OF STIFFENED MEMBRANE ELEMENT PL AN0610
C*****PL AN0620
      4 IF(IT.GT.1) GO TO 600
      CALL DPLAN1 (A(M1),A(M2),A(M3),NUMDV)
      GO TO 600
C*****PL AN0630
C-----DESIGN OF ISOTROPIC MEMBRANE ELEMENT PL AN0640
C*****PL AN0650
      5 CALL DPLAN2(A(M1),A(M2),A(M3),NUMDV)
      GO TO 600
C*****PL AN0660
C-----PROVISION FOR DESIGN OF SPECIAL MEMBRANE ELEMENT PL AN0670
C*****PL AN0680
      6 CONTINUE
      600 WRITE (14,2009) L,STRLAB(IT),(SIG(I),I=1,NP)
      700 CONTINUE
      800 CONTINUE
C*****PL AN0690
      RETURN
      2005 FORMAT(1X,I5,F14.4)
      2006 FORMAT(//45H ANALYSIS OF MEMBRANE ELEMENTS. CONSTRN CODE=,I12//
      111TH SHEET LOAD /---MEMBRANE FORCES IN PL AN1040
      2LOCAL COORDS---//---MEMBRANE FORCES IN MATERIAL COORDS-/ / PL AN1050
      311TH ELEMENT THICKNESS COND LOCATION NXX NYY PL AN1060
      4 NXY N11 N22 M12 /) PL AN1070
      2009 FORMAT(1H+,20X,I5,6X,A3,4X,F13.4)
      2007 FORMAT(//)
      END
      PL AN1080
      PL AN1090
      PL AN1100

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SUBROUTINE FLAW(BETA)
C*****
C-----STRESS / STRAIN RELATION MATRIX
C*****
      JMP(I,C) REFAL#B (A-H,N-7)
      COMMON/JUNK/IF(4),IX(4),FMILL(4,5),D(3,3),XX(4),YY(4),ZZ(4),TMP(4),
      1 ALP(3),TTF(3),PRESS,REF7,NS,JUN,T(3,3),DD(3,3),JUN(148)
      IF (BETA.FD.N.N) GO TO 500
      ANG=REF7A/57.2957795
      SS=DSIN(ANG)
      C2=DCOS(ANG)
      C2=C2*C2
      S2=SS*SS
      SC=SS*C2
C*****
C-----SET D FOR SIG(N)=D*SIG(G)
C*****
      T(1,1)=C2
      T(1,2)=S2
      T(1,3)=2.*SC
      T(2,1)=S2
      T(2,2)=C2
      T(2,3)=-2.*SC
      T(3,1)=-SC
      T(3,2)=SC
      T(3,3)=C2-S2
      DO 300 I=1,3
      DO 300 J=1,3
      SUM=0.
      DO 280 M=1,3
280 SUM=SUM+T(M,I)*D(M,J)
300 DD(I,J)=SUM
      DO 350 I=1,3
      DO 350 J=1,3
      SUM=0.
      DO 330 M=1,3
330 SUM=SUM+DD(I,M)*T(M,J)
      DD(I,J)=SUM
      A1=ALP(1)
      A2=ALP(2)
      ALP(1)=C2*A1+S2*A2
      ALP(2)=S2*A1+C2*A2
      ALP(3)=2.*0*SC*(A1-A2)
500 CALL PDSTINV(I)
      DO 670 I=1,3
      TTF(I)=0.
      DO 670 M=1,3
670 TTF(I)=TTF(I)+D(I,M)*ALP(M)
      REF7IRM
      FMD

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PI AN1110
PL AN1120
PI AN1130
PL AN1140
PI AN1150
PL AN1160
PI AN1170
PL AN1180
PI AN1190
PL AN1200
PI AN1210
PL AN1220
PI AN1230
PL AN1240
PI AN1250
PL AN1260
PI AN1270
PL AN1280
PI AN1290
PL AN1300
PI AN1310
PL AN1320
PI AN1330
PL AN1340
PI AN1350
PL AN1360
PI AN1370
PL AN1380
PI AN1390
PL AN1400
PI AN1410
PL AN1420
PI AN1430
PL AN1440
PI AN1450
PL AN1460
PI AN1470
PL AN1480
PI AN1490
PL AN1500
PI AN1510
PL AN1520
PI AN1530
PL AN1540
PI AN1550
PL AN1560
PI AN1570
PL AN1580
PI AN1590
PL AN1600
PI AN1610

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SUBROUTINE QHIAN(RHO,THICK)
C*****
C-----FORM ELEMENT MATRICES
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      COMMON/ELPAR/NPAR(14),IFLP(19)
      COMMON/FM/LM(12),S(12,12),P1(12,4),P2(12,4),XM(12),ST(15,12),
      1 TT(15,4),RR(12,12),FMM(1891)
      COMMON/JUNK/JF(4),JX(4),EMUL(4,5),D(3,3),X(4),Y(4),Z(4),TM(4),
      1 ALP(3),TTT(3),PRESS,REFE,NS,JUN1,RR(4),ZZ(4),PP1(12),
      2 JJ(4),V(4),W(4),H(6),HR(6),HZ(6),FAC,G(4),F(4),JUN(66)
      DIMENSION SSS(5),SSS(5),TTT(5),IVFCT(4),IVFCT(4),FMM(636)
      EQUIVALENCE (S,FMM)
      DATA SSS/-0.57735026918963,0.57735026918963/
      DATA SSS/0.,-1.,1.,0.,0./, TTT/0.,0.,0.,-1.,1./
      DATA IVFCT/4,2,1,3/,IVFCT/1,3,2,4/
      DO 10 I=1,636
      10 FMM(I)=0.
      DO 20 J=1,12
      20 PP1(J)=0.
C*****
C-----COMPUTE ELEMENT AXES SYSTEM AND CORNER COORDINATES
C*****
      CALL VECTDR(U,X(1),Y(1),Z(1),X(2),Y(2),Z(2))
      CALL VECTDR(F,X(1),Y(1),Z(1),X(4),Y(4),Z(4))
      CALL CRDSS(U,F,W)
      CALL CRDSS(W,H,V)
      CALL VECTDR(G,X(1),Y(1),Z(1),X(3),Y(3),Z(3))
      RR(1)=0.0
      ZZ(1)=0.0
      RR(2)=H(4)
      ZZ(2)=0.0
      RR(3)=G(4)*DDT(G,H)
      ZZ(3)=G(4)*DDT(G,V)
      RR(4)=F(4)*DDT(F,H)
      ZZ(4)=F(4)*DDT(F,V)
C*****
C-----FORM UNIT STIFFNESS MATRIX , THERMAL LOAD VECTOR AND MASS MATRIX
C*****
      DO 500 JJ=1,2
      DO 500 J,J=1,2
      CALL FORMR(SS(JJ),SS(J,J),RR)
      FTP=H(1)*TM(1)+H(2)*TM(2)+H(3)*TM(3)+H(4)*TM(4)-REFE
      DO 400 J=1,12
      R1=RR(1,J)*FAC
      R2=RR(2,J)*FAC
      R3=RR(3,J)*FAC
      D1=D(1,J)*R1+D(1,2)*R2+D(1,3)*R3
      D2=D(2,J)*R1+D(2,2)*R2+D(2,3)*R3
      D3=D(3,J)*R1+D(3,2)*R2+D(3,3)*R3
      PP1(J)=PP1(J)+FTP*(D1*ALP(1)+D2*ALP(2)+D3*ALP(3))
      DO 400 I=J,12
      S(I,J)=S(I,J)+RR(1,I)*D1+RR(2,I)*D2+RR(3,I)*D3
      400 S(I,I)=S(I,I)
      DO 450 I=1,4
      450 XM(I)=XM(I)+FAC*THICK*H(I)
      500 CONTINUE
C*****
C-----FORM STRESS DISPLACEMENT MATRIX
C*****

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PL AN1620
PL AN1630
PL AN1640
PL AN1650
PL AN1660
PL AN1670
PL AN1680
PL AN1690
PL AN1700
PL AN1710
PL AN1720
PL AN1730
PL AN1740
PL AN1750
PL AN1760
PL AN1770
PL AN1780
PL AN1790
PL AN1800
PL AN1810
PL AN1820
PL AN1830
PL AN1840
PL AN1850
PL AN1860
PL AN1870
PL AN1880
PL AN1890
PL AN1900
PL AN1910
PL AN1920
PL AN1930
PL AN1940
PL AN1950
PL AN1960
PL AN1970
PL AN1980
PL AN1990
PL AN2000
PL AN2010
PL AN2020
PL AN2030
PL AN2040
PL AN2050
PL AN2060
PL AN2070
PL AN2080
PL AN2090
PL AN2100
PL AN2110
PL AN2120
PL AN2130
PL AN2140
PL AN2150
PL AN2160
PL AN2170
PL AN2180
PL AN2190
PL AN2200
PL AN2210

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      LL=NS/3                                PL AN2220
      DO 530 I=1,LL                          PL AN2230
      CALL FORMR( SSS(L),TTT(L),RR)          PL AN2240
      FIP=H(I)*TM(I)+H(2)*TM(2)+H(3)*TM(3)+H(4)*TM(4)-RFFT PL AN2250
      DO 530 I=1,3                          PL AN2260
      I=I+3*(I-1)                          PL AN2270
      TT(I,4)=-TTT(I)*FIP                  PL AN2280
      DO 530 J=1,12                         PL AN2290
      DO 530 K=1,3                          PL AN2300
      530 ST(I,J)=ST(I,J)+D(I,I,K)*RR(K,J) PL AN2310
C*****PL AN2320
C-----FLIMINATE EXTRA DEGREES OF FREEDOM PL AN2330
C*****PL AN2340
      IF ( IX(3) .EQ. IX(4) ) GO TO 560 PL AN2350
      IF (MPAR(6),NF,0) GO TO 560          PL AN2360
      DO 550 NN=1,4                        PL AN2370
      L=12-NN                             PL AN2380
      K=L+1                                PL AN2390
      C=PP1(K)/S(K,K)                     PL AN2400
      DO 535 J=1,NS                       PL AN2410
      535 TT(J,4)=TT(J,4)+C*ST(J,K)        PL AN2420
      DO 550 I=1,L                         PL AN2430
      C=S(I,K)/S(K,K)                     PL AN2440
      PP1(I)=PP1(I)-C*PP1(K)              PL AN2450
      DO 540 J=1,NS                       PL AN2460
      540 ST(J,I)=ST(J,I)-C*ST(J,K)        PL AN2470
      DO 550 J=1,L                         PL AN2480
      550 S(I,J)=S(I,J)-C*S(K,J)          PL AN2490
C*****PL AN2500
C-----ROTATE STRESS-DISPLACEMENT TRANSFORMATION TO GIVE STRESSES PL AN2510
C      NORMAL AND PARALLEL TO SIDES - SIMILARLY ROTATE INITIAL STRESSES PL AN2520
C*****PL AN2530
      560 NSFT=LL-1                        PL AN2540
      IF ( NSFT .LE. 0 ) GO TO 730         PL AN2550
      DO 720 I=1,NSFT                     PL AN2560
      IV=JVFCT(I)                          PL AN2570
      JV=JVFCT(I)                          PL AN2580
      CALL VFCTDR(G,RR(JV),Z7(JV),0,0,0,RR(JV),Z7(JV),0,0,0) PL AN2590
      S2=G(1)*G(1)                         PL AN2600
      C2=G(2)*G(2)                         PL AN2610
      SC=-G(1)*G(2)                       PL AN2620
      I1=2*I+1                            PL AN2630
      I2=I1+1                             PL AN2640
      I3=I1+2                             PL AN2650
      T1=TT(I1,4)                         PL AN2660
      T2=TT(I2,4)                         PL AN2670
      T3=TT(I3,4)                         PL AN2680
      T4=2.0*SC*T3                        PL AN2690
      TT(I1,4)=C2*T1+S2*T2+T4             PL AN2700
      TT(I2,4)=S2*T1+C2*T2-T4             PL AN2710
      TT(I3,4)=SC*(T2-T1)+(C2-S2)*T3      PL AN2720
      DO 710 J=1,8                        PL AN2730
      R1=ST(I1,J)                         PL AN2740
      R2=ST(I2,J)                         PL AN2750
      R3=ST(I3,J)                         PL AN2760
      R4=2.0*SC*R3                        PL AN2770
      ST(I1,J)=C2*R1+S2*R2+R4             PL AN2780
      ST(I2,J)=S2*R1+C2*R2-R4             PL AN2790
      710 ST(I3,J)=SC*(R2-R1)+(C2-S2)*R3 PL AN2800
      720 CONTINUE                        PL AN2810

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```

730 JF(NPAR(5),NF,2) GO TO 150                                PL AN2820
C*****PL AN2830
C-----CALCULATE PRESSURE LOADS ON J-J FACE IN GLOBAL COORDINATES PL AN2840
C*****PL AN2850
      XX=0.5*PPFSS*RR(2)                                PL AN2860
      DO 185 J=1,3                                          PL AN2870
        I=(J-1)*4+1                                         PL AN2880
        DO 185 L=1,4                                         PL AN2890
          P2(I,L)=XX*V(I)*FMI(L,2)                          PL AN2900
        185 P2(I+1,L)=P2(I,L)                                PL AN2910
C*****PL AN2920
C-----COORDINATE TRANSFORMATION PL AN2930
C*****PL AN2940
      150 DO 190 I=1,3                                       PL AN2950
        DO 190 K=1,4                                         PL AN2960
          KK=4*(J-1)+K                                       PL AN2970
          DO 190 J=1,3                                       PL AN2980
            DO 190 L=1,4                                       PL AN2990
              LL=4*(J-1)+L                                   PL AN3000
            180 RR(KK,LL)=U(I)*(S(K,L)*U(I)+S(K,L+4)*V(J))+ PL AN3010
              V(I)*(S(K+4,L)*U(J)+S(K+4,L+4)*V(J))          PL AN3020
              X1=U(I)*PP1(K)+V(I)*PP1(K+4)                 PL AN3030
            DO 190 L=1,4                                       PL AN3040
              190 P1(KK,L)=X1*FMI(L,1)                      PL AN3050
            DO 195 I=1,12                                     PL AN3060
              DO 195 J=1,12                                   PL AN3070
                S(I,J)=RR(I,J)                               PL AN3080
              195 S(J,I)=S(I,J)                              PL AN3090
            DO 210 K=1,NS                                     PL AN3100
              DO 200 L=1,4                                     PL AN3110
                DO 200 J=1,3                                   PL AN3120
                  LL=4*(J-1)+L                               PL AN3130
                200 PP1(LL)=ST(K,L)*U(J)+ST(K,L+4)*V(J)     PL AN3140
              DO 210 J=1,12                                   PL AN3150
                210 ST(K,J)=PP1(J)                          PL AN3160
              DO 220 I=1,4                                     PL AN3170
                XX=XM(I)*RHO                                  PL AN3180
                DO 220 L=1,4                                   PL AN3190
                  P1(I,L)=P1(I,L)+XX*FMI(L,3)              PL AN3200
                  P1(I+4,L)=P1(I+4,L)+XX*FMI(L,4)          PL AN3210
                220 P1(I+8,L)=P1(I+8,L)+XX*FMI(L,5)         PL AN3220
              DO 600 L=1,4                                     PL AN3230
                DO 600 I=1,NS                                 PL AN3240
                  600 T1(I,L)=T1(I,4)*FMI(L,1)             PL AN3250
              RETURN                                          PL AN3260
              FMD                                             PL AN3270

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      SHROUITHNE FORMR(S,T,H)                                PL AN3280
C*****                                                    PL AN3290
C-----FORM SHAPE-FUNCTION DERIVATIVES AND STRAIN-DISPLACEMENT MATRIX PL AN3300
C*****                                                    PL AN3310
      TMP1,ICIT,REAL*8 (A-H,I-7)                                PL AN3320
      DIMENSION R(12,12),I1(6),J1(6)                            PL AN3330
      COMMON/SHUNK/IF(4),IX(4),FMUL(4,5),O(3,3),X(4),Y(4),Z(4),TMP(4), PL AN3340
      1 ALP(2),T11(2),PRESS,REF1,NS,JUN1,RR(4),Z7(4),PP1(12), PL AN3350
      2 H1(4),V(4),W(4),H(6),HR(6),HZ(6),X1,HS(6),HT(6),JUN(5R) PL AN3360
      DATA I1/1,2,3,4,9,10/,J1/5,6,7,8,11,12/ PL AN3370
      SM=1.0-S                                                    PL AN3380
      SP=1.0+S                                                    PL AN3390
      TM=1.0-T                                                    PL AN3400
      TP=1.0+T                                                    PL AN3410
      H(1)=SM*TM*.25                                              PL AN3420
      H(2)=SP*TM*.25                                              PL AN3430
      H(3)=SP*TP*.25                                              PL AN3440
      H(4)=SM*TP*.25                                              PL AN3450
      H(5)=(1.0-S*S)                                              PL AN3460
      H(6)=(1.0-T*T)                                              PL AN3470
      HS(1)=-TM*.25                                              PL AN3480
      HS(2)=-HS(1)                                              PL AN3490
      HS(3)=TP*.25                                              PL AN3500
      HS(4)=-HS(3)                                              PL AN3510
      HS(5)=-2.*S                                              PL AN3520
      HS(6)=0.0                                                  PL AN3530
      HT(1)=-SM*.25                                              PL AN3540
      HT(2)=-SP*.25                                              PL AN3550
      HT(3)=-HT(2)                                              PL AN3560
      HT(4)=-HT(1)                                              PL AN3570
      HT(5)=0.0                                                  PL AN3580
      HT(6)=-2.*T                                              PL AN3590
      P7T=HT(3)*Z7(3)+H1(4)*Z7(4)                                PL AN3600
      P7S=HS(3)*Z7(3)+HS(4)*Z7(4)                                PL AN3610
      PRS=HS(2)*RR(2)+HS(3)*RR(3)+HS(4)*RR(4)                    PL AN3620
      PRT=HT(2)*RR(2)+HT(3)*RR(3)+HT(4)*RR(4)                    PL AN3630
      IF(DARS(Z7(3)-Z7(4)),LF,1.0F-10) P7S=0. PL AN3640
      IF(DARS(RR(2)-RR(3)),LF,1.0F-10,AND,DARS(RR(4)),LF,1.0F-10) PRT=0. PL AN3650
      XJ=PRS*P7T-PRT*P7S                                          PL AN3660
      PSR=P7T/XJ                                                  PL AN3670
      PTR=-P7S/XJ                                                  PL AN3680
      PS7=-PRT/XJ                                                  PL AN3690
      PT7=PRS/XJ                                                  PL AN3700
      DO 100 I=1,6                                                PL AN3710
      HR(I)=PS*HS(I)+PTR*HT(I)                                    PL AN3720
      100 H7(I)=PS7*HS(I)+PT7*HT(I)                                PL AN3730
C*****                                                    PL AN3740
C-----FORM STRAIN DISPLACEMENT MATRIX PL AN3750
C*****                                                    PL AN3760
      DO 200 K=1,6                                                PL AN3770
      I=I1(K)                                                    PL AN3780
      J=J1(K)                                                    PL AN3790
      R(1,I)=HR(K)                                                PL AN3800
      R(2,J)=H7(K)                                                PL AN3810
      R(3,I)=H7(K)                                                PL AN3820
      200 R(3,J)=HR(K)                                            PL AN3830
      RETURN                                                       PL AN3840
      END                                                           PL AN3850

```

```

SUBROUTINE POSINV(A)
C*****
C*****
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      DIMENSION A(3,3)
      DO 200 N=1,3
        D=A(N,N)
        DO 100 J=1,3
          A(N,J)=-A(N,J)/D
          DO 150 I=1,3
            IF(N-I) 110,150,110
          110 DO 140 J=1,3
            IF(N-J) 120,140,120
          120 A(I,J)=A(I,J)+A(I,N)*A(N,J)
          140 CONTINUE
          150 A(I,N)=A(I,N)/D
          A(N,N)=1./D
        200 CONTINUE
      RETURN
      END
PL AN3860
PL AN3870
PL AN3880
PL AN3890
PL AN3900
PL AN3910
PL AN3920
PL AN3930
PL AN3940
PL AN3950
PL AN3960
PL AN3970
PL AN3980
PL AN3990
PL AN4000
PL AN4010
PL AN4020
PL AN4030
PL AN4040
PL AN4050
PL AN4060

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SUBROUTINE PLNAXI(UWT,ID,X,Y,Z,T,NTC,WT,PGFN,PMAT,NUMDV,NUMNP,
      NUMMAT,NUMTC,KORF,NUMF,NUMGEF)
C*****
C-----STIFFNESS MEMBRANE ELEMENT
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*4 UWT,X,Y,Z,T,PGFN,WT,PMAT,RF1,F4,F5,F6,F7,SBC,PRC,GRC,FRC
      DIMENSION UWT(NUMDV),ID(NUMNP,6),X(NUMNP),Y(NUMNP),Z(NUMNP),
      1 T(NUMNP),NTC(NUMMAT),WT(NUMMAT),PGFN(NUMMAT,5),
      2 PMAT(NUMTC,6,NUMMAT)
      COMMON/EM/LM(12),S(12,12),P1(12,4),P2(12,4),XM(12),ST(15,12),
      1 IT(15,4),RR(12,12),FMI(189)
      COMMON/JUNK/IF(4),IX(4),FMI(4,5),C(3,3),XX(4),YY(4),ZZ(4),TMP(4),
      1 ALP(2),TII(3),PRESS,REF1,NS,NUM1,X1,X2,X3,X4,Y1,Y2,Y3,Y4,FF(7),
      2 JUM(154)
      COMMON/JUMITS/IR,IW,IP,II,I2,I3,I8,I9,I10,I11,I12
C*****
C-----CONTROL INFORMATION
C*****
      MU=1
      NV=1
      ND=12
      NW=1
      NT=0
      IFX=3
      WRITE(IW,2000)NUMF,KORF,NUMMAT,NUMGEF,NUMTC
      WRITE(IW,2010)
      DO 60 M=1,NUMMAT
        READ(IR,1010) N,NTC(N),WT(N)
        IF(NTC(N).LE.0) NTC(N)=1
        WRITE(IW,2020) N,NTC(N),WT(N)
C*****
C-----TEMPERATURE DEPENDENT MATERIAL PROPERTIES
C*****
PL AN4070
PL AN4080
PL AN4090
PL AN4100
PL AN4110
PL AN4120
PL AN4130
PL AN4140
PL AN4150
PL AN4160
PL AN4170
PL AN4180
PL AN4190
PL AN4200
PL AN4210
PL AN4220
PL AN4230
PL AN4240
PL AN4250
PL AN4260
PL AN4270
PL AN4280
PL AN4290
PL AN4300
PL AN4310
PL AN4320
PL AN4330
PL AN4340
PL AN4350
PL AN4360
PL AN4370
PL AN4380
PL AN4390
PL AN4400

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```

NT=NTC(N)
RFAD(IR,1005) (PMAT(I,J,N),J=1,8),I=1,N1)
DO 10 I=1,NT
IF(PMAT(I,6,N).LE.0.) PMAT(I,6,N)=PMAT(I,5,N)
IF(PMAT(I,7,NT).LE.0.) PMAT(I,7,N)=PMAT(I,5,N)*0.577
IF(PMAT(I,8,NT).LE.0.) PMAT(I,8,N)=PMAT(I,6,N)
10 CONTINUE
60 WRITE(IW,2010) (PMAT(I,J,N),J=1,8),I=1,NT)
C*****PL AN4490
C-----GFOMFTRIC PROPERTY CARDS
C*****PL AN4500
WRITE(IW,2011)
DO 70 I=1,NHMGFN
RFAD(IR,1006) N,TH,W,SA,SI,D,WF
IF(WF,LE.0.) WF=W
PGFN(N,1)=1.0+SA/(W*TH)
PGFN(N,2)=W/TH
PGFN(N,3)=WF/TH
DR=SA*D/(W*TH+SA)
R1=W*TH**3/12.0+W*TH*DR*DR+SI+SA*(D/PGFN(N,1))**2
PGFN(N,4)=R1/TH**4
C1=12.0*SI*0.925/(W*TH**3)
C2=SA*D/D/SI
C3=1.0+C2/(0.88*PGFN(N,1)+0.12)
PGFN(N,5)=2.0*PGFN(N,2)**2*(DSORT(1.0+C1*C3)+1.0)
70 WRITE(IW,2012) N,TH,W,SA,SI,D,WF
C*****PL AN4670
C-----FLFMFNT I.DAD MHI,IIPLIFRS
C*****PL AN4680
DO 131 I=1,4
RFAD(IR,1002) FMIL(I,1),(FMIL(I,J),J=3,5)
131 FMIL(I,2)=0.
WRITE(IW,2004)(FMIL(I,1),(FMIL(I,J),J=3,5),I=1,4)
C*****PL AN4740
C-----FLFMFNT CARDS
C*****PL AN4750
WRITE(IW,2002)
N=1
130 RFAD(IR,1003) IFL,IF,IMAT,IND,FPC,RFFI,AA,AB,AFIA,EFC,NS,INC
IF(FRC,LE.0.) FPC=1.
IF(FFC,LE.0.) FFC=1.
IF(INC,FO.0) INC=1
IF(NS,FO.0) NS=3
IF(NS,LI.3) NS=1
IF((IF(3),FO,IF(4)),AND,(NS,FO,15)) NS=12
ANG=RFIA/57.2957795
RHO=WT(IMAT)
THICK=PGFN(IMAT,1)
RFT=RFIA
KK=INC*(IFL-N)
DO 142 I=1,4
142 IX(I)=IF(I)-KK
DO 500 MFL=N,IFL
TFMP=0.
DO 501 I=1,4
II=IX(I)
TFMP=TFMP+T(II)*0.25
XX(I)=X(II)
YY(I)=Y(II)
501 Z(I)=Z(II)

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PL AN4410
PL AN4420
PL AN4430
PL AN4440
PL AN4450
PL AN4460
PL AN4470
PL AN4480
PL AN4490
PL AN4500
PL AN4510
PL AN4520
PL AN4530
PL AN4540
PL AN4550
PL AN4560
PL AN4570
PL AN4580
PL AN4590
PL AN4600
PL AN4610
PL AN4620
PL AN4630
PL AN4640
PL AN4650
PL AN4660
PL AN4670
PL AN4680
PL AN4690
PL AN4700
PL AN4710
PL AN4720
PL AN4730
PL AN4740
PL AN4750
PL AN4760
PL AN4770
PL AN4780
PL AN4790
PL AN4800
PL AN4810
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PL AN4830
PL AN4840
PL AN4850
PL AN4860
PL AN4870
PL AN4880
PL AN4890
PL AN4900
PL AN4910
PL AN4920
PL AN4930
PL AN4940
PL AN4950
PL AN4960
PL AN4970
PL AN4980
PL AN4990
PL AN5000

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C*****PI AN5010
C-----INTERPOLATE MATERIAL PROPERTIES FOR AVERAGE ELEMENT TEMPERATURE PI AN5020
C*****PI AN5030
      CALL INTERP(PMAT,FF,NIIMTC,NIIMMAT,H,7,NIC(IMAT),IMAT,TEMP) PI AN5040
      F4=FF(4) PI AN5050
      F5=FF(5) PI AN5060
      F6=FF(6) PI AN5070
      F7=FF(7) PI AN5080
      C1=FF(1)*9.8696 PI AN5090
      C2=C1/13.0*(1.0-FF(2)**2) PI AN5100
C*****PI AN5110
C-----FORM CONSTITUTIVE LAW AND COMPUTE THERMAL STRESSES PI AN5120
C*****PI AN5130
      DO 265 I=1,3 PI AN5140
      DO 265 J=1,3 PI AN5150
265 C(I,J)=0. PI AN5160
      C(2,2)=1.0/FF(1) PI AN5170
      C(1,1)=C(2,2)/THICK PI AN5180
      C(1,2)=-C(1,1)*FF(2) PI AN5190
      C(2,1)=C(1,2) PI AN5200
      C(3,3)=C(2,2)*2.0*(1.0+FF(2)) PI AN5210
      ALP(1)=FF(3) PI AN5220
      ALP(2)=FF(3) PI AN5230
      ALP(3)=0. PI AN5240
      CALL FLAW(BETA) PI AN5250
C*****PI AN5260
C-----FORM ELEMENT LOCATION MATRIX AND COMPUTE ELEMENT MATRICES PI AN5270
C*****PI AN5280
      DO 170 I=1,4 PI AN5290
      IX(I) PI AN5300
      TMP(I)=T(II) PI AN5310
      LM(I)=JN(II,1) PI AN5320
      LM(I+4)=JN(II,2) PI AN5330
170 LM(I+8)=JN(II,3) PI AN5340
      CALL QUAD(RHO,THICK) PI AN5350
      AREA=XM(1)+XM(2)+XM(3)+XM(4) PI AN5360
      IWT(IDV)=IWT(IDV)+AREA*RHO*FRC PI AN5370
C*****PI AN5380
C-----COMPUTE ELEMENT DESIGN INFORMATION PI AN5390
C*****PI AN5400
      IF(AA.LF.0)AA=.5*(IX2+X3-X1-X4)*DCOS(ANG)-(Y2+Y3-Y1-Y4)*DSIN(ANG) PI AN5410
      IF(AB.LF.0)AB=.5*(IX3+X4-X1-X2)*DSIN(ANG)+(Y3+Y4-Y1-Y2)*DCOS(ANG) PI AN5420
      SRC=C1*FRC/PGFN(IMAT,4)/(AA*AA*PGFN(IMAT,2)) PI AN5430
      PRC=C2*THICK/PGFN(IMAT,3)**2 PI AN5440
      GRC=C2*0.25*PGFN(IMAT,5)/AR**4 PI AN5450
C*****PI AN5460
C-----CALCULATE RANDOM VIB AND WRITE ELEMENT INFO. ON TAPES PI AN5470
C*****PI AN5480
      NN=NS*ND*NI PI AN5490
      CALL REAPAN(S1,ST,15,12,1,NS,ND,NI,NN) PI AN5500
      NN=NS*4*NI PI AN5510
      CALL REARAN(TT,11,15,4,1,NS,4,NW,NN) PI AN5520
      CALL CALBAN(NDIF,LM,S,P1,ST,TT,NI,NV,NS,ND,NW,IDV,IFX,FRC) PI AN5530
      WRITE(I7R)NI,BF1,F4,F5,F6,F7,PGFN(IMAT,1),SRC,PRC,GRC PI AN5540
      WRITE(LW,2003)NFI,IX,IMAT,IDV,FRC,REFI,AA,AB,BETA,FRC,NS,ND,IF PI AN5550
      DO 450 I=1,4 PI AN5560
450 IX(I)=IX(I)+INC PI AN5570
500 CONTINUE PI AN5580
      N=TFI+1 PI AN5590
      IF(N.LF.NIME)GO TO 130 PI AN5600

```

```

RETURN
1002 FORMAT(4F10.0)
1003 FORMAT(7I5,5X,4F10.0/2F10.0,2I5)
1005 FORMAT(8F10.0)
1006 FORMAT(15,6F10.0)
1010 FORMAT(2I5, F10.0)
2000 FORMAT(43H)NUMBER OF MEMBRANE ELEMENTS
1 44H CONSTRUCTION CODE
2 44H NUMBER OF MATERIALS
3 44H NUMBER OF GEOMETRIC PROPERTIES
4 44H NUMBER OF TEMPS FOR WHICH MATL PROPS GIVEN=,15/
2002 FORMAT(// 23H PROCESSED ELEMENT DATA//
1121H ELEMNT/-----NODES-----//--ID NOS--/ DES VAR REFERENCE
2MAX LENGTH WIDTH ANGLE TO END FIXITY PRNT BAND /
3121H NUMMR I J K L MAT DV FRACTION TEMP
40F STIFFNR OF ELEMENT PRINC DIRN COEFFT CODE WDTN /
2003 FORMAT(1X,7I5,6F12.4,2I6)
2004 FORMAT(23H ELEMENT LOAD FRACTIONS /59H LOAD CASE TEMPERATURE X-DIR
1RECTION Y-DIRECTION Z-DIRECTION /9X,1HA,4F12.3/
2 9X,1HP,4F12.3/ 9X,1HC,4F12.3/ 9X,1HD,4F12.3)
2010 FORMAT(1H+,25X,8F13.4/(26X,8F14.4))
2011 FORMAT(/91H GEOMETRY SHEET SPACING OF /-----STIFFENP
1ER PROPERTIES-----/ WIDTH OF /
2 91H NUMMRP THICKNESS STIFFENERS AREA INERTIA
4 DIST OF CGG SHEET )
2012 FORMAT(1X,15,6F14.4)
2019 FORMAT(// 25H MATERIAL PROPERTY CARDS /
1/125H MATL NO OF SPECIFIC YOUNGS
2SSONS COEFFT OF /-----ALLOWABLE STRESSES-----/
2/121H MRR TMRP WEIGHT TEMPERATURE MODULUS
4ATTN THERM EXPN TENS COMP SHEAR CRIPLING /
2020 FORMAT(1X,14,16,2X,F14.4)
END

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PL AN5610
PI AN5620
PL AN5630
PI AN5640
PL AN5650
PI AN5660
PL AN5670
PI AN5680
PL AN5690
PI AN5700
PL AN5710
PI AN5720
PL AN5730
PI AN5740
PL AN5750
PI AN5760
PL AN5770
PI AN5780
PL AN5790
PI AN5800
PL AN5810
PI AN5820
PL AN5830
PI AN5840
PL AN5850
PI AN5860
PL AN5870
PI AN5880
PL AN5890
PI AN5900
PI AN5910
PI AN5920
PI AN5930

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```

SUBROUTINE DP1AN1 (ADLN,ANFW,LOAD,NUMDV)
C*****
C-----DESIGN OF STIFFENED MEMBRANE ELEMENT
C*****
DIMENSION ADLN(NUMDV),ANFW(NUMDV),LOAD(NUMDV)
COMMON/JUNK/,HIN(16),LT,LH,L,SG(20),SIG(7),IDVAR,IFX,FRC,ARFA,
1 XINFR1,RETA,TENS,COMP,SHEAR,CRIUSH,TAU,SRC,PRC,GRC,JUNI(240)
PX=SIG(4)
PY=SIG(5)
PXY=SIG(6)
C*****
C-----FULLY STRESSED DESIGN
C*****
P1=COMP*TAU*ARFA
P2=COMP*ARFA
P12=SHEAR*ARFA
IF (PX,GT,0.0) P1=TENS*TAU*APFA
IF (PY,GT,0.0) P2=TENS*ARFA
RMAX=(PX/P1)**2+(PY/P2)**2-(PX/P1)*(PY/P2)+(PXY/P12)**2
RMAX=SQRT(RMAX)
IF (PX,GE,0.0) GO TO 100
C*****
C-----STIFFENED FAILURE

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```

PI AN5940
PI AN5950
PI AN5960
PI AN5970
PI AN5980
PI AN5990
PI AN6000
PI AN6010
PI AN6020
PI AN6030
PI AN6040
PI AN6050
PI AN6060
PI AN6070
PI AN6080
PI AN6090
PI AN6100
PI AN6110
PI AN6120
PI AN6130
PI AN6140
PI AN6150
PI AN6160

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C*****PI AN6170
P=-PXPI AN6180
PF=SRC*XINERTPI AN6190
AA=P/PFPI AN6200
R=1.0/IFXPI AN6210
R=AA*RPI AN6220
IF (R.GT.RMAX) RMAX=RPI AN6230
P1=CRUSH*TAU*ARFAP1 AN6240
P2=0.5*P1PI AN6250
CALL IDHMS (IFX,P,P1,P2,PF,R)PI AN6260
IF (R.GT.RMAX) RMAX=RPI AN6270
C*****PI AN6280
C-----SHEET BUCKLING BETWEEN STIFFENERSPI AN6290
C*****PI AN6300
100 PX=-PXPI AN6310
PY=-PYPI AN6320
AA=PX+4.0*PY/TAUPI AN6330
BB=1.495*PXY/TAUPI AN6340
R=0.5*(AA+SQR(AA**2+BB**2))/PHCPI AN6350
IF (R.GT.RMAX) RMAX=RPI AN6360
C*****PI AN6370
C-----GENERAL BUCKLING OF PANELPI AN6380
C*****PI AN6390
IF (PX.LT.0.0) GO TO 118PI AN6400
PF=SRC*XINERT*AREAA*ARFAP1 AN6410
AA=PX/PFPI AN6420
R=AA**0.2PI AN6430
IF (R.GT.RMAX) RMAX=RPI AN6440
118 AA=RMAX*ADLN(DVVAR)PI AN6450
IF(AA.LT.ANEW(DVVAR)) GO TO 60PI AN6460
ANEW(DVVAR)=AAP1 AN6470
LOAD(DVVAR)=LPI AN6480
60 CONTINUEPI AN6490
RETURNPI AN6500
ENDPI AN6510

```

```

      SUBROUTINE PLNAX2(IJW1,JD,X,Y,Z,T,NTC,W1,PMAT,NUMDV,NUMNP,NUMMAT, PI AN6520
1 NUMTC,KODE,NUMF) PI AN6530
C-----PI AN6540
C-----PLANF ISOTROPIC MEMBRANE ELEMENTS PI AN6550
C-----PI AN6560
      IMPLICIT REAL*8 (A-H,O-Z) PI AN6570
      REAL*4 IJW1,X,Y,Z,T,W1,PMAT,REF1,F4,F5,F6,FRC PI AN6580
      DIMENSION IJW1(NUMDV),JD(NUMNP,6),X(NUMNP),Y(NUMNP),Z(NUMNP), PI AN6590
      IT(NUMNP),NTC(NUMMAT),W1(NUMMAT),PMAT(NUMTC,7,NUMMAT) PI AN6600
      COMMON/FM/LM(12),S(12,12),P(12,4,2),XM(12),ST(15,12),TT(15,4), PI AN6610
      I RR(12,12),FM(11891) PI AN6620
      COMMON/JUNK/IF(4),IX(4),EMUL(4,5),D(3,3),XX(4),YY(4),ZZ(4),TMP(4), PI AN6630
      I ALP(3),TTI(3),PRESS,RFFT,NS,JUN1,EE(6),JUN(172) PI AN6640
      COMMON/UNIT5/IR,IW,IP,I1,I2,I3,IR,[9,110,111,112 PI AN6650
C-----PI AN6660
C-----CONTROL INFORMATION PI AN6670
C-----PI AN6680
      NI=1 PI AN6690
      ND=12 PI AN6700
      NV=2 PI AN6710
      NW=1 PI AN6720
      NI=4 PI AN6730
      IFX=0 PI AN6740
      WRITE(IW,2000)NUMF,KODE,NUMMAT,NUMTC PI AN6750
C-----PI AN6760
C-----MATRIAL PROPERTY CARDS PI AN6770
C-----PI AN6780
      WRITE(IW,2019) PI AN6790
      DO 60 M=1,NUMMAT PI AN6800
      READ(IR,1010) N,NTC(N),WT(N) PI AN6810
      IF(NTC(N).LE.0) NTC(N)=1 PI AN6820
      WRITE(IW,2020) N,NTC(N),WT(N) PI AN6830
C-----PI AN6840
C-----TEMPERATURE DEPENDENT MATERIAL PROPERTIES PI AN6850
C-----PI AN6860
      NT=NTC(N) PI AN6870
      READ(IR,1005) ((PMAT(I,J,N),J=1,7),I=1,NT) PI AN6880
      DO 10 I=1,NT PI AN6890
      IF(PMAT(I,6,N).LE.0.) PMAT(I,6,N)=PMAT(I,5,N) PI AN6900
      10 CONTINUE PI AN6910
      60 WRITE(IW,2010) ((PMAT(I,J,N),J=1,7),I=1,NT) PI AN6920
C-----PI AN6930
C-----ELEMENT LOAD MULTIPLERS PI AN6940
C-----PI AN6950
      READ(IR,1002) ((FMUL(I,J),J=1,5),I=1,4) PI AN6960
      WRITE(IW,2004) ((FMUL(I,J),J=1,5),I=1,4) PI AN6970
C-----PI AN6980
C-----ELEMENT CARDS PI AN6990
C-----PI AN7000
      WRITE(IW,2002) PI AN7010
      N=1 PI AN7020
      130 READ(IR,1003) IF1,IF,IMAT,INDV,FRC,RFFT,PRESS,BETA,NS,INC PI AN7030
      IF (FRC.LE.0.) FRC=1. PI AN7040
      IF(INC.FE.0.) INC=1 PI AN7050
      IF(NS.FE.0.) NS=3 PI AN7060
      IF(NS.LE.3) NS=1 PI AN7070
      IF(1IF(3).FE.0. IF(4)).AND.(NS.FE.15)) NS=12 PI AN7080
      RHO=WT(IMAT) PI AN7090
      THICK=1.0 PI AN7100
      RFT=RFTA PI AN7110

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      KK=INC*(IFL-N)
      DO 142 I=1,4
142  IX(I)=IF(I)-KK
      DO 500 NEL=N,IFL
      TFMP=0.
      DO 501 I=1,4
      II=IX(I)
      TFMP=TFMP+T(II)*0.25
      XX(I)=Y(II)
      YY(I)=Y(II)
501  ZZ(I)=Z(II)
C*****
C-----INTERPOLATE MATERIAL PROPERTIES FOR AVERAGE ELEMENT TEMPERATURE
C*****
      CALL INTERP(MAT,FF,NUMTC,NUMMAT,7,6,NTC(I,MAT),IMAT,TEMP)
      F4=FF(4)
      F5=FF(5)
      F6=FF(6)
C*****
C-----FORM CONSTITUTIVE LAW AND COMPUTE THERMAL STRESSES
C*****
      DO 265 I=1,3
      DO 265 J=1,3
265  D(I,J)=0.
      D(2,2)=1.0/FF(1)
      D(1,1)=D(2,2)
      D(1,2)=-D(1,1)*FF(2)
      D(2,1)=D(1,2)
      D(3,3)=D(2,2)*2.0*(1.0+FF(2))
      ALP(1)=FF(3)
      ALP(2)=FF(3)
      ALP(3)=0.
      CALL FLAW(0,000)
C*****
C-----FORM ELEMENT LOCATION MATRIX AND COMPUTE ELEMENT MATRICES
C*****
      DO 170 I=1,4
      II=IX(I)
      TMP(I)=T(II)
      LM(I)=ID(II,1)
      LM(I+4)=ID(II,2)
170  LM(I+8)=ID(II,3)
      CALL QUAD(RHO,THICK)
      AREA=XM(1)+XM(2)+XM(3)+XM(4)
      IWT(IDV)=IWT(IDV)+AREA*RHO*FRC
C*****
C-----CALCULATE RANDWIDTH AND WRITE ELEMENT INFO. ON TAPES
C*****
      NN=NS*ND*NI
      CALL RFARAN(ST,ST,15,12,1,NS,ND,NI,NN)
      NN=NS*4*NW
      CALL RFARAN(IT,IT,15,4,1,NS,4,NW,NN)
      CALL CALRAN(NDIF,LM,S,P,ST,TT,NU,NV,NS,ND,NW,IDV,IFX,FRC)
      WRITE(I8) NI,RFI,F4,E5,F6
      WRITE(IW,2003) NEL,IX,IMAT,IDV,FRC,REF1,PRESS,BETA,NS,NDIF
      DO 450 I=1,4
450  IX(I)=IX(I)+INC
500  CONTINUE
      N=IFL+1
      IF(N,LF,NUMF) GO TO 130

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PI AN7120
PI AN7130
PI AN7140
PI AN7150
PI AN7160
PI AN7170
PI AN7180
PI AN7190
PI AN7200
PI AN7210
PI AN7220
PI AN7230
PI AN7240
PI AN7250
PI AN7260
PI AN7270
PI AN7280
PI AN7290
PI AN7300
PI AN7310
PI AN7320
PI AN7330
PI AN7340
PI AN7350
PI AN7360
PI AN7370
PI AN7380
PI AN7390
PI AN7400
PI AN7410
PI AN7420
PI AN7430
PI AN7440
PI AN7450
PI AN7460
PI AN7470
PI AN7480
PI AN7490
PI AN7500
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PI AN7570
PI AN7580
PI AN7590
PI AN7600
PI AN7610
PI AN7620
PI AN7630
PI AN7640
PI AN7650
PI AN7660
PI AN7670
PI AN7680
PI AN7690
PI AN7700
PI AN7710

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      RETURN                                PL AN7720
1002 FORMAT(5F10.0)                        PL AN7730
1003 FORMAT(7I5,F5.0,3F10.0,2I5)          PL AN7740
1005 FORMAT (7F10.0)                       PL AN7750
1010 FORMAT(2I5, F10.0)                   PL AN7760
2000 FORMAT(44H)NUMBER OF MEMBRANE ELEMENTS      =,I5 /      PL AN7770
1      44H CONSTRUCTION CODE                      =,I5/      PL AN7780
2      44H NUMBER OF MATERIALS                    =,I5/      PL AN7790
3      44H NUMBER OF TEMPS FOR WHICH MATL PROPS GIVEN=,I5)  PL AN7800
2002 FORMAT(/ /23H PROCESSED ELEMENT DATA//      PL AN7810
1 9TH ELEMNT/-----NODES-----//ID NOS-/      DEF VAR      REFERENCE      PL AN7820
2                                PRMT RAND ./      PL AN7830
3 9TH NUMBR I      J      K      L      MAT DV      FRACTION      TEMP      PL AN7840
4PRESSURE      BETA      CODE WOTH      /)      PL AN7850
2003 FORMAT(1X,7I5,4F12.4,2I6)              PL AN7860
2004 FORMAT(23H ELEMENT LOAD FRACTIONS//71H LOAD CASE TEMPERATURE      PREPL AN7870
1SSURE X-DIRECTION Y-DIRECTION Z-DIRECTION /      PL AN7880
2 6X .1HA .3X .5F12.3/ 6X .1HB .3X .5F12.3/ 6X .1HC .3X .5F12.3/      PL AN7890
3 6X .1HD .3X .5F12.3 )      PL AN7900
2010 FORMAT(1H+,27X,7F14.4 /(28X,7F14.4))      PL AN7910
2019 FORMAT(/ /25H MATERIAL PROPERTY CARDS /      PL AN7920
1/125H MATL NO OF SPECIFIC      YOUNGS      POIPL AN7930
2SSONS      COEFFT OF /-----ALLOWABLE STRESSES-----/      PL AN7940
3/121H NBR      TEMP      WEIGHT      TEMPERATURE      MODULUS      RPL AN7950
4ATTN      THERM EXPN      TENSION      COMPRESSION      SHEAR/)      PL AN7960
2020 FORMAT(1X,I4,I6,2X,F14.4)              PL AN7970
      END                                PL AN7980

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      SUBROUTINE DPLAN2 (AOLD,ANFW,LOAD,NUMDV)      PL AN7990
C*****                                PL AN8000
C-----STRESS DESIGN OF ISOTROPIC MEMBRANE ELEMENT      PL AN8010
C*****                                PL AN8020
      DIMENSION AOLD(NUMDV),ANFW(NUMDV),LOAD(NUMDV)      PL AN8030
      COMMON/JUNK/JUN(16),L1,LH,L,SG(20),SIG(7),IDVAR,IFX,FRC,AREA,      PL AN8040
1 XINERT,BETA,TFMS,COMP,SHEAR,JUN1(245)      PL AN8050
      CC=(SIG(1)+SIG(2))*0.5      PL AN8060
      RR=(SIG(1)-SIG(2))*0.5      PL AN8070
      CR=SQRT(RR*RR+SIG(3)**2)      PL AN8080
      PX=CC+CR      PL AN8090
      PY=CC-CR      PL AN8100
      P1=COMP*ARFA      PL AN8110
      P2=COMP*ARFA      PL AN8120
      IF (PX.GT.0.0) P1=TFMS *ARFA      PL AN8130
      IF (PY.GT.0.0) P2=TFMS*ARFA      PL AN8140
      RMAX=(PX/P1)**2+(PY/P2)**2-(PX/P1)*(PY/P2)      PL AN8150
      RMAX=SQRT(RMAX)      PL AN8160
      IF(SHEAR.FD.0.) GO TO 50      PL AN8170
      PXY=CR/(ARFA*SHEAR)      PL AN8180
      IF(RMAX.I.T.PXY) RMAX=PXY      PL AN8190
50 AA=RMAX*AOLD(IDVAR)      PL AN8200
      IF(AA.I.T.ANFW(IDVAR)) GO TO 60      PL AN8210
      ANFW(IDVAR)=AA      PL AN8220
      LOAD(IDVAR)=1      PL AN8230
60 RETURN      PL AN8240
      END                                PL AN8250

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```

      SUBROUTINE SHEAR(A,MTOT)
C*****
C-----SHEAR PANEL ELEMENTS
C*****
      DIMENSION A(MTOT)
      COMMON /ELPAR/ NPAR(4),NIMNP,MRAND,NELTYP,N1,N2,N3,N4,N5,MTIT,NFQ
      1,NIMFL,NIMDV,M1,M2,M3,LL,LR,NFOR,NRLOCK
      COMMON/JUNK/,JUN(16),LT,LH,L,SIG(27),IDVAR,TEX,FRC,AREA,XINERT,
      1,JUN1(249)
      COMMON/UNITS/IR,IW,IP,I1,I2,I3,IR,IR,I10,I11,I12
      NIMF=NPAR(2)
      KODF=NPAR(5)
      IF(NPAR(1).EQ.0)GO TO 500
      N6=N5+NIMNP
      GO TO (1,2),KODF
C*****
C-----SHEAR PANEL WITH STRESS AND BUCKLING CONSTRAINTS
C*****
      1 NIMMAT=NPAR(3)
      NIMTC=NPAR(4)
      N7=N6+NIMMAT
      NR=N7+NIMMAT
      N9=NR+NIMMAT+NIMTC*4
      MM=N9-MTIT
      IF(MM.GT.0)CALL ERROR(MM)
      CALL PANFL(A(M1),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),
      1 A(NR),NIMDV,NIMNP,NIMMAT,NIMTC,KODF,NIMF)
      RETURN
C*****
C-----PROVISION FOR SPECIAL SHEAR PANEL ELEMENT
C*****
      2 CALL NOELEM(NPAR(1),NPAR(5),IW)
      RETURN
      500 WRITE(IW,2002) KODF
      DO 800 MM=1,NIMF
      CALL STRSC(A(M1),A(N1),A(N3),NFQ,NIMDV,LL,LR,IR,0)
      AB=A(IDVAR)*FRC
      WRITE(IW,2005) MM,AB
      DO 800 L=LT,LH
      IF(L.GT.IT) WRITE(IW,2006)
      CALL STRSC(A(M1),A(N1),A(N3),NFQ,NIMDV,LL,LR,IR,1)
      SIG(5) = (SIG(1)+SIG(2)+SIG(3)+SIG(4)) *0.25
      WRITE(IW,2007) L,(SIG(1),I=1,5)
      GO TO (3,4),KODF
C*****
C-----DESIGN OF SHEAR PANEL WITH STRESS AND BUCKLING CONSTRAINTS
C*****
      3 CALL DPANEL(A(M1),A(M2),A(M3),NIMDV)
      GO TO 800
C*****
C-----PROVISION FOR DESIGN OF SPECIAL SHEAR PANEL ELEMENT
C*****
      4 CONTINUE
      800 CONTINUE
      RETURN
      2002 FORMAT(/40H ANALYSIS OF SHEAR PANELS, CONSTRM CODE=,I2 //
      1 92H
      2DES-----/ AVERAGE /-----SHEAR FLOW AT N)
      3 92H ELEMENT THICKNESS COND
      4K L SHEAR FLOW /)

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```

      SHEAR0000
      SHEAR0010
      SHEAR0020
      SHEAR0030
      SHEAR0040
      SHEAR0050
      SHEAR0060
      SHEAR0070
      SHEAR0080
      SHEAR0090
      SHEAR0100
      SHEAR0110
      SHEAR0120
      SHEAR0130
      SHEAR0140
      SHEAR0150
      SHEAR0160
      SHEAR0170
      SHEAR0180
      SHEAR0190
      SHEAR0200
      SHEAR0210
      SHEAR0220
      SHEAR0230
      SHEAR0240
      SHEAR0250
      SHEAR0260
      SHEAR0270
      SHEAR0280
      SHEAR0290
      SHEAR0300
      SHEAR0310
      SHEAR0320
      SHEAR0330
      SHEAR0340
      SHEAR0350
      SHEAR0360
      SHEAR0370
      SHEAR0380
      SHEAR0390
      SHEAR0400
      SHEAR0410
      SHEAR0420
      SHEAR0430
      SHEAR0440
      SHEAR0450
      SHEAR0460
      SHEAR0470
      SHEAR0480
      SHEAR0490
      SHEAR0500
      SHEAR0510
      SHEAR0520
      SHEAR0530
      SHEAR0540
      SHEAR0550
      SHEAR0560
      SHEAR0570
      SHEAR0580
      SHEAR0590

```


2005	FORMAT(J6,IX,F15.4)	SHER0600
2006	FORMAT(/)	SHER0610
2007	FORMAT(1H+,23X,I5,1X,5F12.4)	SHER0620
	END	SHER0630

```

      SUBROUTINE PANFL(IJW,T,IX,Y,Z,T,NTC,WT,PMAT,NUMDV,NUMNP,NUMMAT,
1) NUMTC,KODE,NUMF)
C*****
C-----SHEAR PANFL ELEMENTS
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      REAL*4 IJW,T,X,Y,Z,T,WT,PMAT,FRC,F3,SHCR
      DIMENSION IJW( NUMDV ),ID( NUMNP,6 ),X( NUMNP ),Y( NUMNP ),Z( NUMNP ),
1T( NUMNP ),NTC( NUMMAT ),WT( NUMMAT ),PMAT( NUMTC,4,NUMMAT ),CC( 6,2 )
      COMMON/FM/LM(12),S(12,12),P(12,4),ST(4,12),TT(4,4),XM(12),
1 FM(12259)
      COMMON/JUNK/FMUJ(3,4),IF(4),IX(4),XX(4),YY(4),ZZ(4),EF(3),AREA,
1 TF(4,2),U(4),V(4),O(4),D(4),P1,P2,JUN1(184)
      COMMON/UNITS/IR,IY,IP,II,I2,I3,IR,I9,I10,I11,I12
      DATA CC/5.35, 8.99, 8.99, 5.35, 5.35, 7.07,
1 3.99, 5.72, 3.29, 7.25, 5.63, 3.91 /
C*****
C-----CONTROL INFORMATION
C*****
      NI=1
      NV=1
      NW=1
      ND=12
      NS=4
      IFX=3
      NJ=2
      WRITE(IW,2000)NUMF,KODE,NUMMAT,NUMTC
C*****
C-----MATERIAL PROPERTY CARDS
C*****
      WRITE(IW,2001)
      DO 5 M=1,NUMMAT
      READ(IR,1001) N,NTC(N),WT(N)
      IF (NTC(N).EQ.0) NTC(N)=1
      WRITE(IW,2002) N,NTC(N),WT(N)
C*****
C-----TEMPERATURE DEPENDENT MATERIAL PROPERTIES
C*****
      NT=NTC(N)
      DO 5 J=1,NT
      READ(IR,5001) (PMAT(J,K,N),K=1,4)
      IF (J.NF.1) WRITE(IW,6002)
      5 WRITE(IW,6003) (PMAT(J,K,N),K=1,4)
C*****
C-----ELEMENT LOAD MULTIPLIERS
C*****
      READ(IR,1003) (FMUJ(I,J),J=1,4),I=1,3)
      WRITE(IW,2003) (FMUJ(I,J),J=1,4),I=1,3)
C*****
C-----ELEMENT CARDS
C*****

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```

      WRITE(IW,2005)
      N=1
      6 READ(IR,1004) IFL,IF,IMAT,IND,ISU,FRC,AL,BL,INC
      IF(INC.F0.0) INC=1
      IF(FRC.LF.0.0) FRC=1.0
      IF(IMAT.F0.0) IMAT=1
      RHO=WT(IMAT)
      KK=INC*(IFL-N)
      DO 50 J=1,4
      50 IX(J)=IF(J)-KK
      DO 500 NFI=N,IFL
      TFMP=0.
      DO 100 I=1,4
      II=IX(I)
      XX(I)=X(II)
      YY(I)=Y(II)
      ZZ(I)=Z(II)
      100 TFMP=TFMP+T(II)*0.25
      C*****
      C-----INTERPOLATE MATERIAL PROPERTIES FOR AVERAGE ELEMENT TEMPERATURE
      C*****
      CALL INTERP(PMAT,FF,NUMTC,NUMMAT,4,3,NTC(IMAT),IMAT,TFMP)
      F3=FF(2)
      C*****
      C-----FORM ELEMENT UNIT MATRICES AND LOAD VECTORS
      C*****
      SMOD=0.5*FF(1)/(1.0+FF(2))
      CALL FPANEL(SMOD,FF(2),RHO,XL,YL,NEL,IW)
      C*****
      C-----COMPUTE BUCKLING DATA
      C*****
      SHCR=0.
      IF(ISU.F0.0) GO TO 121
      IF(XL.GF.YL) GO TO 120
      H=YL
      YL=XL
      XL=H
      120 IF(AL.LF.0.) AL=XL
      IF(BL.LF.0.) BL=YL
      H=CC(ISU,1)+CC(ISU,2)*BL*BL/(AL*AL)
      SHCR=H*0.8696*FF(1)/(12.0*BL*BL*(1.0-FF(2)*FF(2)))
      121 IWT(IND)=IWT(IND)+RHO*AREA*FRC
      C*****
      C-----FORM LOCATION MATRIX AND COMPUTE BAND WIDTH
      C*****
      DO 470 J=1,4
      II=IX(J)
      DO 470 J=1,3
      IJ=(I-1)*3+J
      470 LM(IJ)=ID(II,IJ)
      CALL CALBAN(INF,LM,S,P,ST,IT,NH,NV,NS,MN,NW,IND,IFX,FRC)
      WRITE(IR) NI,F3,SHCR
      WRITE(IW,2004) NFI,IX,IMAT,IND,ISU,FRC,AL,BL,NFI
      C*****
      C-----CHECK FOR MORE ELEMENTS
      C*****
      DO 450 J=1,4
      450 IX(J)=IX(J)+INC
      500 CONTINUE
      N=IFL+1

```

```

SHFR1150
SHFR1160
SHFR1170
SHFR1180
SHFR1190
SHFR1200
SHFR1210
SHFR1220
SHFR1230
SHFR1240
SHFR1250
SHFR1260
SHFR1270
SHFR1280
SHFR1290
SHFR1300
SHFR1310
SHFR1320
SHFR1330
SHFR1340
SHFR1350
SHFR1360
SHFR1370
SHFR1380
SHFR1390
SHFR1400
SHFR1410
SHFR1420
SHFR1430
SHFR1440
SHFR1450
SHFR1460
SHFR1470
SHFR1480
SHFR1490
SHFR1500
SHFR1510
SHFR1520
SHFR1530
SHFR1540
SHFR1550
SHFR1560
SHFR1570
SHFR1580
SHFR1590
SHFR1600
SHFR1610
SHFR1620
SHFR1630
SHFR1640
SHFR1650
SHFR1660
SHFR1670
SHFR1680
SHFR1690
SHFR1700
SHFR1710
SHFR1720
SHFR1730
SHFR1740

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```

      IF(N,I,F,NUMF) GO TO 6
      RETURN
1001 FORMAT(2I5,F10.0)
1003 FORMAT(4F10.0)
1004 FORMAT(8I5,3F10.0,I5)
2000 FORMAT(44H)NUMBER OF SHEAR PANEL ELEMENTS          =,I5/
1      44H CONSTRUCTION CODE                          =,I5/
2      44H NUMBER OF MATERIALS                        =,I5/
4      44H NUMBER OF TEMPS FOR WHICH MATL PROPS GIVEN=,I5)
2001 FORMAT(/ / 25H MATERIAL PROPERTY CARDS //
191H MATERIAL  NUMBER    SPECIFIC          YOUNGS    POISSNS
2      ALLOWABLE      /
391H  NUMBER OF TEMPS    WEIGHT    TEMP    MODULUS    RATIO
4      SHEAR          /)
2002 FORMAT(16,5X,I5,F12.4)
2003 FORMAT(/ / 25H ELEMENT LOAD MULTIPLIERS //20X,1HA,14X,1HB,14X,1HC,
1 14X,1HD, /6H X-DIR,4F15.6/ 6H Y-DIR,4F15.6/ 6H Z-DIR,4F15.6 )
2004 FORMAT(17,2X,4I6,3I7,3F12.4,I6)
2005 FORMAT(/ / 23H PROCESSED ELEMENT DATA//
196H ELEMENT /-----NODE NOS-----//--FL ID NOS--/  ROUNO    DFS V
2AR /-----EFFECT PANEL DIMNS--/  BAND  /
396H  NUMBER    I      J      K      L  MATL  D VAR    CODE  FRACTI
40N    LONGER    SHORTER  WIDTH  /)
5001 FORMAT(4F10.0)
6002 FORMAT(/)
6003 FORMAT(1H+,30X,4F12.4)
      FMD

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SHFR1750
SHFR1760
SHFR1770
SHFR1780
SHFR1790
SHFR1800
SHFR1810
SHFR1820
SHFR1830
SHFR1840
SHFR1850
SHFR1860
SHFR1870
SHFR1880
SHFR1890
SHFR1900
SHFR1910
SHFR1920
SHFR1930
SHFR1940
SHFR1950
SHFR1960
SHFR1970
SHFR1980
SHFR1990
SHFR2000
SHFR2010

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```

      SUBROUTINE FPAFEL(G,GG,RHO,XL,YL,MK,IW)
      C*****
      C-----FORM SHEAR PANEL ELEMENT MATRICES
      C*****
      IMPLCIT REAL*8 (A-H,O-Z)
      COMMON/SHINK/EMUL(3,4),IF(4),IX(4),X(4),Y(4),Z(4),EF(3),AREA,
      1 TF(4,2),U(4),V(4),W(4),P1,P2,VN1(4),VN2(4),V12(4),
      2 V41(4),VP12(4),TI(3),TJ(3),JHN(132)
      COMMON/EM/LM(12),S(12,12),P(12,4),ST(4,12),TT(4,4),XM(12),
      1 FMM(2259)
      C*****
      C-----INIT VECTORS ALONG DIAGONALS, SIDES AND NORMAL TO THE MEANPLANE
      C*****
      CALL VEC1DR(VN1,X(1),Y(1),Z(1),X(3),Y(3),Z(3))
      CALL VEC1DR(VN2,X(2),Y(2),Z(2),X(4),Y(4),Z(4))
      CALL VEC1DR(V12,X(1),Y(1),Z(1),X(2),Y(2),Z(2))
      CALL VEC1DR(V41,X(4),Y(4),Z(4),X(1),Y(1),Z(1))
      CALL CROSS(VN1,VN2,N)
      AREA=0.5*VN1(4)*VN2(4)*N(4)
      C*****
      C-----FORM TRANSFORMATION MATRIX TF
      C*****
      HH=0NT(V12,N)
      N(1:3)=1,3
      10 VP12(1)=(V12(1)-HH*N(1))*V12(4)
      VP12(4)=0SORT(VP12(1)*VP12(1)+VP12(2)*VP12(2)+VP12(3)*VP12(3))
      N(1:3)=1,3
      20 TF(1,1)=VP12(1)/VP12(4)
      CALL CROSS(N,TF,TF(1,2))
      C*****
      C-----COMPUTE ELEMENT CORNER COORDINATES IN LOCAL AXES SYSTEM
      C*****
      X1=0.0
      Y1=0.0
      X2=VP12(4)
      Y2=0.0
      X3=0NT(TF,VN1)*VN1(4)
      Y3=0NT(TF(1,2),VN1)*VN1(4)
      X4=-0NT(TF,V41)*V41(4)
      Y4=-0NT(TF(1,2),V41)*V41(4)
      XL=0.5*(X2-X1+X3-X4)
      YL=0.5*(Y3+Y4)
      X34=X3-Y3*X4/Y4
      Y34=Y3+X3*X4/Y4
      IF(Y3.LT..01.AND.Y4.LT..01.AND.X34.LT..01.AND.X42.GT..01) GO TO 2006
      GO TO 57
      2006 WRITF(IW,2007) MK
      STOP
      C*****
      C-----TEST FOR PARALLEL SIDES
      C*****
      57 A1=0ARS(Y3-Y4)/(X3-X4)
      A2=0ARS(Y4*(X3-X2)-Y3*X4)/(X4*(X3-X2)+Y4*Y3)
      IF(A1.LF..01.AND.A2.LF..01) GO TO 40
      IF(A1.LF..01) GO TO 30
      IF(A2.LF..01) GO TO 35
      GO TO 45
      C*****
      C-----CASE WHEN SIDES 1 AND 3 ARE PARALLEL
      C*****

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SHFR2610

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30 YP=X2*Y3*Y4/(Y3*X4-Y4*(X3-X2))
P1=YP-Y1
P2=YP-Y2
P3=YP-Y3
P4=YP-Y4
XP=X2*Y3*X4/(Y3*X4-Y4*(X3-X2))
AA=(X2-XP)/YP
CC=(X1-XP)/YP
H=P1*P2*ARF A/(P3*P4*2.0*G)
H=H+H*(AA*AA+AA*CC+CC*CC)/(1.5*(1.0+GG))
GN TN 46
*****
C-----CASE WHEN S1DFS 2 AND 4 ARF PARALLEL FL
*****
35 DN=-0.5*(X4/Y4+(X3-X2)/Y3)
XN=X4-(X3-X4)*Y4/(Y3-Y4)
DN=1.0/DSORT(1.0+DN*DN)
P1=(XN-X1-Y1*DN)*AN
P2=(XN-X2-Y2*DN)*AN
P3=(XN-X3-Y3*DN)*AN
P4=(XN-X4-Y4*DN)*AN
RR=(XN-X4)*DN+Y4/(XN-X4-Y4*DN)
H=P1*P2*ARF A/(P3*P4*2.0*G)
H=H+H*(RR*RR+RR*DN+DN*DN)/(1.5*(1.0+GG))
GN TN 46
*****
C-----PARALLEL FL PROGRAM CASE
*****
40 P1=1.0
P2=1.0
P3=1.0
P4=1.0
DN=-0.5*(X4/Y4+(X3-X2)/Y3+(Y3-Y4)/(X3-X4))
H=0.5*ARF A*(1.0+2.0*DN*DN/(1.0+GG))/G
GN TN 46
*****
C-----CASE WHEN NO PARALLEL S1DFS ARF PRESENT
*****
45 XN=X4-(X3-X4)*Y4/(Y3-Y4)
XP=X2*X4*Y3/(Y3*X4-Y4*(X3-X2))
YP=X2*Y3*Y4/(Y3*X4-Y4*(X3-X2))
DJS=DSORT((XN-XP)*(XN-XP)+YP*YP)
DN=(XN-XP)/YP
P1=YP*(XN-X1-Y1*DN)/DJS
P2=YP*(XN-X2-Y2*DN)/DJS
P3=YP*(XN-X3-Y3*DN)/DJS
P4=YP*(XN-X4-Y4*DN)/DJS
CC=DJS/P1-DN
RR=DJS/P4-CC
AA=DJS/P2-DN
F=(AA+RR+(AA**3+RR**3)/1.5+0.2*(AA**5+RR**5))*DLNG(DABS(AA+RR))
1+(CC+DN+(CC**3+DN**3)/1.5+0.2*(CC**5+DN**5))*DLNG(DABS(CC+DN))
2-(RR+CC+(RR**3+CC**3)/1.5+0.2*(RR**5+CC**5))*DLNG(DABS(RR+CC))
3-(DN+AA+(DN**3+AA**3)/1.5+0.2*(DN**5+AA**5))*DLNG(DABS(DN+AA))
4+0.1*(AA*AA-CC*CC)*(RR**3-DN**3)+(RR*RR-DN*DN)*(AA**3-CC**3)
5-0.2*(AA-CC)*(RR**4-DN**4)+(RR-DN)*(AA**4-CC**4)
F=F*P1*P2*P3*P4*0.5/(DJS*DJS)
H=0.5*P1*P2*(ARF A+4.0*(F-ARF A/1.5)/(1.0+GG))/(P3*P4*G)
*****
C-----DEFINITION OF S1DFS MACRO
*****

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SHFR2620
SHFR2630
SHFR2640
SHFR2650
SHFR2660
SHFR2670
SHFR2680
SHFR2690
SHFR2700
SHFR2710
SHFR2720
SHFR2730
SHFR2740
SHFR2750
SHFR2760
SHFR2770
SHFR2780
SHFR2790
SHFR2800
SHFR2810
SHFR2820
SHFR2830
SHFR2840
SHFR2850
SHFR2860
SHFR2870
SHFR2880
SHFR2890
SHFR2900
SHFR2910
SHFR2920
SHFR2930
SHFR2940
SHFR2950
SHFR2960
SHFR2970
SHFR2980
SHFR2990
SHFR3000
SHFR3010
SHFR3020
SHFR3030
SHFR3040
SHFR3050
SHFR3060
SHFR3070
SHFR3080
SHFR3090
SHFR3100
SHFR3110
SHFR3120
SHFR3130
SHFR3140
SHFR3150
SHFR3160
SHFR3170
SHFR3180
SHFR3190
SHFR3200
SHFR3210

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```

C*****SHFR3270
46 DF13=DSORT(X3*Y3+Y3*Y3)SHFR3230
   DF24=DSORT(X4-X2)*(X4-X2)+Y4*Y4)SHFR3240
   U(1)=X3/DF13SHFR3250
   U(2)=(X4-X2)/DF24SHFR3260
   V(1)=Y3/DF13SHFR3270
   V(2)=Y4/DF24SHFR3280
   DO 47 I=3,4SHFR3290
   U(I)=U(I-2)SHFR3300
47 V(I)=V(I-2)SHFR3310
   O(1)=-X2*Y4*DF13*0.5/(X4*Y3-X3*Y4)SHFR3320
   O(2)=X2*Y3*DF24*0.5/(X4*Y3-X3*Y4-X2*(Y3-Y4))SHFR3330
   O(3)=-O(1)SHFR3340
   O(4)=-O(2)SHFR3350
   DO 100 I=1,4SHFR3360
   DO 100 J=1,4SHFR3370
   O(I,J)=O(I,J)*0.5/HSHFR3380
   DO 150 L=1,3SHFR3390
   T(L)=TF(L,1)*U(1)+TF(L,2)*V(1)SHFR3400
150 T(J,L)=U(J)*TF(L,1)+V(J)*TF(L,2)SHFR3410
   DO 160 L=1,3SHFR3420
   DO 160 NN=1,3SHFR3430
   I1=3*(I-1)+LSHFR3440
   J1=3*(J-1)+NNSHFR3450
160 S(I1,J1)=T(L)*T(J,NN)*O(I,J)SHFR3460
100 CONTINUESHFR3470
   DO 180 L=1,12SHFR3480
   DO 180 M=L,12SHFR3490
180 S(L,M)=S(M,L)SHFR3500
C*****SHFR3510
C-----DEFINITION OF STRESS RECOVERY MATRIXSHFR3520
C*****SHFR3530
   DO 300 I=1,4SHFR3540
   I1=(I-1)*3SHFR3550
   SM=-O(I)*0.5/HSHFR3560
   S(I1,I1+1)=SM*(U(1)*TF(1,1)+V(1)*TF(1,2))SHFR3570
   S(I1,I1+2)=SM*(U(1)*TF(2,1)+V(1)*TF(2,2))SHFR3580
300 S(I1,I1+3)=SM*(U(1)*TF(3,1)+V(1)*TF(3,2))SHFR3590
   DO 400 J=1,12SHFR3600
   S(J)=S(I),J)SHFR3610
   S(2,J)=S(1)*P1/P2SHFR3620
   S(3,J)=S(1)*P1*P2/(P3*P3)SHFR3630
   S(4,J)=S(1)*P1*P2/(P4*P4)SHFR3640
400 S(1,J)=S(1)*P2/P1SHFR3650
C*****SHFR3660
C-----GRAVITY AND INERTIA LOADS SHFR3670
C*****SHFR3680
   A1=0.5*X2*Y4SHFR3690
   A2=0.5*X2*Y3SHFR3700
   A3=ARFA-A1SHFR3710
   A4=ARFA-A2SHFR3720
   WTT=RH0/3.0SHFR3730
   F1=(A4+A1+A2)*WTTSHFR3740
   F2=(A1+A2+A3)*WTTSHFR3750
   F3=(A2+A3+A4)*WTTSHFR3760
   F4=(A3+A4+A1)*WTTSHFR3770
   DO 450 I=1,3SHFR3780
   XM(I)=F1SHFR3790
   XM(I+3)=F2SHFR3800
   XM(I+6)=F3SHFR3810

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      XM(I+9)=F4                      SHER3820
      DO 450 I=1,4                     SHER3830
      HH=FMMH(I,I)                     SHER3840
      P(I,I)=HH*F1                      SHER3850
      P(I+3,I)=HH*F2                   SHER3860
      P(I+6,I)=HH*F3                   SHER3870
450  P(I+9,I)=HH*F4                     SHER3880
      DO 460 I=1,4                     SHER3890
      DO 460 J=1,4                     SHER3900
460  TT(I,I)=0.0                       SHER3910
      RETURN                             SHER3920
2007 FORMAT(1X,'ONE OF THE INTERIOR ANGLES FOR SHEAR PANEL NO.=',I5,
1 IS GREATER THAN 180 DEGREES.') SHER3930
      END                               SHER3940
                                         SHER3950

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      SUBROUTINE DPANEL(ADLN,ANFW,LNAD,NUMDV) SHER3960
C***** SHER3970
C-----DESIGN OF SHEAR PANEL ELEMENTS SHER3980
C***** SHER3990
      DIMENSION ADLN(NUMDV),ANFW(NUMDV),LNAD(NUMDV) SHER4000
      COMMON/JUNK/,IUN(16),LT,LH,L,SG(27),IDVAR,IFX,ERC,AREA,XINFRT, SHER4010
      1 SHEAR,SHCR,UM(247) SHER4020
C***** SHER4030
C-----CHECK SHEAR STRESS SHER4040
C***** SHER4050
      SHFLW=ABS(SG(5)) SHER4060
      RMAX=SHFLW/(SHEAR*AREA) SHER4070
C***** SHER4080
C-----CHECK BUCKLING SHER4090
C***** SHER4100
      IF (SHCR,LT,0.0) GO TO 4 SHER4110
      R=SHFLW/(SHCR*XINFRT) SHER4120
      R=R**0.33333 SHER4130
      3 IF (RMAX,LT,R) RMAX=R SHER4140
C***** SHER4150
C-----FULLY STRESSED DESIGN SHER4160
C***** SHER4170
      4 AA=RMAX*ADLN(IDVAR) SHER4180
      IF(AA,LT,ANFW(IDVAR)) GO TO 60 SHER4190
      ANFW(IDVAR)=AA SHER4200
      LNAD(IDVAR)=L SHER4210
      60 CONTINUE SHER4220
      RETURN SHER4230
      END SHER4240

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      SUBROUTINE SHELL (A,MTOT)
      C*****
C-----PLATE/SHELL ELEMENTS
C*****
      DIMENSION A(MTOT)
      COMMON /FLPAR/ NPAR(14),NUMNP,MRAND,NFLTP,N1,N2,N3,N4,N5,M11T,NFQ
      ,NUMFL,NUMDV,M1,M2,M3,LL,LR,NF0R,NRL0CK
      COMMON/JUNK/JUN(16),LT,LH,L,SG(20),SIG(7),IDV,IFX,FRC,THICK,
1 XINERT,TEN,COMP,SHEAR,RFTA,JUNJ(245)
      COMMON/UNIT/IR,IW,JP,I1,I2,I3,IR,I9,I10,I11,I12
      NUMF= NPAR(2)
      KODF=NPAR(5)
      IF(NPAR(1),FQ,0) GO TO 500
      NIIMAT=NPAR(3)
      NIIMTC=NPAR(4)
      NA=N5+NUMNP
      N7=NA+NIIMAT
      NR=N7+NIIMAT
      GO TO (1,2),KODF
C*****
C-----ISOTROPIC PLATE/SHELL ELEMENTS
C*****
1  NR=NR+NIIMAT*NIIMTC*7
   MM=N9-MTOT
   IF(MM,GT,0) CALL ERROR(MM)
   CALL PLATF1(A(M),A(N1),A(N2),A(N3),A(N4),A(N5),A(N6),A(N7),A(NR),
1 NUMDV,NUMNP,NUMF,NIIMAT,NIIMTC,KODF)
   RETURN
C*****
C-----ORTHOTROPIC PLATE/SHELL ELEMENTS
C*****
2  CALL NOFLFM(NPAR(1),KODF,IW)
   RETURN
500 WRITE(IW,2002) KODF
   DO 800 MM=1,NUMF
     CALL STRSC(A(M),A(N1),A(N3),NFQ,NUMDV,LL,LR,IR,0)
     WRITE(IW,2001) MM,THICK
     TFTA=RFTA/57.2957795
     CR=COS(TFTA)
     SR=SIN(TFTA)
     CSR=CR*SR
     CR=CR*CR
     SR=SR*SR
     DO 800 I=LT,LH
       IF(L,GT,LT) WRITE(IW,2004)
       CALL STRSC(A(M),A(N1),A(N3),NFQ,NUMDV,LL,LR,IR,1)
       IF(RFTA,NF,0.) GO TO 20
       DO 30 J=1,6
30    SIG(I)=SG(I)
       GO TO 40
20    DO 10 J=1,4,3
        C1=SG(J)*CR+SG(J+1)*SR
        C2=2.0*SG(J+2)*CSR
        SIG(I)= C1+C2
        SIG(I+1)=C1-C2
10    SIG(I+2)=(-SG(J)+SG(J+1))*CSR+SG(J+2)*(CR-SR)
40    WRITE(IW,2003) I,(SIG(I),I=1,6)
       GO TO (3,4),KODF
C*****
C-----DESIGN OF ISOTROPIC PLATE/SHELL ELEMENTS

```

```

      SHELL 0000
      SHELL 0010
      SHELL 0020
      SHELL 0030
      SHELL 0040
      SHELL 0050
      SHELL 0060
      SHELL 0070
      SHELL 0080
      SHELL 0090
      SHELL 0100
      SHELL 0110
      SHELL 0120
      SHELL 0130
      SHELL 0140
      SHELL 0150
      SHELL 0160
      SHELL 0170
      SHELL 0180
      SHELL 0190
      SHELL 0200
      SHELL 0210
      SHELL 0220
      SHELL 0230
      SHELL 0240
      SHELL 0250
      SHELL 0260
      SHELL 0270
      SHELL 0280
      SHELL 0290
      SHELL 0300
      SHELL 0310
      SHELL 0320
      SHELL 0330
      SHELL 0340
      SHELL 0350
      SHELL 0360
      SHELL 0370
      SHELL 0380
      SHELL 0390
      SHELL 0400
      SHELL 0410
      SHELL 0420
      SHELL 0430
      SHELL 0440
      SHELL 0450
      SHELL 0460
      SHELL 0470
      SHELL 0480
      SHELL 0490
      SHELL 0500
      SHELL 0510
      SHELL 0520
      SHELL 0530
      SHELL 0540
      SHELL 0550
      SHELL 0560
      SHELL 0570
      SHELL 0580
      SHELL 0590

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C*****SHFL 0600
  3 CALL DSHFL1(A(M1),A(M2),A(M3),NUMDV ) SHFL 0610
    GO TO 800 SHFL 0620
C*****SHFL 0630
C-----DESIGN OF ORTHOTROPIC SHELL ELEMENTS SHFL 0640
C*****SHFL 0650
  4 CONTINUE SHFL 0660
  800 CONTINUE SHFL 0670
  RETURN SHFL 0680
C*****SHFL 0690
2001 FORMAT(IX,I7,F14.4) SHFL 0700
2002 FORMAT(//49H ANALYSIS OF PLATE/SHELL ELEMENTS ,CONSTN CODE =,I9//SHFL 0710
  1 113H ELEMENT ELEMENT LOAD /-----MEMBRANE FDSHFL 0720
  2RCFS-----//-----BENDING/TWISTING MOMENTS-----/ / SHFL 0730
  3 113H NUMBER THICKNESS COND NXX NYY SHFL 0740
  4 NXY MXX MYX MXY / ) SHFL 0750
2003 FORMAT(1H+,20X,I7,AF14.4) SHFL 0760
2004 FORMAT(/) SHFL 0770
      FMD SHFL 0780

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      SUBROUTINE PLATF1(IWT, ID, X, Y, Z, T, WT, NTC, PMAT, NUMDV, NUMNP, NIME,
1  NUMMAT, NUMTC, KODF)
      SHFL 0790
      SHFL 0800
C*****
C-----ISOTROPIC PLATF/SHELL ELEMENTS - C.A.F.F.L.I.P.P.A.'S SHELL ELEMENT
      SHFL 0810
C-----NOTE (1) PROGRAM INCLUDES TEMP. GRADIENT LOAD VECTORS AND STRESSES
      SHFL 0820
C-----      (2) PROGRAM IS WRITTEN FOR GENERAL ORTHOTROPIC MAT. PROPERTIES
      SHFL 0830
C-----THESE ARE NOT USED IN THE PRESENT PROGRAM
      SHFL 0840
C*****
      IMPLICIT REAL*8 (A-H,O-Z)
      SHFL 0850
      REAL*4 IWT, X, Y, Z, T, WT, PMAT, FRC, F4, F5, F6, RFT
      SHFL 0860
      DIMENSION IWT(NUMDV), ID(NUMNP, 6), X(NUMNP), Y(NUMNP), Z(NUMNP),
      SHFL 0870
      1 T(NUMNP), WT(NUMMAT), NTC(NUMMAT), PMAT(NUMTC, 7, NUMMAT)
      SHFL 0880
      COMMON/ JUNK /
      SHFL 0890
      1 R1(30), P2(30), ST1(6), ST2(6), TD(3, 3), XX(5), YY(5), ZZ(5),
      SHFL 0900
      2 CM(3, 2), ALFA(3), PHO, NFN, NTRI, JX(4), IF(4), PRESS, REFT, TEMP,
      SHFL 0910
      3 DTMP, FMUL(5, 4), FF(12)
      SHFL 0920
      COMMON/FM/IM(24), S(30, 30, 2), P(24, 4, 3), XM(24), ST(6, 30, 2), II(6, 4, 2),
      SHFL 0930
      1 FM1
      SHFL 0940
      COMMON/UNITS/IR, IW, IP, I1, I2, I3, IR, I9, I10, I11, I12
      SHFL 0950
C*****
C-----CONTROL INFORMATION
      SHFL 0960
C*****
      NII=2
      SHFL 0970
      NV=2
      SHFL 0980
      NW=1
      SHFL 0990
      NS=6
      SHFL 1000
      NJ=4
      SHFL 1010
      IFX=3
      SHFL 1020
      DTMP = 0.
      SHFL 1030
      WRITE(IW, 2000) NIME, NUMMAT, NUMTC, KODF
      SHFL 1040
C*****
C-----READ AND PRINT OF MATERIAL PROPERTIES
      SHFL 1050
C*****
      WRITE(IW, 2001)
      SHFL 1060
      DO 10 M=1, NUMMAT
      SHFL 1070
      READ(IR, 1000) N, NTC(N), WT(N)
      SHFL 1080
      IF(NTC(N), EQ, 0) NTC(N)=1
      SHFL 1090
      WRITE(IW, 2002) N, NTC(N), WT(N)
      SHFL 1100
      NT=NTC(N)
      SHFL 1110
      DO 11 I=1, NT
      SHFL 1120
      READ(IR, 1003) (PMAT(I, J, N), J=1, 7)
      SHFL 1130
      IF(PMAT(I, 6, N), LE, 0.) PMAT(I, 6, N)=PMAT(I, 5, N)
      SHFL 1140
      IF(PMAT(I, 7, N), LE, 0.) PMAT(I, 7, N)=PMAT(I, 5, N)*0.577
      SHFL 1150
      11 CONTINUE
      SHFL 1160
      WRITE(IW, 2009) (PMAT(I, J, N), J=1, 7)
      SHFL 1170
      IF(NT, GT, 1) WRITE(IW, 2008) ((PMAT(I, J, N), J=1, 7), I=2, NT)
      SHFL 1180
      10 CONTINUE
      SHFL 1190
C*****
C-----READ AND PRINT OF ELEMENT LOAD MULTIPLIERS
      SHFL 1200
C*****
      WRITE(IW, 2006)
      SHFL 1210
      READ(IR, 1002) (FMUL(I, J), J=1, 4), I=1, 5)
      SHFL 1220
      WRITE(IW, 2007) (J, (FMUL(I, J), I=1, 5), J=1, 4)
      SHFL 1230
C*****
C-----READ AND PRINT OF ELEMENT DATA
      SHFL 1240
C*****
      WRITE(IW, 2003)
      SHFL 1250
      M=1
      SHFL 1260
      100 READ(IR, 1001) IFL, IF, IMAT, INC, IND, PRESS, REFT, FRC, RFTA
      SHFL 1270
      IF(IFL, LT, N) GO TO 600
      SHFL 1280

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      IF (IMC.FO.O) IMC=1                                SHEFL 1390
      IF (FRC.FO.O.) FRC=1.                                SHEFL 1400
      IF (JMA1.FO.O) IMAT=1                                SHEFL 1410
      NFN=4                                                  SHEFL 1420
      ND=24                                                  SHEFL 1430
      NTR=4                                                  SHEFL 1440
      IF (IF(4).NF.O) GO TO 46                               SHEFL 1450
      NFN=3                                                  SHEFL 1460
      ND=18                                                  SHEFL 1470
      NTR=1                                                  SHEFL 1480
      IX(4)=0                                                SHEFL 1490
46  RHN=NT(IMAT)                                           SHEFL 1500
      RFI=RF1A                                              SHEFL 1510
      KK=IMC*(FI-M)                                         SHEFL 1520
      DO 45 J=1,NFN                                         SHEFL 1530
45  IX(J)=IF(J)-KK                                         SHEFL 1540
      DO 500 NFI=N,IFI                                     SHEFL 1550
      TFMP=0.                                                SHEFL 1560
      DO 40 J=1,NFN                                         SHEFL 1570
      .I=IX(J)                                              SHEFL 1580
      TFMP=TFMP+T(.I)                                       SHEFL 1590
      XX(J)=X(.I)                                           SHEFL 1600
      YY(J)=Y(.I)                                           SHEFL 1610
40  ZZ(J)=Z(.I)                                           SHEFL 1620
      TFMP=TFMP/NFN                                         SHEFL 1630
      IF (NFN.NF.4) GO TO 75                               SHEFL 1640
      XX(5)=0.25*(XX(1))+XX(2)+XX(3)+XX(4))              SHEFL 1650
      YY(5)=0.25*(YY(1)+YY(2)+YY(3)+YY(4))               SHEFL 1660
      ZZ(5)=0.25*(ZZ(1)+ZZ(2)+ZZ(3)+ZZ(4))               SHEFL 1670
C*****                                                    SHEFL 1680
C-----INTERPOLATE MATERIAL PROPERTIES FOR AVERAGE ELEMENT TEMPERATURE SHEFL 1690
C*****                                                    SHEFL 1700
75  CALL INTFRP (PMAT,FF,NUMTC,NUMMAT,7,6,NTC(IMAT),IMAT,TEMP) SHEFL 1710
      TFMP=TFMP-RFFT                                         SHEFL 1720
      ALFA(1)=FF(3)                                         SHEFL 1730
      ALFA(2)=FF(3)                                         SHEFL 1740
      ALFA(3)=0.                                             SHEFL 1750
      CON=FF(1)/(1.0-FF(2)*FF(2))                          SHEFL 1760
      CM(1,1)=CON                                           SHEFL 1770
      CM(1,2)=CON*FF(2)                                     SHEFL 1780
      CM(2,1)=CM(1,2)                                       SHEFL 1790
      CM(2,2)=CON                                           SHEFL 1800
      CM(3,3)=FF(1)*0.5/(1.0+FF(2))                       SHEFL 1810
      CM(1,3)=0.                                             SHEFL 1820
      CM(2,3)=0.                                             SHEFL 1830
      CM(3,1)=0.                                             SHEFL 1840
      CM(3,2)=0.                                             SHEFL 1850
      F4=FF(4)                                              SHEFL 1860
      F5=FF(5)                                              SHEFL 1870
      F6=FF(6)                                              SHEFL 1880
C*****                                                    SHEFL 1890
C-----FORM SHELL GLOBAL STIFFNESS MATRIX, MASS MATRIX, STRESS/DISPLACEMENTS SHEFL 1900
C-----FORM SHELL ELEMENT MATRICES                       SHEFL 1910
C*****                                                    SHEFL 1920
      ARA=C.O                                               SHEFL 1930
      CALL OTSHEI(ARA,ND)                                    SHEFL 1940
      NN=ND*ND*NI                                           SHEFL 1950
      CALL REPARAM(S,S,30,30,2,ND,NI,NI,NI)               SHEFL 1960
      NN=NS*ND*NI                                           SHEFL 1970
      CALL REPARAM(S,ST,6,30,2,NS,ND,NI,NI)               SHEFL 1980

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      NM=ND*4*NV                      SHFL1990
      CALL REARRAN(P,P,24,4,3,ND,4,NV,NM) SHFL2000
900  CONTINUE                          SHFL2010
      UWT(I*DV)=UWT(I*DV)+ARFA*RHND*FRC SHFL2020
C*****                               SHFL2030
C-----FORM LM ARRAY AND COMPUTE BANDWIDTH SHFL2040
C*****                               SHFL2050
      DO 410 I=1,NFM                      SHFL2060
        J=A*I-6                          SHFL2070
        M=IX(I)                          SHFL2080
        DO 410 K=1,6                      SHFL2090
          LM(J+K)=ID(M,K)                SHFL2100
          CALL CALBAN(NDIF,LM,S,P,ST,T1,NH,NV,MS,ND,NW,INDV,IFX,FRC) SHFL2110
          WRITE(IR) NI,F4,F5,F6,RET      SHFL2120
          WRITE(IW,2004) NF,IX,IMAT,INDV,PRESS,REF1,FRC,RETA,NDIF SHFL2130
          DO 450 MM=1,NFM                  SHFL2140
            IX(MM)=IX(MM)+INC            SHFL2150
          500 CONTINUE                    SHFL2160
            N=IFL+I                       SHFL2170
            IF(N,LF,NHMF) GO TO 100       SHFL2180
          RETURN                          SHFL2190
        600 WRITE(IW,2005) N             SHFL2200
        STOP                             SHFL2210
1000  FORMAT(2I5,F10.0)                  SHFL2220
1001  FORMAT(8I5,4F10.0)                 SHFL2230
1002  FORMAT(4F10.0)                     SHFL2240
1003  FORMAT(7F10.0)                     SHFL2250
2000  FORMAT(50H)THIN PLATE / SHELL ELEMENTS. // SHFL2260
      2  22H NUMBER OF ELEMENTS =, I5 /  SHFL2270
      3  22H NUMBER OF MATERIALS =, I5 /  SHFL2280
      4  22H NUMBER OF TEMP CARDS=, I5 /  SHFL2290
      5  22H CONSTRN CODE =, I5// )      SHFL2300
2001  FORMAT(24H MATERIAL PROPERTY TABLE, // SHFL2310
      1  124H MATERIAL NUM OF SPECIFIC TEMP YOUNGS POSHFL2320
      2  21SSONS'S COEFFT OF /-----ALLOWABLE STRESSES-----SHFL2330
      3- / / 117H NUMBER TEMP WEIGHT MODULUS SHFL2340
      4  RATIO THERM EXPN TENSION COMPRESSION SHEAR //SHFL2350
2002  FORMAT(I5,I9,F10.5)                SHFL2360
2003  FORMAT(32H THIN PLATE/SHELL ELEMENT DATA, // RH ELEMENT, 32X, SHFL2370
      1  RHMATERIAL,4X,7HDES VAR,4X,6HNORMAL,4X,9HREFERENCE,5X,7HDES VAR,SHFL2380
      5X,4HRETA,8X,4HRAND /              SHFL2390
      2  7H NUMBER,2X,6HNODE-I,2X,6HNODE-J,IX,6HNODE-K,2X,6HNODE-L, SHFL2400
      3  3X,6HNUMBER,5X,6HNUMBER,4X,8HPRESSURE,2X,11HTEMPERATURE,SHFL2410
      4  3X,8HFRAC TION,16X,5HWIDTH // ) SHFL2420
2004  FORMAT(I5,4IR,2I9,3X,4F12.4,110)  SHFL2430
2005  FORMAT(19H)CARD FOR ELEMENT (,I5,14H) IS IN ERROR., / 1X) SHFL2440
2006  FORMAT(30H ELEMENT LOAD CASE MULTIPLIERS, // 13H ELEMENT LOAD, SHFL2450
      1  4X,8HPRESSURE,5X,7HTHERMAL,13X,2HX-,13X,2HY-,13X,2HZ-, / SHFL2460
      2  13H CASE NUMBER,17X,7HEFFCIS, 3(3X,12HACCELERATION), / 1X) SHFL2470
2007  FORMAT(6X,I1,6X,2F12.3,3F15.3)    SHFL2480
2008  FORMAT(26X,F10.3,1PF14.5,0PF10.3,1PF14.5,0P3F14.2) SHFL2490
2009  FORMAT(1H+,25X,F10.3,1PF14.5,0PF10.3,1PF14.5,0P3F14.2) SHFL2500
      END                                SHFL2510

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SUBROUTINE QTSHELL(ARFA,ND)                                SHELL2520
C*****SHELL2530
C-----THIS SUBROUTINE EVALUATES
C      STIFFNESS MATRIX                                SHELL2550
C      NODAL FORCE VECTOR DUE TO THERMAL STRAINS        SHELL2560
C      MASS MATRIX                                       SHELL2570
C      STRESS/DISPLACEMENT TRANSFORMATION MATRIX       SHELL2580
C      (MEMBRANE AND BENDING)                           SHELL2590
C      NODAL FORCE VECTOR DUE TO DISTRIBUTED LATERAL LOADS SHELL2600
C      AND STRESS CORRECTION MATRIX DUE TO THERMAL STRAINS SHELL2610
C      OF A SHALLOW QUADRILATERAL SHELL ELEMENT ASSEMBLED WITH FOUR FLAT SHELL2620
C      TRIANGLES OR OF A SINGLE TRIANGULAR SHELL ELEMENT SHELL2630
C-----S1 : UNIT STIFFNESS PROPORTIONAL TO THICKNESS   SHELL2640
C      (DUE TO MEMBRANE ACTION)                          SHELL2650
C-----S2 : UNIT STIFFNESS PROPORTIONAL TO (THICKNESS)**3 SHELL2660
C      (DUE TO BENDING ACTION)                          SHELL2670
C-----P1 : UNIT NODAL FORCE VECTOR PROPORTIONAL TO THICKNESS SHELL2680
C      (DUE TO GRAVITY LOADS AND DUE TO MEAN TEMPERATURE DIFFERENCE) SHELL2690
C-----P2 : UNIT NODAL FORCE VECTOR AND IS CONSTANT    SHELL2700
C      (DUE TO NORMAL PRESSURE LOADS)                   SHELL2710
C-----P3 : UNIT NODAL FORCE VECTOR PROPORTIONAL TO (THICKNESS)**3 SHELL2720
C      (DUE TO TEMPERATURE GRADIENT ACROSS THICKNESS)   SHELL2730
C-----XM : MASS MATRIX PROPORTIONAL TO THICKNESS      SHELL2740
C-----SA1 : UNIT STRESS MATRIX PROPORTIONAL TO THICKNESS SHELL2750
C      (DUE TO MEMBRANE ACTION)                          SHELL2760
C-----SA2 : UNIT STRESS MATRIX PROPORTIONAL TO (THICKNESS)**3 SHELL2770
C      (DUE TO BENDING ACTION)                          SHELL2780
C-----T1 : UNIT STRESS CORRECTION VECTOR PROPORTIONAL TO THICKNESS SHELL2790
C      (DUE TO MEAN TEMPERATURE DIFFERENCE - MEMBRANE STRESSES) SHELL2800
C-----T2 : STRESS CORRECTION VECTOR PROPORTIONAL TO (THICKNESS)**3 SHELL2810
C      (DUE TO TEMPERATURE GRADIENT ACROSS THICKNESS)   SHELL2820
C*****SHELL2830
C      IMPLICIT REAL*8 (A-H,O-Z)                        SHELL2840
C      COMMON/JUNK/                                       SHELL2850
C      1 R1(30),R2(30),S1(6),S2(6),T1(3,3), X(5), Y(5), Z(5), SHELL2860
C      2 CM(3,2),ALFA(3),RHO ,NFN,NTRI,IX(4),IF(4),PRESS,REF1,TEMP, SHELL2870
C      3 DTEMP,FMI(5,4),FF(12)                          SHELL2880
C      COMMON/FM/LM(24),S1(30,30),S2(30,30),P1(24,4),P2(24,4),P3(24,4), SHELL2890
C      1 XM(24),SA1(6,30),SA2(6,30),T1(6,4),T2(6,4) ,EM1 SHELL2900
C      COMMON/COMPL/ A(3),B(3),ET(9),ST(9,9),T1(9),T2(9),T3(9),ARFA, SHELL2910
C      1 CT(3,9),SMI(3),RMT(3),LOC(3),ICOMP(4R1)        SHELL2920
C      DIMENSION IPERMO(4),FMM(2520)                   SHELL2930
C      EQUIVALENCE (FMM,S1)                             SHELL2940
C      DATA IPERMO /2,3,4,1/                          SHELL2950
C      WG=1.0                                             SHELL2960
C      N3=3                                               SHELL2970
C      IF(NTRI.EQ.1) GO TO 50                            SHELL2980
C      WG=0.25                                           SHELL2990
C      N3=5                                               SHELL3000
C      50 DO 150 I=1,30                                  SHELL3010
C          R1(I)=0.                                       SHELL3020
C      150 P2(I)=0.                                       SHELL3030
C          DO 151 J=1,2520                               SHELL3040
C      151 FMM(J)=0.                                       SHELL3050
C*****SHELL3060
C-----COMPUTE DIRECTION COSINE MATRIX TO OF LOCAL ELEMENT SYSTEM SHELL3070
C*****SHELL3080
C      CALL QDCOS (NTRI,X,Y,Z,70)                      SHELL3090
C*****SHELL3100
C-----THERMAL STRESS CORRECTION MATRIX                SHELL3110

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C*****SHFL 3120
      NT=NTFMP/12.
      DO 160 I=1,3
      CC=CM(I,1)*ALFA(1)+CM(I,2)*ALFA(2)+CM(I,3)*ALFA(3)
      SMT(I)=-CC*TFMP
      RMT(I)=-CC*NT
      DO 160 J=1,4
      TT(I,J)=SMT(I)*FMUL(2,J)
      160 TT(I+3,J)=RMT(I)*FMUL(2,J)
C*****SHFL 3130
C-----LOAD OVER THE NTRI TRIANGLE COMPONENTS
C*****SHFL 3140
      DO 700 NT = 1,NTRI
      NJ=NT
      N2= IPERMQ(NJ)
      LOC(1)= NJ*6-6
      LOC(2)= N2*6-6
      LOC(3)= N3*6-6
C*****SHFL 3150
C-----COMPUTE DIRECTION COSINES OF LOCAL TRIANGLE SYSTEM
C      AND THE TRIANGLE PROJECTIONS A,B ONTO IT
C-----FORM TRANSFORMATIONS BETWEEN ELEMENT AND NODAL SYSTEMS
C*****SHFL 3160
      CALL TDCOS(NJ,N2,N3,X,Y,Z,A,B,T1,T2,T3,TN,NTRI)
C*****SHFL 3170
C-----FORM MASS MATRIX AND NODAL FORCE VECTOR DUE TO NORMAL PRESSURE
C      AND GRAVITY LOADS IN GLOBAL COORDINATES
C*****SHFL 3180
      ARFA={A(3)*B(2)-A(2)*B(3)}*0.5
      ARFAA=ARFAA+ARFA
      IF(NTRI.F0.1) GO TO 345
      FAC=ARFA*PRESS*0.5
      XMM= ARFA*RHO*0.5
      DO 340 I=1,2
      K=LOC(I)
      DO 340 J=1,3
      K=K+1
      DO 341 L=1,4
      P1(K,L)= P1(K,L)+XMM*FMUL(J+2,L)
      341 P2(K,L)= P2(K,L)+ FAC*FMUL(1,L)*T3(J)
      340 XM(K)=XM(K)+XMM
      GO TO 350
      345 FAC= ARFA*PRESS/3.
      XMM=ARFA*RHO/3.0
      DO 360 J=1,3
      K=LOC(J)
      DO 360 J=1,3
      K=K+1
      DO 361 L=1,4
      P1(K,L)= P1(K,L)+XMM*FMUL(J+2,L)
      361 P2(K,L)= P2(K,L)+ FAC*FMUL(1,L)*T3(J)
      360 XM(K)=XM(K)+XMM
      350 CONTINUE
C*****SHFL 3190
C-----MEMBRANE CONTRIBUTION
C*****SHFL 3200
      CALL SLST (CM)
C*****SHFL 3210
C-----LOCAL TO GLOBAL COORDINATE TRANSFORMATION OF TRIANGLE ELEMENT
C      MEMBRANE STIFFNESS
C*****SHFL 3220

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C*****SHFL 3720
  LT=0 SHFL 3730
  DO 400 J,I=1,3 SHFL 3740
    J = J,I + J,I SHFL 3750
    M = LNC(J,I) SHFL 3760
    DO 400 L=1,3 SHFL 3770
      M = M + 1 SHFL 3780
      LT=LT+1 SHFL 3790
      C1=T1(LT) SHFL 3800
      C2=T2(LT) SHFL 3810
      KT=0 SHFL 3820
      DO 390 IJ=1,JJ SHFL 3830
        I = IJ + IJ SHFL 3840
        KK=3 SHFL 3850
        IF (IJ.FO,JJ) KK = L SHFL 3860
        H1 = S1(I-1,J-1)*C1 + S1(I-1,J)*C2 SHFL 3870
        H2 = S1(I,J-1)*C1 + S1(I,J)*C2 SHFL 3880
        N = LNC(IJ) SHFL 3890
        DO 390 K=1,KK SHFL 3900
          N = N + 1 SHFL 3910
          KT=KT+1 SHFL 3920
          S0= S1(N,M)+11(KT)*H1+12(KT)*H2 SHFL 3930
          S1(N,M)=S0 SHFL 3940
        390 S1(M,M)=S0 SHFL 3950
      400 CONTINUE SHFL 3960
C*****SHFL 3970
C-----LOCAL TO GLOBAL COORDINATE TRANSFORMATION OF STRESS MATRIX AND SHFL 3980
C THERMAL LOAD VECTOR SHFL 3990
C*****SHFL 4000
  DO 410 J,I=1,3 SHFL 4010
    M=LNC(J,I) SHFL 4020
    J=J,I+J,I SHFL 4030
    DO 410 L=1,3 SHFL 4040
      M = M+1 SHFL 4050
      R1(M)=R1(M)+T1(L)*FT(J-1)+T2(L)*FT(J) SHFL 4060
      DO 410 K=1,3 SHFL 4070
        410 SA1(K,M)=SA1(K,M)+(CT(K,J-1)*T1(L) +CT(K,J)*T2(L))*WG SHFL 4080
      SHFL 4090
    SHFL 4100
C-----PLATE BENDING CONTRIBUTION SHFL 4110
C*****SHFL 4120
  CALL SLCTT(CM,NTRI) SHFL 4130
C*****SHFL 4140
C-----LOCAL TO GLOBAL TRANSFORMATION OF TRIANGLE ELEMENT SHFL 4150
C BENDING STIFFNESS SHFL 4160
C*****SHFL 4170
  DO 500 JJ = 1,3 SHFL 4180
    JT = 3*JJ-3 SHFL 4190
    J = JJ + 1 SHFL 4200
    DO 480 II = 1,JJ SHFL 4210
      IT = 3*II-3 SHFL 4220
      I = II + 1 SHFL 4230
      KK=6 SHFL 4240
      DO 480 L=1,6 SHFL 4250
        IF (II.FO,JJ) KK = L SHFL 4260
        M = LNC(JJ) + 1 SHFL 4270
        L3 = L - 3 SHFL 4280
        IF (L3.GT,0) GO TO 460 SHFL 4290
        C3=T3(JT+L) SHFL 4300
        H1 = S1(I,J)*C3 SHFL 4310
        H2 = S1(I+1,J)*C3

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      H3 = ST(I+2,J)*C3
      GO TO 470
460 C1=T1(I,J+L3)
      C2=T2(I,J+L3)
      H1 = ST(I,J+1)*C1 + ST(I,J+2)*C2
      H2 = ST(I+1,J+1)*C1 + ST(I+1,J+2)*C2
      H3 = ST(I+2,J+1)*C1 + ST(I+2,J+2)*C2
470 N = I,NC(I,I)
      DO 480 K = 1,KK
      N = N + 1
      K3 = K - 3
      K1 = I1 + K
      K2 = I1 + K3
      IF (K3,LF,0) SO = S2(N,M) + T3(K1)*H1
      IF (K3,GT,0) SO = S2(N,M) + T1(K2)*H2 + T2(K2)*H3
      S2(N,M) = SO
480 S2(M,N) = SO
500 CONTINUE
C*****SHFL 4500
C-----LOCAL TO GLOBAL TRANSFORMATION OF MOMENT RESULTANT MATRIX AND
C THERMAL LOAD VECTOR
C*****SHFL 4530
      DO 680 J,1,3
      M=LOC(I,J)
      J=(J,1-1)*3+1
      DO 686 I,1,3
      M = M+1
      R2(M)=R2(M)+FT(I)*T3(I)
      DO 686 K=1,3
686 SA2(K+2,M)=SA2(K+3,M)+CT(K,J)*T3(I)*WG
      DO 680 I,1,3
      M=M+1
      R2(M)=R2(M)+FT(I+1)*T1(I)+FT(J+2)*T2(I)
      DO 680 K=1,3
680 SA2(K+3,M)=SA2(K+3,M)+(CT(K,J+1)*T1(I) +CT(K,J+2)*T2(I))*WG
700 CONTINUE
      IF(MTR1,F0,1) GO TO 900
C*****SHFL 4690
C-----CHECK FOR POSSIBLE INTERNAL STIFFNESS SINGULARITY (FLAT
C OR NEARLY FLAT QUADRILATERAL) AND TRANSFORM STIFFNESS AT 5TH NODE
C TO GLOBAL COORDINATES
C*****SHFL 4730
      IF(S1(27,27),GT,(S1(25,25)+S1(26,26))*1.0E-07) GO TO 690
      DO 691 I=1,27
      S1(I,27)=0.0
691 S1(27,I)=0.0
690 DO 510 I=1,27
      DO 511 J=1,3
511 FT(I)=S1(I,25)*T0(1,J)+S1(I,26)*T0(2,J)+S1(I,27)*T0(3,J)
      DO 510 J=1,3
510 S1(I,J+24)=FT(I)
      DO 520 J,25,27
      DO 521 I=1,3
521 FT(I)=T0(1,I)*S1(25,J)+T0(2,I)*S1(26,J)+T0(3,I)*S1(27,J)
      DO 520 I=1,3
520 S1(24+I,J)=FT(I)
      DO 530 I=1,24
      DO 530 J=25,27
530 S1(I,J)=S1(I,J)
      CALL TRANS(S2,T0,FT,FT(4),FT(7))

```



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C*****SHEL 4920
C-----CONDENSATION OF INTERNAL DEGREES OF FREEDOM      SHEL 4930
C*****SHEL 4940
      CALL CONDEN (1,3,S1,R1,SA1,ST1)      SHEL 4950
      CALL CONDEN (4,6,S2,R2,SA2,ST2)      SHEL 4960
      DO 851 J=1,6                          SHEL 4970
      DO 851 J=1,4                          SHEL 4980
      TT1(I,J)=TT1(I,J)+ST1(I)*FMIH(2,J)   SHEL 4990
851  TT2(I,J)=TT2(I,J)+ST2(I)*FMIH(2,J)   SHEL 5000
900  DO 850 J=1,NN                          SHEL 5010
      DO 850 J=1,4                          SHEL 5020
      P1(I,J)=P1(I,J)+R1(I)*FMIH(2,J)     SHEL 5030
850  P3(I,J)=R2(I)*FMIH(2,J)              SHEL 5040
      RETURN                                SHEL 5050
      END                                  SHEL 5060

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      SUBROUTINE CONDEN(NN,MM,S,R,SA,ST)      SHEL 5070
C*****SHEL 5080
C-----CONDENSATION OF INTERNAL DEGREES OF FREEDOM      SHEL 5090
C*****SHEL 5100
      IMPL(I,IT) REAL*8 (A-H,O-Z)           SHEL 5110
      DIMENSION S(30,30),R(30),SA(6,30),ST(6) SHEL 5120
      DO 850 I=1,6                          SHEL 5130
850  ST(I)=0.                                SHEL 5140
      DO 800 J=1,6                          SHEL 5150
      L=30-J                                SHEL 5160
      M=L+1                                  SHEL 5170
      PIV=S(M,M)                            SHEL 5180
      IF(PIV.LE.0) GO TO 800                 SHEL 5190
      RI=R(M)/PIV                           SHEL 5200
      DO 820 K=J+L                          SHEL 5210
      R(K)=R(K)-S(K,M)*RI                   SHEL 5220
      SS=S(M,K)/PIV                         SHEL 5230
      DO 830 I=1,K                          SHEL 5240
830  S(K,I)=S(K,I)-S(M,I)*SS               SHEL 5250
      DO 820 I=NN,MM                        SHEL 5260
820  SA(I,K)=SA(I,K)-SA(I,M)*SS            SHEL 5270
      DO 810 J=NN,MM                        SHEL 5280
810  ST(I)=ST(I)-SA(I,M)*RI                SHEL 5290
800  CONTINUE                               SHEL 5300
      DO 900 I=2,24                         SHEL 5310
      II=I-1                                SHEL 5320
      DO 900 J=1,II                         SHEL 5330
900  S(J,I)=S(I,J)                          SHEL 5340
      RETURN                                SHEL 5350
      END                                  SHEL 5360

```

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      SHRRDUTINF TRANS(S,TD,C1,C2,C3)                                SHFL 5370
C*****SHFL 5380
C-----TRANSFORM THE STIFFNESS MATRIX AT 5TH NODE TO GLOBAL COORDINATES SHFL 5390
C*****SHFL 5400
      IMPLICIT REAL*8 (A-H,O-Z)                                SHFL 5410
      DIMENSION S(30,30),TD(3,3),C1(3),C2(3),C3(3)            SHFL 5420
      IF(S (25,25).GT. S (27,27)*1.0E-07) GO TO 692           SHFL 5430
      DO 693 J=1,30                                             SHFL 5440
        S (I,25)=0.0                                           SHFL 5450
693   S (25,J)=0.0                                             SHFL 5460
692   IF(S (26,26).GT.S (27,27)*1.0E-07) GO TO 694           SHFL 5470
      DO 695 J=1,30                                             SHFL 5480
        S (I,26)=0.0                                           SHFL 5490
695   S (26,J)=0.0                                             SHFL 5500
694   IF(S (30,30).GT.(S (29,29)+S (28,28))*1.0E-08) GO TO 730 SHFL 5510
      DO 710 J=1,30                                             SHFL 5520
        S (I,30)=0.0                                           SHFL 5530
710   S (30,J)=0.0                                             SHFL 5540
730   DO 10 I1=1,30                                             SHFL 5550
        DO 11 J=1,3                                             SHFL 5560
          C1(I)=S (I,25)*TD(1,I)+S (I,26)*TD(2,I)+S (I,27)*TD(3,I) SHFL 5570
          C2(I)=S (I,28)*TD(1,I)+S (I,29)*TD(2,I)+S (I,30)*TD(3,I) SHFL 5580
          DO 10 J=1,3                                             SHFL 5590
            S (I,J+24)=C1(I,J)                                SHFL 5600
10     S (I,J+27)=C2(I,J)                                       SHFL 5610
          DO 20 J1=25,27                                         SHFL 5620
            J3=J1+3                                             SHFL 5630
            DO 21 J=1,3                                          SHFL 5640
              T1=TD(1,I)                                         SHFL 5650
              T2=TD(2,I)                                         SHFL 5660
              T3=TD(3,I)                                         SHFL 5670
              C1(I)=I1*S (25,J1)+I2*S (26,J1)+I3*S (27,J1)     SHFL 5680
              C2(I)=T1*S (25,J3)+I2*S (26,J3)+I3*S (27,J3)     SHFL 5690
21     C3(I)=I1*S (28,J3)+I2*S (29,J3)+I3*S (30,J3)           SHFL 5700
            DO 20 J=1,3                                          SHFL 5710
              S (I+24,J1)=C1(I)                                SHFL 5720
              S (I+24,J3)=C2(I)                                SHFL 5730
              S (J3,I+24)=C3(I)                                SHFL 5740
20     S (I+27,J3)=C3(I)                                       SHFL 5750
            DO 30 J=1,24                                         SHFL 5760
            DO 30 J1=25,30                                       SHFL 5770
30     S (J,I)=S (I,J)                                         SHFL 5780
      RETURN                                                    SHFL 5790
      ENN                                                       SHFL 5800

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SUBROUTINE SLST (C )                                SHFL 5810
C*****                                              SHFL 5820
C-----THIS SUBROUTINE FORMS THE STIFFNESS MATRIX ,THERMAL LOAD VECTOR, SHFL 5830
C      AND STRESS MATRIX OF A CONSTANT STRAIN TRIANGLE WITH SHFL 5840
C      LINEAR ELASTIC ANISOTROPIC PROPERTIES SHFL 5850
C*****                                              SHFL 5860
      IMPLCIT REAL*8 ( A-H,O-Z) SHFL 5870
      COMMON/COMMON/A(3),R(3),F(9),S(9),T(9),T2(9),T3(9),AREA, SHFL 5880
      1 CT(3,9),SMT(3),BMT(3),LOC(3),ICOMP(4*1) SHFL 5890
      DIMENSION C(3,3) SHFL 5900
      FAC=0.25/AREA SHFL 5910
      FAC1=0.5/AREA SHFL 5920
      C11 = C(1,1)*FAC SHFL 5930
      C22 = C(2,2)*FAC SHFL 5940
      C33 = C(3,3)*FAC SHFL 5950
      C12 = C(1,2)*FAC SHFL 5960
      C13 = C(1,3)*FAC SHFL 5970
      C23 = C(2,3)*FAC SHFL 5980
      DO 200 J=1,3 SHFL 5990
        L=J+J SHFL 6000
C*****                                              SHFL 6010
C-----THERMAL LOAD VECTOR SHFL 6020
C*****                                              SHFL 6030
      FT(L-1)=(-R(J)*SMT(1)-A(J)*SMT(2))*0.5 SHFL 6040
      FT(L)=(-A(J)*SMT(2)-R(J)*SMT(3))*0.5 SHFL 6050
C*****                                              SHFL 6060
C-----STRESS DISPLACEMENT TRANSFORMATION MATRIX SHFL 6070
C*****                                              SHFL 6080
      DO 300 I=1,3 SHFL 6090
        CT(I,L-1)= (C(I,1)*R(J)+C(I,3)*A(J))*FAC1 SHFL 6100
        300 CT(I,L)= (C(I,2)*A(J)+C(I,3)*R(J))*FAC1 SHFL 6110
C*****                                              SHFL 6120
C-----STIFFNESS MATRIX IN TRIANGLE LOCAL COORDINATES SHFL 6130
C*****                                              SHFL 6140
      DO 200 I=1,J SHFL 6150
        K=I+I SHFL 6160
        AA=A(I)*A(J) SHFL 6170
        AB=A(I)*R(J) SHFL 6180
        RB=R(J)*R(J) SHFL 6190
        RA=R(I)*A(J) SHFL 6200
        ARA=AR+RA SHFL 6210
        ST(K-1,L-1)=C11*RB+C13*ARA+C33*AA SHFL 6220
        ST(K-1,L)=C12*RA+C13*RB+C23*AA+C33*AR SHFL 6230
        ST(K,L-1)= C12*AR+C13*RB+C23*AA+C33*RA SHFL 6240
      200 ST(K,L)= C22*AA+C23*ARA+C33*RB SHFL 6250
      DO 400 I=3,6 SHFL 6260
      DO 400 J=1,I SHFL 6270
      400 ST(I,J)=ST(J,I) SHFL 6280
      RETURN SHFL 6290
      END SHFL 6300

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SUBROUTINE SLCT(CM,NTRI)
C*****
C-----THIS SUBROUTINE FORMS THE PLATE BENDING STIFFNESS AND THE
C CONSTITUENT LOAD VECTOR DUE TO THERMAL LOADS AND STRESS
C TRANSFORMATION MATRIX OF A LINEAR CURVATURE COMPATIBLE TRIANGLE
C WITH 6 NODAL POINTS. MID SIDE NODES ARE ELIMINATED BY ASSUMING
C NORMAL SLOPE AT THE MID SIDE NODE TO BE AVERAGE OF THE ONES AT TWO
C ADJACENT CORNERS.
C*****
IMPLICIT REAL*8 (A-H,O-Z)
COMMON/COMMONP/Δ(3),R(3),FT(9),ST(9,9),T1(9),T2(9),T3(9),ARFA,
1 CT(3,9),SM1(3),SM2(3),LOC(3),JUN,II(3),IX(3),IY(3),Q(3,6),P(21,9),
2 G(21),HT(3)
DIMENSION IPERM(3),CM(3,3)
DATA IPERM/2,3,1/
FAC1=ARFA/432.
FAC2=1./12.
DO 150 I=1,3
J = IPERM(I)
K = IPERM(J)
X= A(I)**2+R(I)**2
II(I)= -(A(I)*A(J)+R(I)*R(J))/X
X=DSORT(X)
Y=4.*ARFA/X
HT(I) =2.*Y
TX(I)= Y*A(J)/X
IY(I)=-Y*R(I)/X
A1=0.5*A(I)/ARFA
A2=0.5*A(J)/ARFA
R1=0.5*R(I)/ARFA
R2=0.5*R(J)/ARFA
Q(1,I) = R1*R1
Q(2,I) = A1*A1
Q(3,I) = 2.*A1*R1
Q(1,I+3) = 2.*R1*R2
Q(2,I+3) = 2.*A1*A2
Q(3,I+3) = 2.*(A1*R2+A2*R1)
150 CONTINUE
C*****
C-----CURVATURE DISPLACEMENT RELATION FOR THREE TRIANGULAR REGIONS
C*****
DO 200 I=1,3
J=IPERM(I)
K=IPERM(J)
II=3*I
J1=3*J
KK=3*K
A1= A(I)
A2= A(J)
A3= A(K)
R1=R(I)
R2=R(J)
R3=R(K)
II=II(I)
I2=II(J)
I3=II(K)
W1=1.-II1
W2=1.-I2
W3=1.-I3
R1D=R1+R1

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SHFL 6310
SHFL 6320
SHFL 6330
SHFL 6340
SHFL 6350
SHFL 6360
SHFL 6370
SHFL 6380
SHFL 6390
SHFL 6400
SHFL 6410
SHFL 6420
SHFL 6430
SHFL 6440
SHFL 6450
SHFL 6460
SHFL 6470
SHFL 6480
SHFL 6490
SHFL 6500
SHFL 6510
SHFL 6520
SHFL 6530
SHFL 6540
SHFL 6550
SHFL 6560
SHFL 6570
SHFL 6580
SHFL 6590
SHFL 6600
SHFL 6610
SHFL 6620
SHFL 6630
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SHFL 6650
SHFL 6660
SHFL 6670
SHFL 6680
SHFL 6690
SHFL 6700
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SHFL 6790
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SHFL 6830
SHFL 6840
SHFL 6850
SHFL 6860
SHFL 6870
SHFL 6880
SHFL 6890
SHFL 6900

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R2D=R2+R2
R2D=R2+R2
A1D=A1+A1
A2D=A2+A2
A3D=A3+A3
C21 = R1-R3*U12 + TX(K)
C31 = A1-A3*U12 + TY(K)
C51 = R3*W3-R2 + TX(K)
C61 = A3*W3-A2 + TY(K)
C81 = R3-R2D-R2*U12 + TX(J)
C91 = A3-A2D-A2*U12 + TY(J)
C22=-R1D+R2*W2+R3*U12 + TX(J)-TX(K)
C32=-A1D+A2*W2+A3*U12+TY(J)-TY(K)
C52 = R2D-R3*W3-R1*U11 + TX(I)-TX(K)
C62 = A2D-A3*W3-A1*U11 + TY(I)-TY(K)
C82 = R1D-R3+R1*W1 + TX(I)
C92 = A1D-A3+A1*W1 + TY(I)
DO 200 N=1,3
L= 6*( I-1)+N
O11=O(N,I)
O22=O(N,J)
O33=O(N,K)
O12=O(N,I+3)
O23=O(N,J+3)
O31=O(N,K+3)
O2333=O23-O33
O3133=O31-O33
P(I, ,I1-2) = 6.*(-O11+W2*O33+U2*O2333)
P(I, ,I1-1) = C21*O23+C22*O33-R3D*O12+R2D*O31
P(I, ,I1) = C31*O23+C32*O33-A3D*O12+A2D*O31
P(I, ,J1-2) = 6.*(O22+W3*O2333)
P(I, ,J1-1) = C51*O2333+R3D*O22
P(I, ,J1) = C61*O2333+A3D*O22
P(I, ,KK-2) = 6.*(1.+U2)*O33
P(I, ,KK-1) = C81*O33
P(I, ,KK) = C91*O33
P(I+3, ,I1-2) = 6.*(O11+U3*O3133)
P(I+3, ,I1-1) = C21*O3133-R3D*O11
P(I+3, ,I1) = C31*O3133-A3D*O11
P(I+3, ,J1-2) = 6.*(-O22+U1)*O33+W3*O3133
P(I+3, ,J1-1) = C51*O31+C52*O33+R3D*O12-R1D*O23
P(I+3, ,J1) = C61*O31+C62*O33+A3D*O12-A1D*O23
P(I+3, ,KK-2) = 6.*(1.+W1)*O33
P(I+3, ,KK-1) = C82*O33
P(I+3, ,KK) = C92*O33
P(N+1R, I1-2) = 2.*(O11+U3*O12+W2*O31)
P(N+1R, KK-1) = (R1D-R2D)*O33+C82*O23+C81*O31)/3.
P(N+1R, KK) = ((A1D-A2D)*O33+C92*O23+C91*O31)/3.
200 CONTINUE
DO 400 J=1,9
FT(J)=0.
DO 340 L=1,3
IT=L
KK=L+1P
P3=P(KK,J)
G(KK)=0.
DO 340 N=1,3
JL=I1+?
SUM=P(I1,J)+P(J,J)+P3
G(I1)=SUM+P(I1,J)

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SHFL 6910
SHFL 6920
SHFL 6930
SHFL 6940
SHFL 6950
SHFL 6960
SHFL 6970
SHFL 6980
SHFL 6990
SHFL 7000
SHFL 7010
SHFL 7020
SHFL 7030
SHFL 7040
SHFL 7050
SHFL 7060
SHFL 7070
SHFL 7080
SHFL 7090
SHFL 7100
SHFL 7110
SHFL 7120
SHFL 7130
SHFL 7140
SHFL 7150
SHFL 7160
SHFL 7170
SHFL 7180
SHFL 7190
SHFL 7200
SHFL 7210
SHFL 7220
SHFL 7230
SHFL 7240
SHFL 7250
SHFL 7260
SHFL 7270
SHFL 7280
SHFL 7290
SHFL 7300
SHFL 7310
SHFL 7320
SHFL 7330
SHFL 7340
SHFL 7350
SHFL 7360
SHFL 7370
SHFL 7380
SHFL 7390
SHFL 7400
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SHFL 7430
SHFL 7440
SHFL 7450
SHFL 7460
SHFL 7470
SHFL 7480
SHFL 7490
SHFL 7500

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      G(I,J)=SIIM+P(I,I,J)                                SHFL 7510
      G(KK)=G(KK)+SIIM+P3                                  SHFL 7520
      FT(J)=FT(J)-SIIM*BMT(L)*ARFA/9.0                    SHFL 7530
      II=J+6                                                SHFL 7540
360  CONTINUE                                               SHFL 7550
      DO 360 N=1,19,3                                       SHFL 7560
      G1=G(N)                                                SHFL 7570
      G2=G(N+1)                                              SHFL 7580
      G3=G(N+2)                                              SHFL 7590
      G(N)=CM(1,1)*G1+CM(1,2)*G2+CM(1,3)*G3              SHFL 7600
      G(N+1)=CM(1,2)*G1+CM(2,2)*G2+CM(2,3)*G3            SHFL 7610
360  G(N+2)=CM(1,3)*G1+CM(2,3)*G2+CM(3,3)*G3            SHFL 7620
      DO 390 I=1,J                                          SHFL 7630
      X=0.0                                                  SHFL 7640
      DO 380 N=1,21                                          SHFL 7650
380  X=X+G(N)*P(N,I)                                       SHFL 7660
      X=X*FAC1                                              SHFL 7670
      ST(I,I)=X                                              SHFL 7680
390  ST(I,J)=X                                              SHFL 7690
400  CONTINUE                                               SHFL 7700
C*****SHFL 7710
C-----CURVATURE DISPLACEMENT - DISPLACEMENT RELATION AT ELEMENT CENTRE SHFL 7720
C*****SHFL 7730
      IF(NTRJ.FO.1) GO TO 551                               SHFL 7740
      DO 550 J=1,9                                           SHFL 7750
      P(19,J)=(P(10,J)+P(13,J))*0.5                         SHFL 7760
      P(20,J)=(P(11,J)+P(14,J))*0.5                         SHFL 7770
550  P(21,J)=(P(12,J)+P(15,J))*0.5                         SHFL 7780
C*****SHFL 7790
C-----MOMENT - DISPLACEMENT RELATION SHFL 7800
C*****SHFL 7810
551  DO 600 I=1,3                                           SHFL 7820
      DO 600 J=1,9                                           SHFL 7830
      SIIM=0.0                                               SHFL 7840
      DO 610 K=1,3                                           SHFL 7850
610  SIIM=SIIM+CM(I,K)*P(K+18,J)                           SHFL 7860
600  CT(I,J)=-FAC2*SIIM                                    SHFL 7870
      RETURN                                                SHFL 7880
      END                                                    SHFL 7890

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SUBROUTINE DDCOS(N1,N2,N3,X,Y,Z,A,B,T1,T2,T3,T,NTRI)          SHFI 7900
C*****SHFI 7910
C-----THIS SUBROUTINE COMPUTES THE DIRECTION COSINES OF THE LOCAL SHFI 7920
C SYSTEM AND THE PROJECTED DIMENSIONS OF A SUBTRIANGLE COMPONENT SHFI 7930
C*****SHFI 7940
IMPLICIT REAL*8 (A-H,O-Z)          SHFI 7950
DIMENSION X(5),Y(5),Z(5),A(3),B(3),T1(9),T2(9),T3(9),T(9)          SHFI 7960
A1 = X(N1)-X(N3)          SHFI 7970
A2 = Y(N1)-Y(N3)          SHFI 7980
A3 = Z(N1)-Z(N3)          SHFI 7990
B1 = X(N2)-X(N3)          SHFI 8000
B2 = Y(N2)-Y(N3)          SHFI 8010
B3 = Z(N2)-Z(N3)          SHFI 8020
IF(NTRI.FO.4) GO TO 300          SHFI 8030
DO 350 I=1,3          SHFI 8040
T1(I)=T(I*3-2)          SHFI 8050
T1(I+3)=T1(I)          SHFI 8060
T1(I+6)=T1(I)          SHFI 8070
T2(I)=T(I*3-1)          SHFI 8080
T2(I+3)=T2(I)          SHFI 8090
T2(I+6)=T2(I)          SHFI 8100
T3(I)=T(I*3)          SHFI 8110
T3(I+3)=T3(I)          SHFI 8120
350 T3(I+6)=T3(I)          SHFI 8130
GO TO 400          SHFI 8140
300 T31 = A1*B2-B2*B1          SHFI 8150
T32 = A1*B3-B3*B1          SHFI 8160
T33 = A1*B2-B2*B1          SHFI 8170
S = DSORT (T31**2+T32**2+T33**2)          SHFI 8180
T31 = T31/S          SHFI 8190
T32 = T32/S          SHFI 8200
T33 = T33/S          SHFI 8210
T11= T33*T(5)-T32*T(8)          SHFI 8220
T12= T31*T(8)-T33*T(2)          SHFI 8230
T13= T22*T(2)-T31*T(5)          SHFI 8240
S = DSORT(T11**2+T12**2+T13**2)          SHFI 8250
T11=T11/S          SHFI 8260
T12=T12/S          SHFI 8270
T13=T13/S          SHFI 8280
T21= T13*T32-T12*T33          SHFI 8290
T22= T11*T33-T12*T31          SHFI 8300
T23= T12*T31-T11*T32          SHFI 8310
T1(1)=T11          SHFI 8320
T1(2)=T12          SHFI 8330
T1(3)=T13          SHFI 8340
T2(1)=T21          SHFI 8350
T2(2)=T22          SHFI 8360
T2(3)=T23          SHFI 8370
T3(1)=T31          SHFI 8380
T3(2)=T32          SHFI 8390
T3(3)=T33          SHFI 8400
DO 100 I=1,3          SHFI 8410
J=I+3          SHFI 8420
K=I+6          SHFI 8430
T1(J)=T1(I)          SHFI 8440
T2(J)=T2(I)          SHFI 8450
T3(J)=T3(I)          SHFI 8460
C1=T(I)          SHFI 8470
CJ=T(J)          SHFI 8480
CK=T(K)          SHFI 8490

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      T1(K)=T11*C1+T12*CJ+T13*CK                      SHFI 8500
      T2(K)=T21*C1+T22*CJ+T23*CK                      SHFI 8510
      T3(K)=T31*C1+T32*CJ+T33*CK                      SHFI 8520
100  A(1)=-T1(1)*A2-T1(2)*R2-T1(3)*C2                SHFI 8530
400  A(2)=-T1(1)*A1+T1(2)*R1+T1(3)*C1                SHFI 8540
      A(3)=-A(1)-A(2)                                  SHFI 8550
      R(1)=-T2(1)*A2+T2(2)*R2+T2(3)*C2                SHFI 8560
      R(2)=-T2(1)*A1-T2(2)*R1-T2(3)*C1                SHFI 8570
      R(3)=-R(1)-R(2)                                  SHFI 8580
      RETURN                                             SHFI 8590
      FND                                               SHFI 8600

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      SUBROUTINE DDCOS (N,X,Y,Z,1)                      SHFI 8610
C*****SHFI 8620
C-----THIS SUBROUTINE COMPUTES THE DIRECTION COSINES OF THE LOCAL SHFI 8630
C      ELEMENT SYSTEM OF A QUADRILATERAL(N=4) OR SINGLE TRIANGLE(N=1) SHFI 8640
C*****SHFI 8650
      IMPLICIT REAL*8 (A-H,O-Z)                        SHFI 8660
      DIMENSION X(5),Y(5),Z(5),T(9)                  SHFI 8670
      X1 = X(2)+X(3)-X(N)-X(1)                        SHFI 8680
      Y1 = Y(2)+Y(3)-Y(N)-Y(1)                        SHFI 8690
      Z1 = Z(2)+Z(3)-Z(N)-Z(1)                        SHFI 8700
      X2 = X(3)+X(N)-X(1)-X(2)                        SHFI 8710
      Y2 = Y(3)+Y(N)-Y(1)-Y(2)                        SHFI 8720
      Z2 = Z(3)+Z(N)-Z(1)-Z(2)                        SHFI 8730
      S1 = X1**2+Y1**2+Z1**2                            SHFI 8740
      C = (X1*X2+Y1*Y2+Z1*Z2)/S1                      SHFI 8750
      X2 = X2-C*X1                                      SHFI 8760
      Y2 = Y2-C*Y1                                      SHFI 8770
      Z2 = Z2-C*Z1                                      SHFI 8780
      S1=DSORT(S1)                                      SHFI 8790
      S2=DSORT(X2*X2+Y2*Y2+Z2*Z2)                      SHFI 8800
      X1=X1/S1                                          SHFI 8810
      Y1=Y1/S1                                          SHFI 8820
      Z1=Z1/S1                                          SHFI 8830
      X2=X2/S2                                          SHFI 8840
      Y2=Y2/S2                                          SHFI 8850
      Z2=Z2/S2                                          SHFI 8860
      T(1) = X1                                          SHFI 8870
      T(2) = X2                                          SHFI 8880
      T(3) = Y1*Z2-Y2*Z1                                SHFI 8890
      T(4) = Y1                                          SHFI 8900
      T(5) = Y2                                          SHFI 8910
      T(6) = Z1*X2-Z2*X1                                SHFI 8920
      T(7) = Z1                                          SHFI 8930
      T(8) = Z2                                          SHFI 8940
      T(9) = X1*Y2-X2*Y1                                SHFI 8950
      RETURN                                             SHFI 8960
      FND                                               SHFI 8970

```



```

      SHARP(UTIME) DSHELL(1) (AOLD,ANFW,LOAD,NUMDV) ) SHFL 8980
C-----DESIGN OF PLATE/SHELL ELEMENTS FOR STRESS CONSTRAINTS SHFL 8990
C-----DESIGN OF PLATE/SHELL ELEMENTS FOR STRESS CONSTRAINTS SHFL 9000
      DIMENSION AOLD(NUMDV),ANFW(NUMDV),LOAD(NUMDV) SHFL 9010
      COMMON/SHK/JUN(16),LT,LH,L,SG(20),FX,FY,FXY,SMX,SMY,SMXY,SIG, SHFL 9020
      1 IDVAR,IFX,IRC,H,XINERT,TEN,COMP,SHFAR,RETA,HP(2),JUN(243) SHFL 9030
      FXY=FX/(SHFAR*H) SHFL 9040
      SMXY=6.0*SMXY/(SHFAR*H*H) SHFL 9050
      CC=-1.0 SHFL 9060
      DO 200 I=1,2 SHFL 9070
        IF(I.EQ.2) CC=1.0 SHFL 9080
        C1=FX/H+CC*6.0*SMX/(H*H) SHFL 9090
        C2=FY/H+CC*6.0*SMY/(H*H) SHFL 9100
        AX=TFN SHFL 9110
        AY=TFN SHFL 9120
        IF(C1.LT.0.) AX=COMP SHFL 9130
        IF(C2.LT.0.) AY=COMP SHFL 9140
        FX1=FX/(AX*H) SHFL 9150
        FY1=FY/(AY*H) SHFL 9160
        SMX1=6.0*SMX/(AX*H*H) SHFL 9170
        SMY1=6.0*SMY/(AY*H*H) SHFL 9180
        CXX= FX1*FX1+FY1*FY1+FXY1*FXY1-FX1*FY1 SHFL 9190
        CY=2.0*(FX1*SMX1+FY1*SMY1+FXY1*SMXY1)- FX1*SMY1-FY1*SMX1 SHFL 9200
        CX=CX*CC SHFL 9210
        C= SMX1*SMX1+SMY1*SMY1+SMXY1*SMXY1-SMX1*SMY1 SHFL 9220
        HP(I)=H SHFL 9230
        DO 100 J=1,10 SHFL 9240
          HHH=(CXX+CX*H/HP(I))*0.5 SHFL 9250
          HHH=HHH+SQRT(HHH*HHH+C) SHFL 9260
          HHH=SQRT(HHH)*H SHFL 9270
          IF(ABS(HHH-HP(I)).LT.0.001) GO TO 200 SHFL 9280
100 HP(I)=HHH SHFL 9290
200 HP(I)=HHH SHFL 9300
      HH=HP(1) SHFL 9310
      IF(HH.LT.HP(2)) HH=HP(2) SHFL 9320
      HH=HH/IRC SHFL 9330
      IF(HH.LF.ANFW(IDVAR)) GO TO 400 SHFL 9340
      ANFW(IDVAR) =HH SHFL 9350
      LOAD(IDVAR) =1 SHFL 9360
400 RETURN SHFL 9370
      FND SHFL 9380

```

```

      SUBROUTINE ROUNDO (A,MTOT)
      *****
C-----BOUNDARY ELEMENTS
      *****
      DIMENSION A(MTOT)
      COMMON /ELPAR/ NPAR(14),NIMNP,MRAND,MFLYP,N1,N2,N3,N4,N5,M111,NFOROUN0050
      ,NIMFL,NIMDV,M1,M2,M3,LL,LR,NFOR,MLOCK
      COMMON/JOINK/JOIN(16),LT,LH,L,SG(27),J111(254)
      COMMON/UNIT/IR,IW,IP,I1,I2,I3,IR,I9,I10,I11,I12
      NIME=NPAP(2)
      IF (NPAR(1),EQ,0) GO TO 500
      CALL CLAMP(A(N1),A(N2),A(N3),A(N4),NIME,NIMNP)
      RETURN
500 WRITE(IW,2002)
      DO 800 MM=1,NIME
      CALL STRSC (A(M)),A(N1),A(N3),NFO,NIMDV,LL,LR,IR,0)
      DO 800 L=LT,LH
      CALL STRSC (A(M)),A(N1),A(N3),NFO,NIMDV,LL,LR,IR,1)
      WRITE(IW,3002) MM,L,( SG(I),I=1,2)
800 CONTINUE
      RETURN
2002 FORMAT(//50H ANALYSIS OF BOUNDARY ELEMENTS - CONSTRAINT FORCES //
154H CONST NUMBER LOAD CASE FORCE MOMENT//)
3002 FORMAT (1X,2I10,4X,2F15.5)
      END

```

```

      SUBROUTINE CLAMP( ID,X,Y,7,NIME,NIMNP)
      *****
C-----BOUNDARY ELEMENT MATRICES
      *****
      IMPLT(1) REAL*8 (A-H,O-Z)
      REAL*4 X,Y,7,FRC
      DIMENSION X(NIMNP),Y(NIMNP),7(NIMNP),ID(NIMNP,6),FMM(86)
      COMMON/FH/LM(6),S(6,6),P(6,4),XM(6),ST(2,6),TT(2,4),FM(2444)
      COMMON/JOINK/R(6),FMI(4),T(4),IF(5),IX(5),XX(5),YY(5),ZZ(5),U(4),
1 V(4),J111(216)
      COMMON/UNIT/IR,IW,IP,I1,I2,I3,IR,I9,I10,I11,I12
      EQUIVALENCE (FMM,S)
      DO 10 I=1,86
10 FMM(I)=0.
      *****
C-----CONTROL INFORMATION
      *****
      N1=1
      N2=6
      N3=2
      N4=1
      N5=1
      N6=1
      N7=0
      IFY=0
      FRC=0.
      WRITE(IW,2000) NIME
      READ(IR,1005) FMI
      WRITE(IW,2005) FMI
      *****
C-----ELEMENT CAPS

```

```

C*****RQIN0550
  WRITF(W,2001)
  N=1
200 READ(IR,1000) IFL,IF,KD,KR,INC,SD,SR,TRACE
  IF(KD.NF.1) KD=0
  IF(KR.NF.1) KR=0
  IF(INC.F0.0) INC=1
  IF(TRACE.F0.0) TRACE= 1.0F 10
  KK=INC*(IFL-N)
  DO 100 I=1,5
100 IX(I)=IF(I)-KK
  IF(IF(3).NF.0) GO TO 210
  DO 101 I=3,5
101 IX(I)=0
210 DO 550 NFI=N,IFL
  DO 110 I=1,5
  II=IX(I)
  IF(II.F0.0) GO TO 110
  XX(I)=X(II)
  YY(I)=Y(II)
  ZZ(I)=Z(II)
110 CONTINUE
  IF(IX(3).F0.0) GO TO 250
  CALL VFCTDR(II,XX(2),YY(2),ZZ(2),XX(3),YY(3),ZZ(3))
  CALL VFCTDR(IV,XX(4),YY(4),ZZ(4),XX(5),YY(5),ZZ(5))
  CALL CROSS(II,V,I)
  GO TO 260
250 CALL VFCTDR(I,XX(1),YY(1),ZZ(1),XX(2),YY(2),ZZ(2))
260 DO 50 J=1,3
  S(I,J)=T(J)*TRACE*KD
  S(I+3,J)=T(J)*TRACE*KR
  R(J)=T(J)*TRACE*SD*KD
  R(J+3)=T(J)*TRACE*SR*KR
  DO 50 J=1,J
  S(I+3,J)=T(I)*T(J)*TRACE*KR
50 S(I+3,J+3)=T(I)*T(J)*TRACE*KR
  DO 500 I=2,6
  II=I-1
  DO 500 J=1,11
500 S(I,J)=S(I,II)
  DO 520 J=1,4
  TT(1,J)=-TRACE*KD*SD*FMUL(J)
  TT(2,J)=-TRACE*KR*SR*FMUL(J)
  DO 520 I=1,6
520 P(I,J)=R(I)*FMUL(J)
  II=IX(I)
  DO 600 I=1,6
600 LM(I)=ID(II,I)
  CALL CALHAM(NDIF,LM,S,P,ST,TT,MU,NV,NS,ND,NW,IND,IE,FRC)
  WRITF(W,2100) NFI,IX,KD,KR,SD,SR,TRACE
  IX(1)=IX(1)+INC
  IX(2)=IX(2)+INC
  IF(IX(3).F0.0) GO TO 650
  DO 650 I=3,5
650 IX(I)=IX(I)+INC
650 CONTINUE
  N=IFL+1
  IF(N.IF.NUMF) GO TO 200
  RETURN
1000 FORMAT(9I5,5X,3F10.0)

```

```

RQIN0560
RQIN0570
RQIN0580
RQIN0590
RQIN0600
RQIN0610
RQIN0620
RQIN0630
RQIN0640
RQIN0650
RQIN0660
RQIN0670
RQIN0680
RQIN0690
RQIN0700
RQIN0710
RQIN0720
RQIN0730
RQIN0740
RQIN0750
RQIN0760
RQIN0770
RQIN0780
RQIN0790
RQIN0800
RQIN0810
RQIN0820
RQIN0830
RQIN0840
RQIN0850
RQIN0860
RQIN0870
RQIN0880
RQIN0890
RQIN0900
RQIN0910
RQIN0920
RQIN0930
RQIN0940
RQIN0950
RQIN0960
RQIN0970
RQIN0980
RQIN0990
RQIN1000
RQIN1010
RQIN1020
RQIN1030
RQIN1040
RQIN1050
RQIN1060
RQIN1070
RQIN1080
RQIN1090
RQIN1100
RQIN1110
RQIN1120
RQIN1130
RQIN1140

```

```

1005 FORMAT (4F10.0)
2000 FORMAT(34H) B O U N D A R Y E L E M E N T S //
      1 23H NUMBER OF ELEMENTS =,15 )
2001 FORMAT(//22H BOUNDARY ELEMENT DATA //
      1 5X,5HCONST,5X,6HNODE,42H /--NODES DEFINING CONSTRAINT DIRECTION--
      2//,5X,5HCONST, 8X,5HDISPL,5X,8HROTATION,4X,5HSTIFF /
      3 4X,6HNUMBER,6X,1HN,8X,2HNI,8X,2HNI,8X,2HNI,8X,2HNI,6X,2HND,3X,
      4 2HND,11X ,1HD,11X,1HP,11X,1HS )
2005 FORMAT (// 25H ELEMENT LOAD MULTIPLIERS//
      * 9X,1HA,4X,1HR,9X,1HC,9X,1HD /4F10.4)
2100 FORMAT(17,5I10,3X,2I5,5X,1P3F12.2)
      END

```

```

RDUM1150
RDUM1160
RDUM1170
RDUM1180
RDUM1190
RDUM1200
RDUM1210
RDUM1220
RDUM1230
RDUM1240
RDUM1250
RDUM1260

```

```

SUBROUTINE TRUSS (A,MTOI)
DIMENSION A(MTOI)
WRITE(A,202)
STOP
202 FORMAT(1X,' PROGRAM ENTERED DUMMY SUBROUTINE TRUSS ' //)
END

```

```

SUBROUTINE BEAM (A,MTOI)
DIMENSION A(MTOI)
WRITE(A,202)
STOP
202 FORMAT(1X,' PROGRAM ENTERED DUMMY SUBROUTINE BEAM ' //)
END

```

```

SUBROUTINE PLANE (A,MTOI)
DIMENSION A(MTOI)
WRITE(A,202)
STOP
202 FORMAT(1X,' PROGRAM ENTERED DUMMY SUBROUTINE PLANE ' //)
END

```

```

SUBROUTINE SHEAR (A,MTOI)
DIMENSION A(MTOI)
WRITE(A,202)
STOP
202 FORMAT(1X,' PROGRAM ENTERED DUMMY SUBROUTINE SHEAR ' //)
END

```

```

SUBROUTINE SHELL (A,MTOI)
DIMENSION A(MTOI)
WRITE(A,202)
STOP
202 FORMAT(1X,' PROGRAM ENTERED DUMMY SUBROUTINE SHELL ' //)
END

```

```

SUBROUTINE RHOINH(A,MTOI)
DIMENSION A(MTOI)
WRITE(A,202)
STOP
202 FORMAT(1X,' PROGRAM ENTERED DUMMY SUBROUTINE RHOINH ' //)
END

```